



Welcome to the first *SeRaMCo* Webinar *Secondary Raw Materials for Concrete Precast Products*

22 June 2020 10:30-12:00 CEST



Programme

10:30	Welcome	Christian GLOCK, University of Kaiserslautern
10:35	Concrete and the challenge of a low-carbon, sustainable and circular construction: Will precast concrete still be used in 2050?	Alessio RIMOLDI, BIBM
10:45	The influence of the crushing production process on the quality of recycled aggregates	Julien HUBERT, University of Liège
10:55	 Availability of recycled material: Characterization of the building stock in Luxembourg Assessment of concrete volumes Availability of the future mineral waste stock based on stochastic scenarios 	Lorenc BOGOVIKU, University of Luxembourg



Programme

11:05	 Development of innovative concrete mixtures: High water demand of the recycled aggregates and the regulating effect of the superplasticizer ACE in a mixture. Effect of the particle size distribution on the workability of concrete. Development of medium to high strength concrete with recycled aggregates 	Gaël Gelen CHEWE NGAPEYA, University of Luxembourg
11:15	Concrete containing recycled aggregates from unknown origin – Development of new concrete mixes for structural precast elements and pavement blocks	Anja TUSCH, University of Kaiserslautern
11:25	Closed-loop supply chain of construction and demolition wastes: Towards a circular economy in French regions	Nacef TAZI, Cerema
11:35	Discussion, questions & answers	All
11:55	Wrap-up	Christian GLOCK, University of Kaiserslautern
12:00	End	



Concrete and the challenge of a low carbon, sustainable and circular construction

Will precast concrete still be used in 2050?

Webinar 22nd June 2020 Alessio RIMOLDI Secretary General

bibm





Construction 2050

- Low carbon
- Sustainable
- Circular

Zero pollution





 Low carbon
 o. business as usual











• Low carbon - Mitigation

Designers				
Designers Optimisation High-strength concrete Digitalisation	Raw materials Cement • Energy • Material/process Aggregates • Recycled • Artificial	Precast manufa Circularity • Long service life • Easy maintenance and repair • Easy disassembly Innovation	Acturers Society Concrete benefits • Energy efficiency • Adaptation to CC • Healthy and safe places	

• Low carbon - Removal





(INTERNAL) Carbonation





ABSORPTION OF CO2 IN CONCRETE



- Curing of precast concrete with CO₂
- Sequestration during lifetime of construction
- Recycled concrete fines recarbonate with CO₂



USER NEEDS & TECHNICAL REQUIREMENTS

HOLISTIC

Construction work Whole life cycle













Concrete

♦ High quality ♦ Long service life ♦ Fire safety ♦ Versatility ♦ Healthy ♦ Affordable ♦ Aesthetic Thermal comfort Acoustic comfort

Respond to societal challenges

Healthy & Comfortable

Safe and resilient

ocial



Natural materials



Temperature

Thermal Mass

Environment

Climate resilient

• Circular – decoupling economic growth from resource use



Circular in construction



Ensure a service life as long as possible

Favour internal processes with lower energy

- Repair
- Maintain

Avoid "exiting"

- Re-use
- Recycle

MINIMIZATION AND PREVENTION



Most favored

Average

Least favored

MINIMIZATION AND PREVENTION



Durability

Easy maintenance and repair

New Concretes





PRODUCT REUSE



GEOTECHNICAL WORKS







RECYCLED AGGREGATES Conclusion

PRECAST provides solutions to the challenges of construction 2050

Low-carbon

Sustainable

♦ Circular

♦ Fire resistance Adapting to climate change ♦ Affordable Thermal comfort ♦ Resilient **PRECAST** provides

Solutions to other societal challenges



PRECAST will be the

backbone

for a transition to Construction 2050





Not an obstacle

Conclusion

Providing that the precast industry

3. Fully embraces circular economy principles



1. Engages in a transition towards **low-carbon** together with stakeholders



2. Keeps on manufacturing with **sustainability** in mind





Thank you for attention.

Secondary Raw Materials for Concrete precast products

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Recycled aggregates properties – Influence of the crushing method

SeRaMCo Webinar

22nd of June 2020

J.Hubert, Z. Zhao, F. Michel & L. Courard (ULiege)

Summary of the presentation



- Materials and methods
 - Crushing methods
 - Concrete compositions
- Results
 - Grain size distribution
 - Morphology of the aggregates
 - Cement paste content
 - Water absorption
- Energy consumption study

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Materials and methods

Crushing methods Production of 0/25

Impact crusher

Set at 6,5 kW (40% of maximum power)

Jaw crusher

Interreg

SeRaMCo

North-West Europe





Jaw crusher set at a 22 mm opening

Materials and methods

Concrete compositions



	1.0	1.1	1.2	2	3
Name	Reference	CEMIII	Sandstone	Low Cement	Low W/C
Aggregates type	Limestone	Limestone	Sandstone	Limestone	Limestone
Cement type	CEMI 52.5	CEMIII 52.5	CEMI 52.5	CEMI 52.5	CEMI 52.5
Cement quantity (kg/m ³)	400	400	400	320	452
Cement paste volume (dm ³ /m ³)	351	358	351	282	351
W/C	0.56	0.56	0.56	0.56	0.46

Grain size distribution



The jaw crusher produces aggregates with a more constrained grain size range



Morphology



The flakiness index decreases with increasing granular fraction and the jaw crusher produces flakier aggregates

No influence of the concrete composition in the investigated range



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Cement paste content



Decrease in cement paste content with increasing granular fraction No influence of the crushing method



Water absorption

Interreg EUROPEAN UNION North-West Europe SeRaMCo European Regional Development Fund

Decrease in water absorption with increasing granular fraction



Water absorption



No significant influence of the crushing method on the water absorption of the recycled aggregates (for all tested composition)



Energy consumption study



	Jaw crusher	Impact crusher
(a) Running power (kW)	1,8-2,0	6,5-6,6
(b) Mean net power (kW)	1,9-2,1	0,5-0,8
(c) Mean crushing duration (s)	200	252
(d) Crushed mass of material per hour (t/h)	2,0-2,3	1,6-1,7
(e) Net specific energy consumption (kWh/t) (b/d)	0,9-1,0	0,30-0,50
<pre>(f) Total specific energy consumption (kWh/t) ((a+b)/d)</pre>	1,8-1,9	4,1-4,5
<pre>(g) Percentage of energy consumed for crushing (=b/(a+b))</pre>	~50	~10
Crushing specific energy analysis



No correlation between jaw crusher specific energy consumption and impact crusher specific energy consumption

No correlation between specific energy consumption and compressive strength



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Conclusion



	Impact crusher	Jaw crusher	
Aggregates geometry	More spherical	_	
Grain size distribution	_	More constrained	
Fine content	_	Less fine content	
Cement paste content	No influence	No influence	
Water absorption	No influence	No influence	
Energy consumption	-	Less consuming	
Crushing duration	_	Shorter	





Thank you for your attention

The work was carried out thanks to the financial support of the European Commission in the framework of the **Interreg NWE SeRaMCo project**

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UNIVERSITY OF LUXEMBOURG Department of Engineering

Recycled Aggregates Concrete

Dr. Gael CHEWE NGAPEYA Prof. Dr.-Ing. Danièle Waldmann

Luxembourg, June 2020

High water demand of RAC





High water demand of RAC

- The higher the mortar content is, the higher the porosity of RA, and the higher the water absorption.
- The water absorption of RA is 2.3 to 4.6 times higher than that of natural aggregate, irrespective of the original concrete strength. [3,4]
- The high water demand of RA leads to a reduction of the workability of RA concrete.
- The high water demand of RA leads to a reduction of the workability of RA concrete.

[3] T.C. Hansen, N. Henrik, Strength of recycled concrete made from crushed concrete coarse aggregate, Concr. Int. 5 (1) (1983) 79-83
[4] S.R. Suryawanshi, B. Singh, P. Bhargava, Characterization of recycled aggregate concrete, Adv. Struct. Eng (2015) 1813-1822.



[2] Z.H. Duan, C.S. Poon, Properties of recycled aggregate concrete made with recycled aggregates with different amounts of old adhered mortars, Materials and Design 58 (2014) 19-29



High water demand

42

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Medium to high trength concrete

Particle size distribution and workability of concrete

As the RA gradually

crumbles

uni. In

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The adhered mortar content increases with the decrease in the aggregate size.

Cement mortar

accumulates in fines RA

- The saturated surface dry density decreases with the absorption, i.e. with the adhered mortar content, i.e. with the particle size distribution.
- A proportion of more than 20% recycled fine aggregate results in a large reduction of the workability, a phenomenon linked to the saturated surface dry-density of RA.



manufacture of concret

properties in the characterisation of mixed recycled aggregates for use in the

Density of recycled fine

aggregate decreases

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Development of medium to high strength concrete

The interfacial transition zone strongly impact the performance of RA concrete

Soft interface provides a major interfacial cracking mode, while stiff interface induces a main bulk cracking behavior.

ͺΥ Δu_y ↑↑↑↑↑↑↑↑↑↑↑↑

- (a) Geometry/boundary conditions (b) Soft interphase (c) Stiff interphase (c) Stiff interphase (c) Stiff interphase (c) Stiff interphase
- An enhancement of the ITZ performance results in an improvement of the compressive strength of RA concrete.

The ITZ enhancement could be achieved by:

1- A two stage mixing approach for improving the micro structure of old adhered mortar.

2- A separation of adhered mortar or a treatment with a polymer solution



recycled concrete by using a phase field model. A high risk of cracking is noted [22, 23]

Medium to high strength concrete



Development of medium to high strength concrete

Mixing procedure



□ Improve the microstructure of old mortar

Enhance the performance of the ITZ by producing a thin layer of cement slurry on RA.





MDĬ.

It is already known that the concrete compressive strength decreases with the increase of the replacement rate of NA with recycled ones, irrespective of aggregate type.

Low performance of the Interfacial Transition Zone

Low bonding between old attached mortars and the fresh mortar paste

□ High-Strength Concrete

Micro-silica ~ 2% of the binder weight Superplasticizer ~ 3 % of the binder weight Binder to aggregate ratio ~ 1:3.6 Water to binder ratio w/b ~ 0.35 Particle size skeleton reconstructed

 $f_{c,28} = 5.7 MPa$

E = 1500 MPa

 $f_{c,28} = 58.5 MPa$

E = 29500 MPa

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Developed concretes using 100% of recycled aggregates from known origin

Open Structure Concrete

Micro-silica ~ 2% of the binder weight

Binder to aggregate ratio ~ 1:2.9
 Water to binder ratio w/b ~ 0.35
 Particle size skeleton reconstructed

Self-Compacting Concrete

Master air ~ 0.15% of the binder weight Superplasticizer ~ 1.5% of the binder weight Binder to aggregate ratio ~ 1:3.1 Water to binder ratio w/b ~ 0.35 Particle size skeleton reconstructed

 $f_{c,28} = 32.4 MPa$

E = 6700 MPa

Villmools Merci!





Concrete containing recycled aggregates from unknown origin Development of new mixes for structural precast elements and pavement blocks



Anja Tusch



Aim



Development of different new concrete mixes containing recycled aggregates from unknown origin





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Challenges

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Production of concrete containing recycled aggregates from unknown origin causes some challenges:







Mixture for the production of structural elements

Mixture for the production of non-structural elements

Rammed concrete

Salty concrete







Crushed concrete

Type A (except R_a)

WA24: 4–5 %

Density: 2.3 kg/dm³

Fractions: 2-6 mm, 6-14 mm, 14-22 mm



Mixed aggregates

Type B (except R_a)

WA24: 6-9 %

Density: 2.2 kg/dm³

Fractions: 2-6 mm, 6-14 mm, 14-22 mm





Mixture for the production of structural elements

Mixture for the production of non-structural elements/ Pavement





Starting point: Development of a concrete mixture, which can be used for different structural elements

Challenge: The products are not known yet and the mixture has to be very variably

Planned test procedure:

- Design a mixture which is able to match C 30/37 by using a standard CEM I 42.5 and recycled aggregates
- Using two different w/c ratios for the concreting of the mixture → w/c: 0.45; 0.55
- Verify the results by using different cements → CEM II 42.5; CEM I 52.5







Results test series 1:



The variations of the w/c ratio results in a scattering of the compressive strength





Results test series 2:



- Crushed concrete, 28d, CEM II 42.5 N
- Crushed concrete, 28d, CEM I 52.5 N
- Mixed aggregates, 28d, CEM II 42.5 N
- Mixed aggregates, 28d, CEM I 52.5 N
- Theoretical strength CEM 42.5, 28d
- Theoretical strength CEM 52.5, 28d





Mixture for the production of structural elements

Mixture for the production of non-structural elements/ Pavement



Development of the concrete mix for non-structural elements / paving blocks



Requirements:

- Slump 0 (earth-moist concrete)
- High early age strength
- The resulting concrete has to fulfill the standards of EN 1338

Challenge: Properties of the product depend on the mixture as well as on the used process technology







Development of the concrete mix for non-structural elements / paving blocks



Test procedure:





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Development of the concrete mix for non-structural elements / paving blocks



First results



Procedure to find a suitable mixture:

- Selection of aggregates
- Determination of average cement content (corresponds to mixing ratio)
- Determination of the optimum water content in the test
- Preparation of samples and determination of strength (applying strength by cement content)
- Calculation of the mixture composition from the ingredients



Development of the concrete mix for non-structural elements / paving blocks



Results green strength

Parameter	Influence			
Water content	Most important (optimum = W _{opt})			
Concrete composition (cement content and specific surface!)	Increasing with increasing cement content and specific surface			
Grading curve of aggregates	Minor influence			
Admixtures/additives	Depends on individual case (mixing ratio, added amount)			
Compaction energy	Important			





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Development of the concrete mix for non-structural elements /

paving blocks

Results green strength

BAUINGENIEURWESEN

Mix	Mixing ratio	W	С	FA	QP	Aggregates
1	1:6	х	х	0	0	Gravel
2	1:5	х	х	0	0	Crushed concrete
3	1:6	х	х	0	0	Gravel
4	1:5	х	x	0	0	Crushed concrete
5	1:5	х	х	х	0	Gravel
6	1:5	х	х	0	х	Gravel
7	1:5	х	х	х	0	Gravel
8	1:5	х	х	0	х	Gravel
9	1:5	х	х	х	0	Crushed concrete
10	1:5	х	х	0	x	Crushed concrete



□ M7/G, FA o M9/R, FA △ M2/G ■ M8/G, QP ● M10/R, QP ▲ M4/R



🗆 M2, G 🔹 M4, RC





Thank you for your attention!







Centre d'étude et d'expertise sur les risques, l'environnement, la mobilité et l'aménagement

Closed-loop supply-chain of construction and demolition wastes: Towards circular economy in French regions

N. TAZI, R. IDIR and A. BEN FRAJ





- The necessity to handle inert wastes from dwellings construction and demolition
- Methods
- Results in nutshell
- Conclusions and perspectives





- Assess the ability of a region to reach a sustainable reverse logistic model in the construction and demolition sector
- Stock deposit
- Assessment of inert wastes from dwelling stock
- Avoided resource indicator









Model framework







Annual flows from inert wastes







Chronological concrete flows generated in French regions from collective (left) and individual (right) dwellings





Annual recycled inert wastes (regional)

Vs.

Regional natural resource depletion (NA)







Sustainability criterion




- Towards circular economy in the construction sector (locks and opportunities)
- MCDA of recycling processes of CDW
- Environmental assessment of the reverse logistic





process













Centre d'étude et d'expertise sur les risques, l'environnement, la mobilité et l'aménagement

Closed-loop supply-chain of construction and demolition wastes: Towards circular economy in French regions

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June, 22





Discussion, questions & answers



Save the date:

SeRaMCo Final Conference "Precast Concrete in the Circular Economy"

15-16 February 2021 University of Kaiserslautern, Germany



Thank you for your attention.

We hope to see you again at our next webinar!

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