

Real-time surgical simulation using a lattice-continuum approach

Implementation and verification

Huu Phuoc Bui¹, Hadrien Courtecuisse¹, Stéphane P.A. Bordas², Stéphane Cotin³



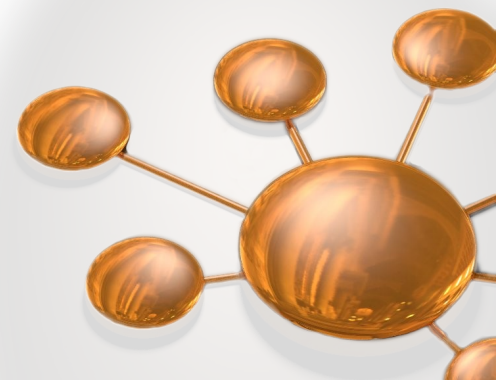
¹ ICube laboratory, University of Strasbourg

² University of Luxembourg

³ Mimesis team, Inria

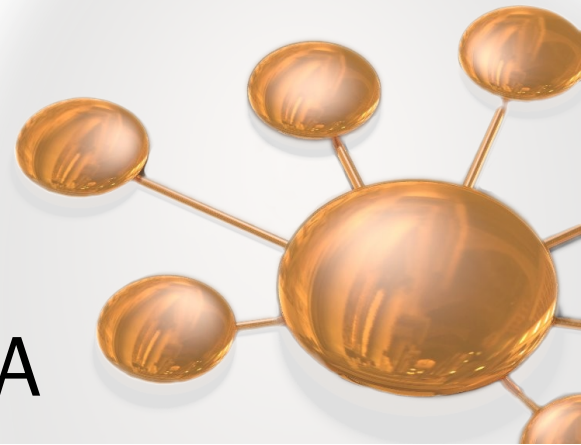


SOFA



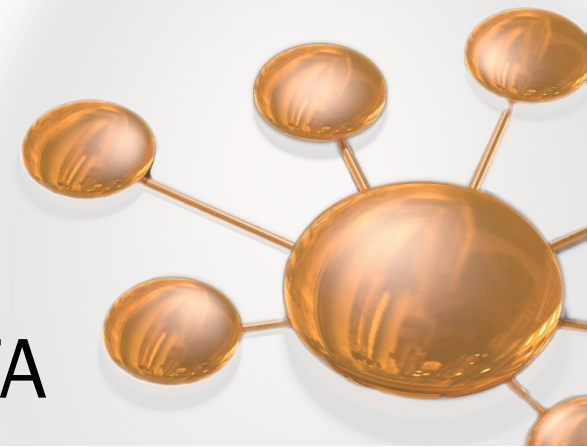
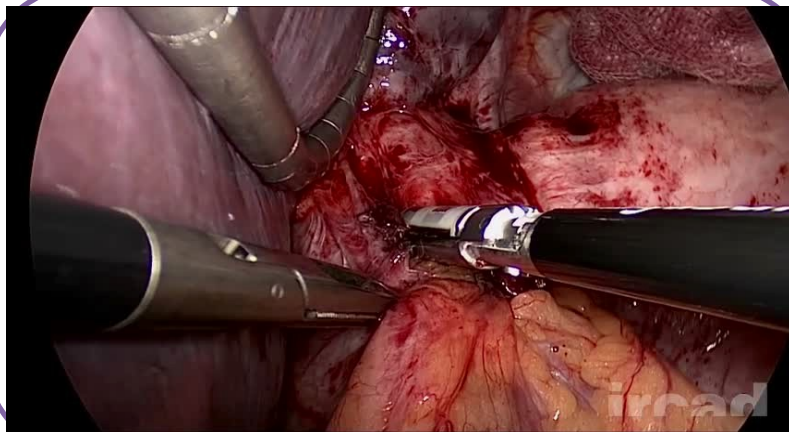
Some words about me

- ▶ PhD at University of Grenoble (November 2013)
Multiscale approach of concrete structure failure
- ▶ Lecturer (ATER) at 3SR laboratory (2014)
Segmentation of cracks in concrete structure
- ▶ Arrived in Strasbourg (September 2014)



Context

- ▶ Surgery: complex practice
 - ▶ Experiences of surgeons
 - ▶ A number of risks



SOFA

Context

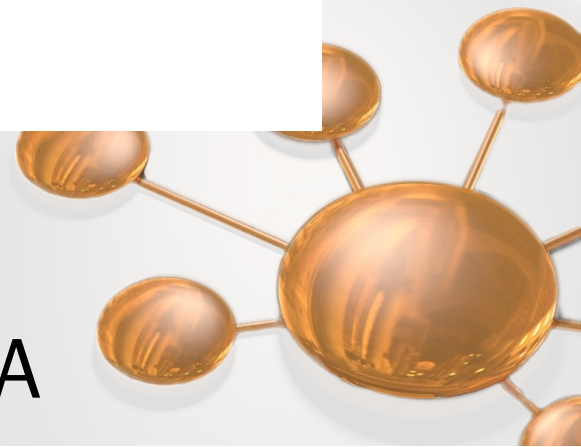
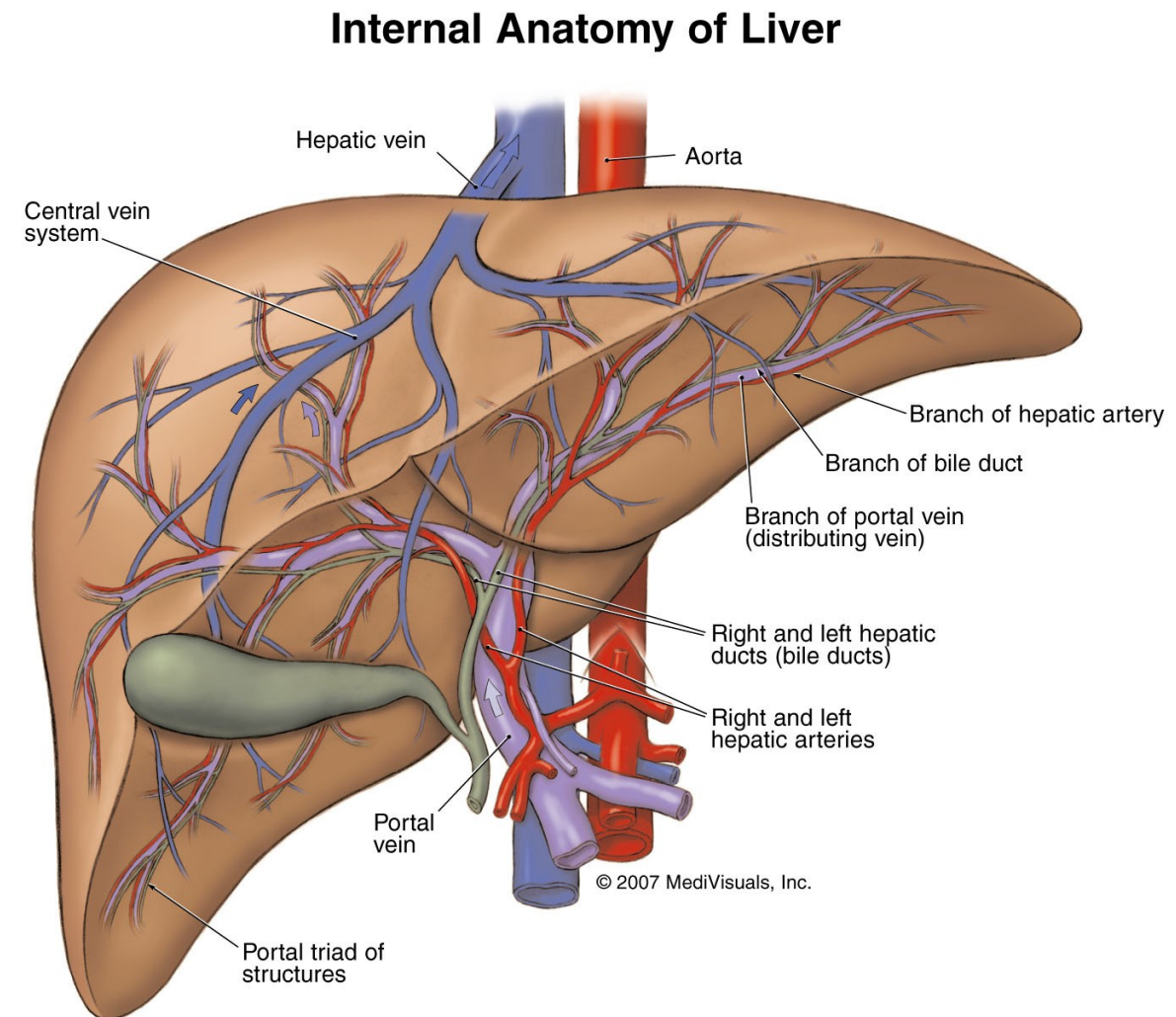
Courtecuisse *et al*, 2013

► Computer-based simulation

- Surgical training
- Guidance
- Surgical robotics

► **Challenges:** cutting, tearing, needle insertion, ...

- Topological changes
- Contacts
- **Microstructure** of the tissue (discontinuities, holes,)

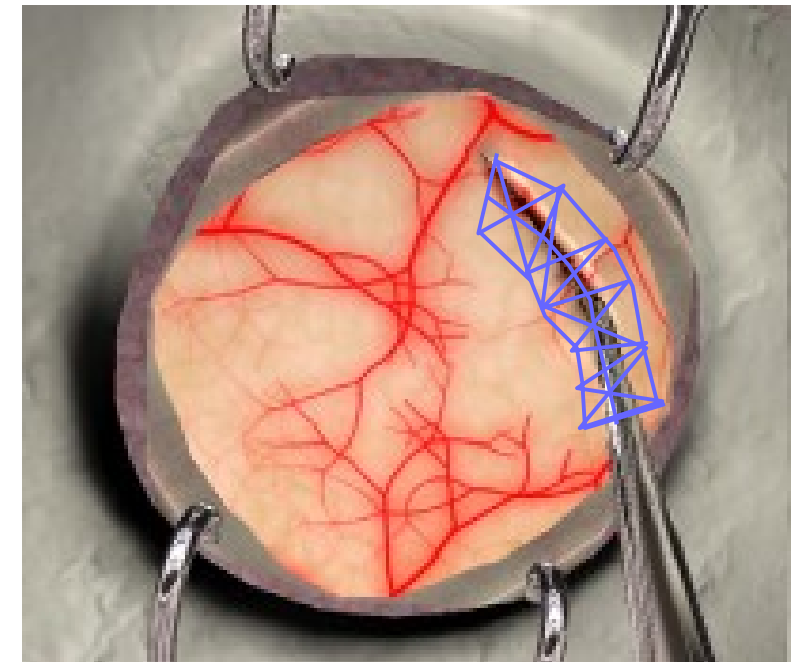


Objectives

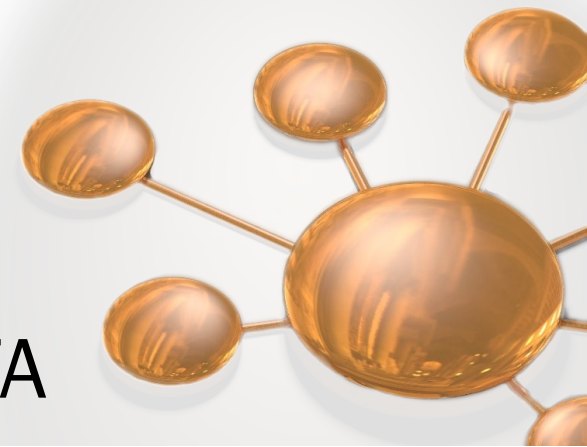
- ▶ Development of numerical tool
 - ▶ Real-time simulation
 - ▶ Multi-domain: continuum-lattice approach
 - ▶ Multiscale: macro, mesoscopic scale (material scale)

- ⇒
- ▲ Computational gains
 - ▲ Increase the quality of the cut

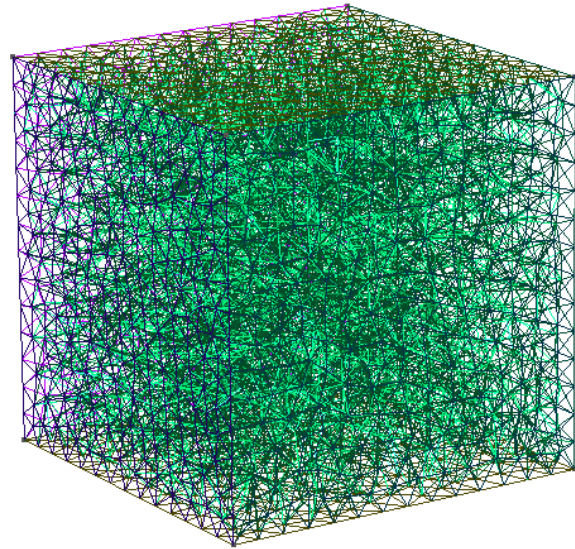
- ▶ The algorithm is implemented into SOFA framework



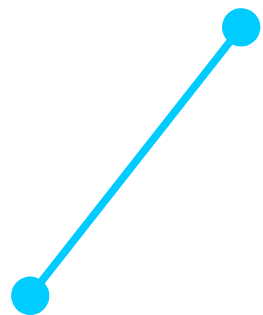
SOFA



Lattice approach

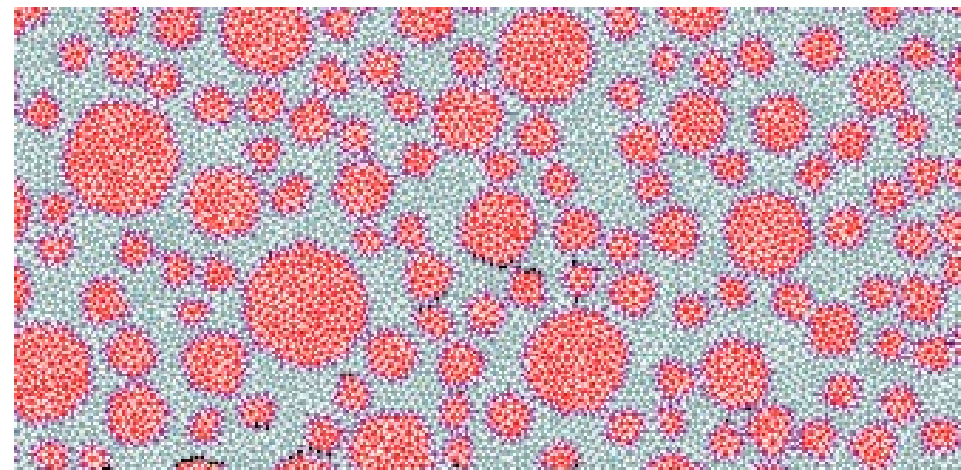


Discretization by 1D elements

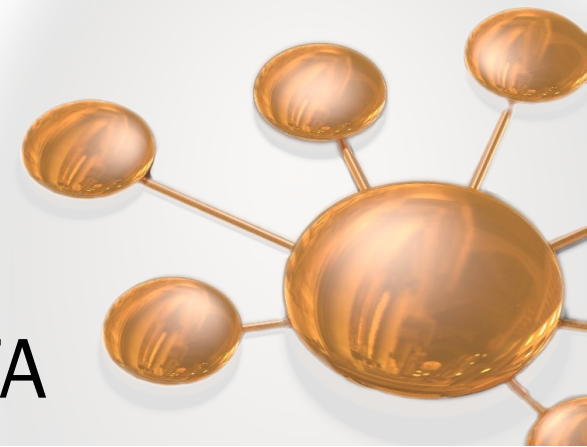


- Beam element
- Truss element

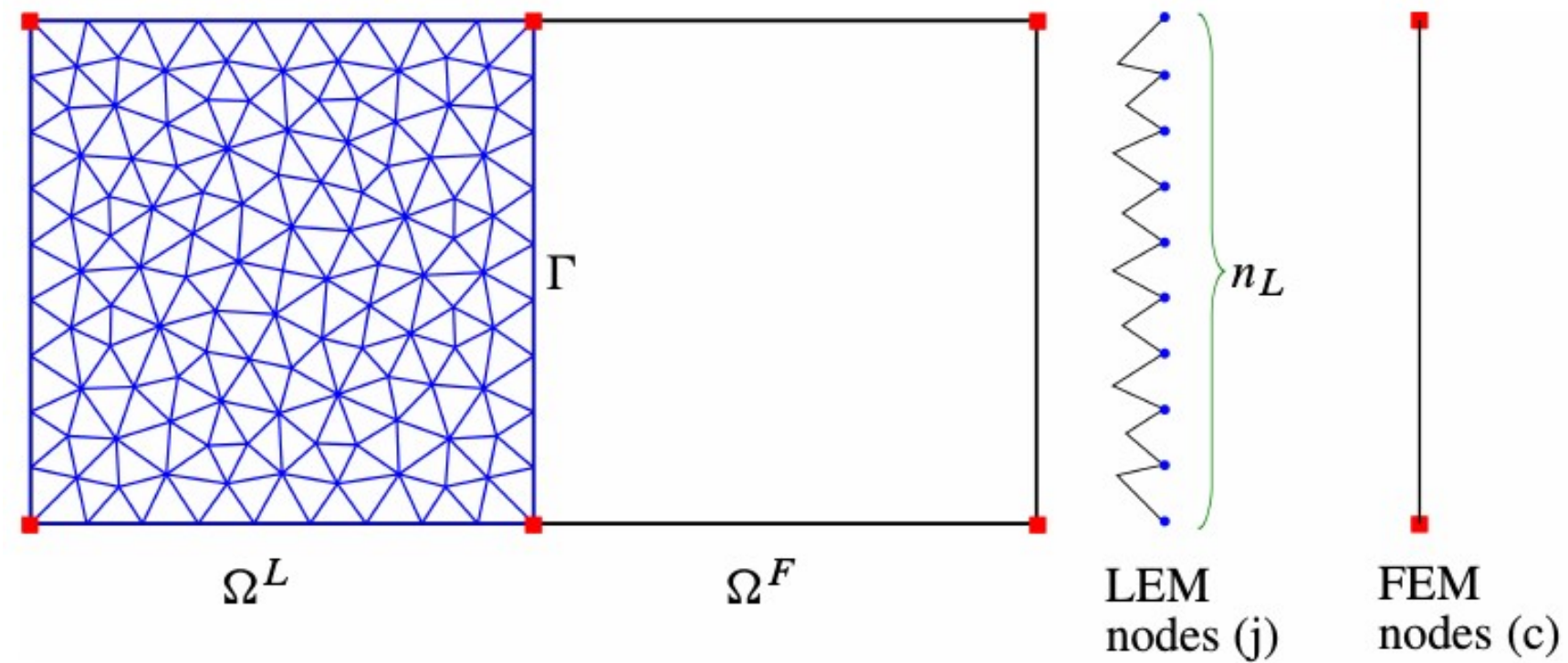
- ▲ Discrete model: suitable for discontinuity problems
- ▲ Simplicity to incorporate fracture, cutting
- ▲ Modeling of material heterogeneity



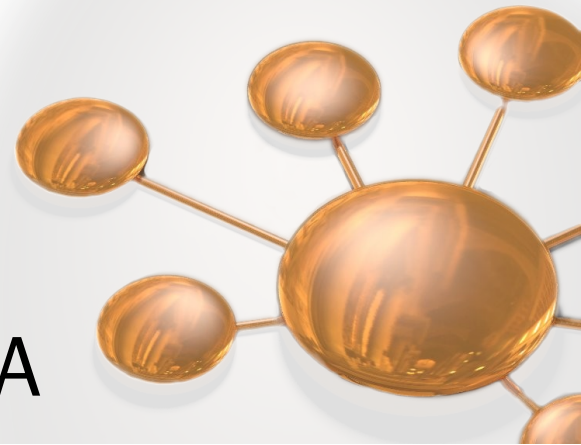
▼ Computational cost



Continuum-lattice approach



$$\mathbf{u}_j^L = \mathbf{N} \cdot \mathbf{u}_c^F = N_c(\mathbf{x}_j) \cdot u_c, \forall j = \{1, 2, \dots, n_L\}$$



Coupling methods

1. Penalty method: with penalty coefficients $\alpha \gg 1$

$$\int_{\Gamma_i} \alpha \|(\mathbf{u}^F - \mathbf{u}^L)\|^2 d\Gamma_i$$

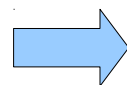
2. Lagrange multipliers:

$$\int_{\Gamma_i} \boldsymbol{\lambda}(\mathbf{u}^F - \mathbf{u}^L) d\Gamma_i$$

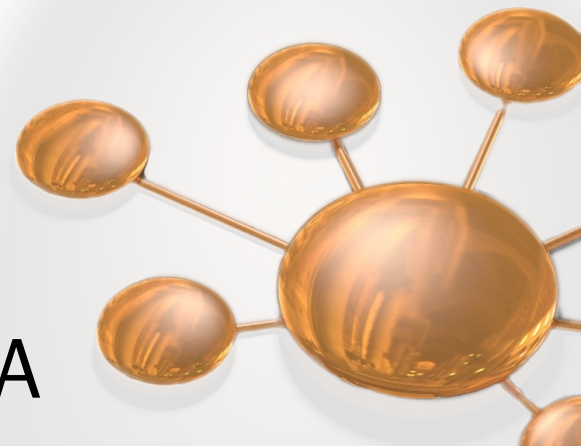
3. Master/slave approach (*Belytschko et al, 2000*):
F :master, L: slave

$$\mathbf{u}^L = \mathbf{J} \mathbf{u}^F$$

$$\mathbf{F}^F = \mathbf{F}^F + \mathbf{J}^T \mathbf{F}^L$$



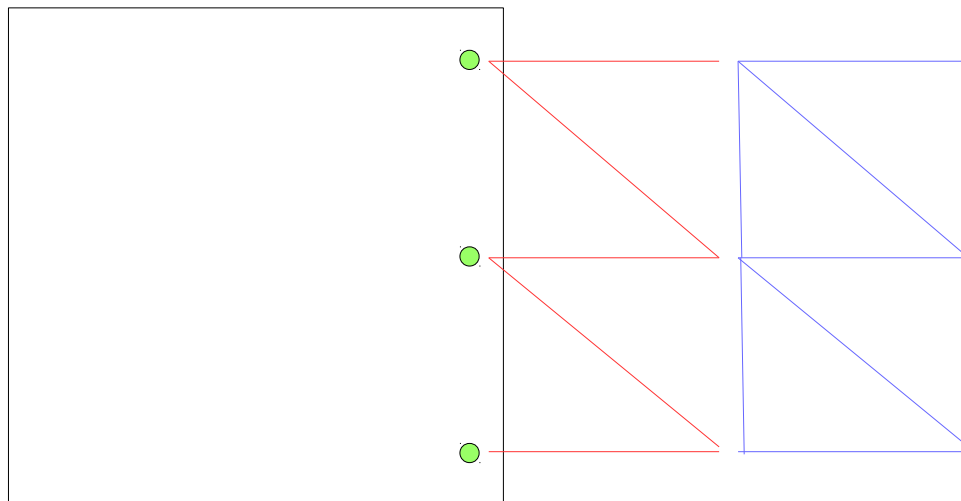
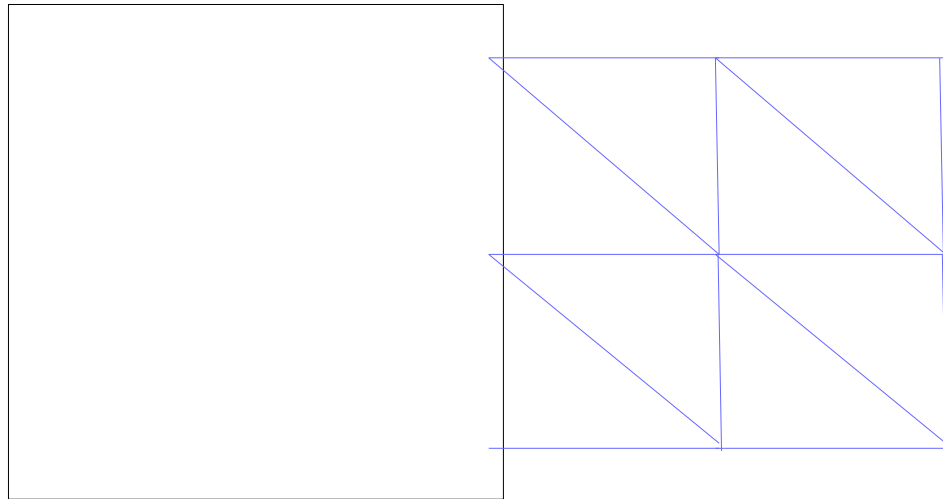
Mapping mechanism in SOFA



FEM-LEM coupling

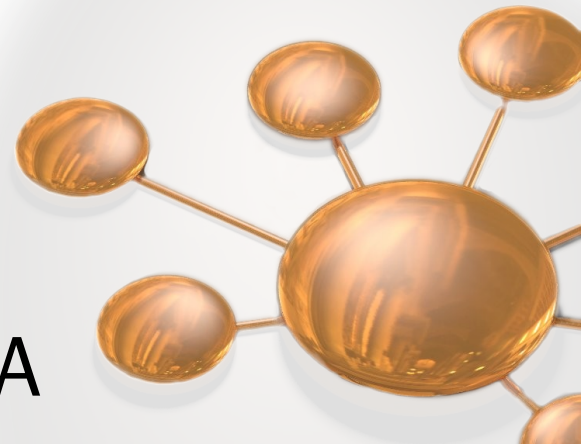
FEM

LEM

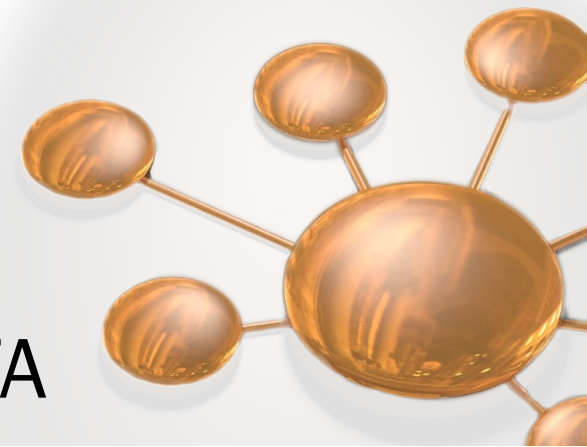


➡ **Multi-mapping** mechanism in SOFA

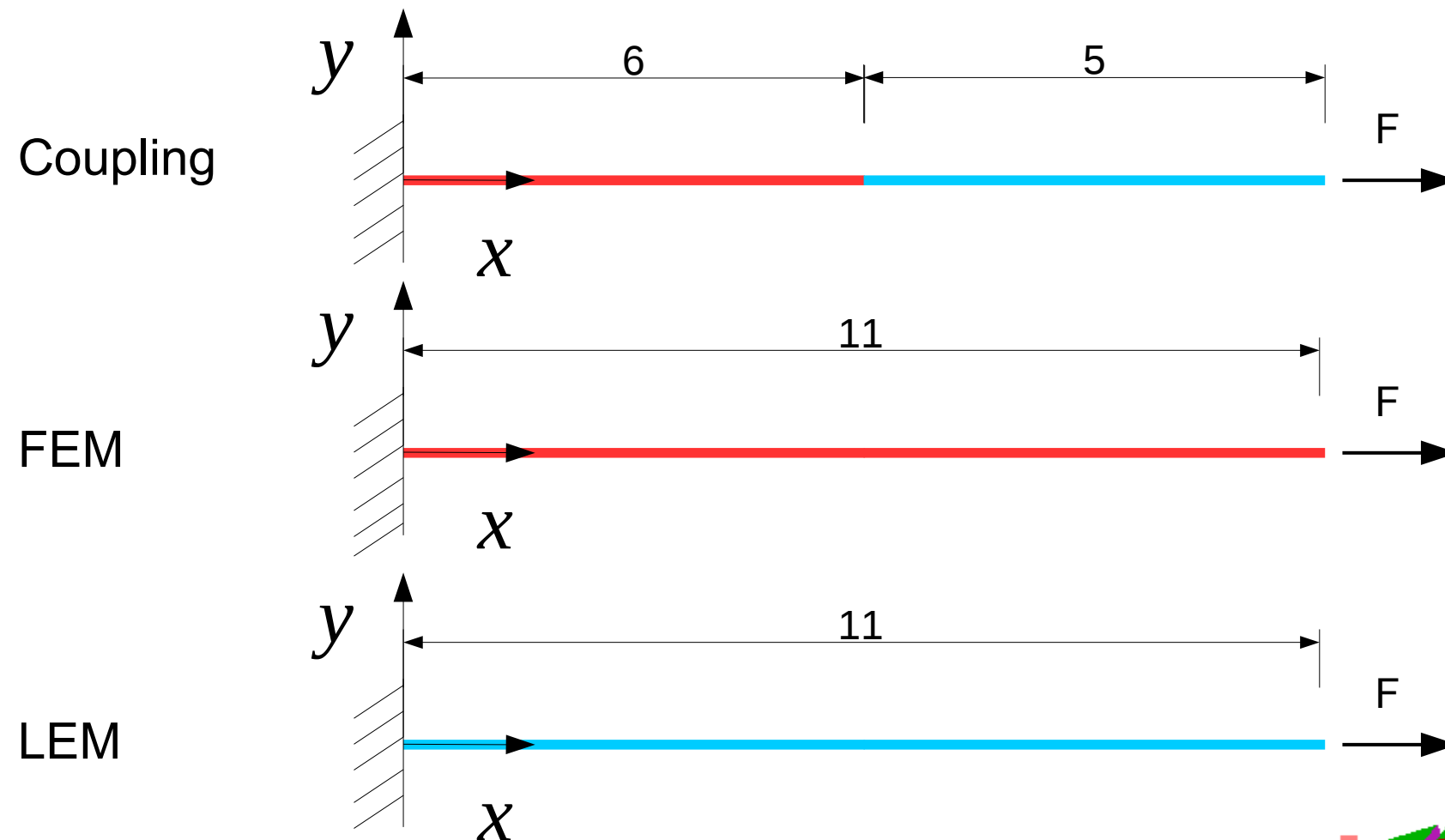
SOFA



Verification tests



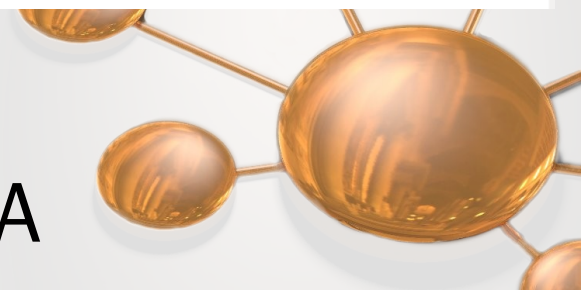
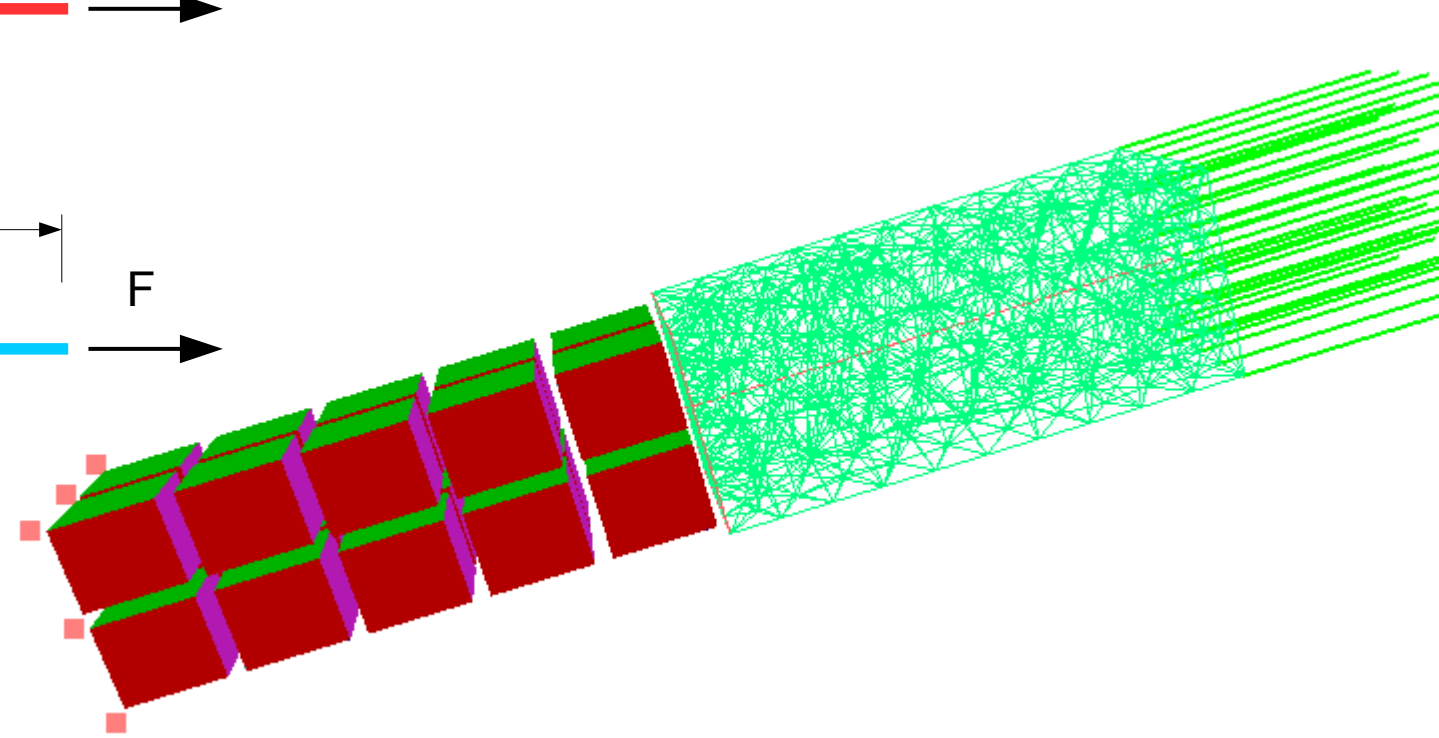
Verification tests: 3D tensile test



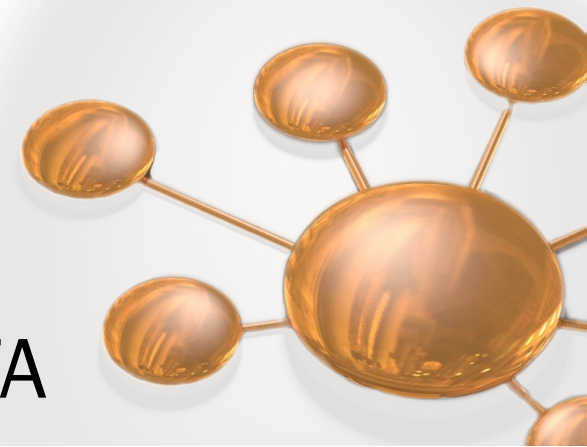
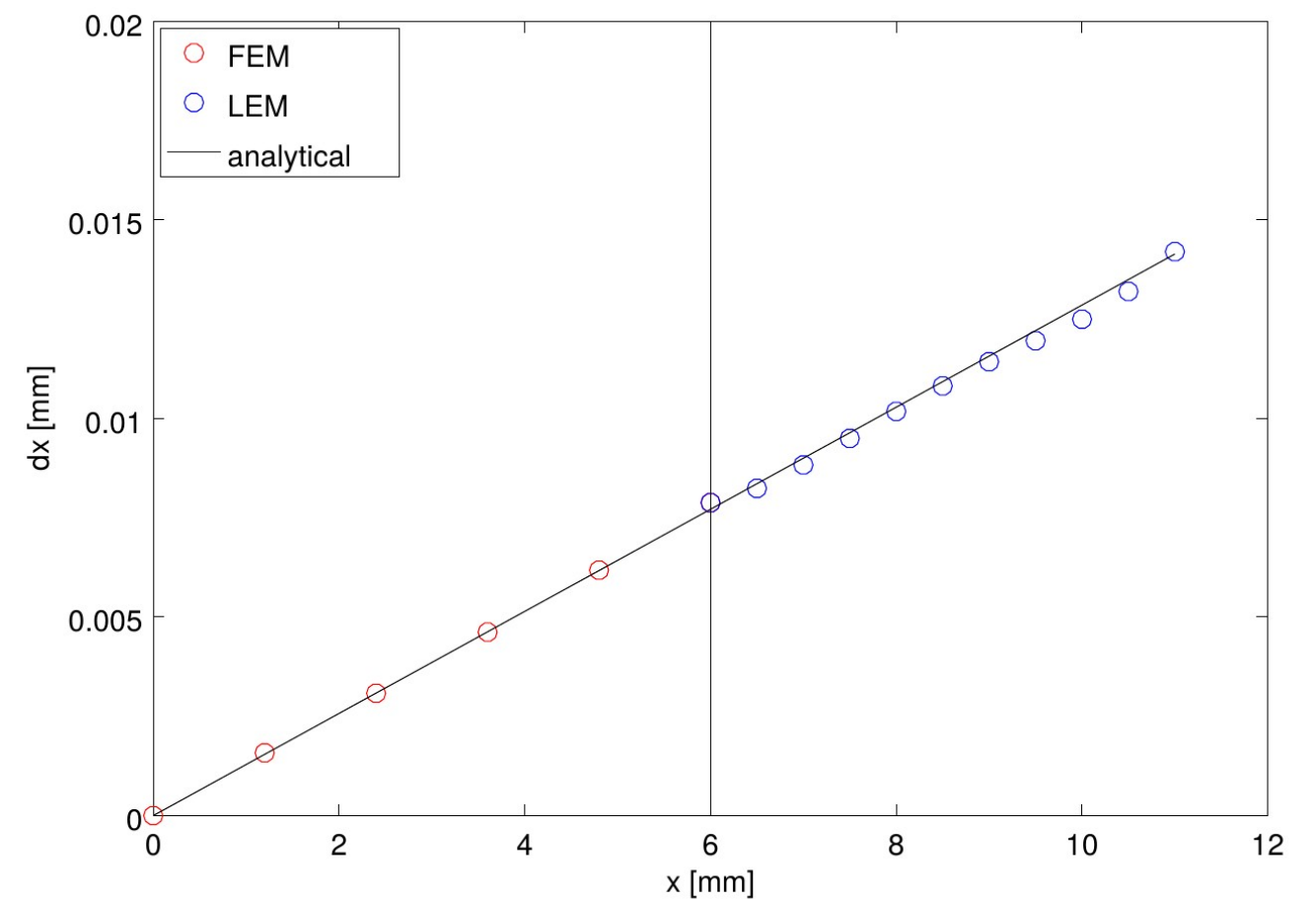
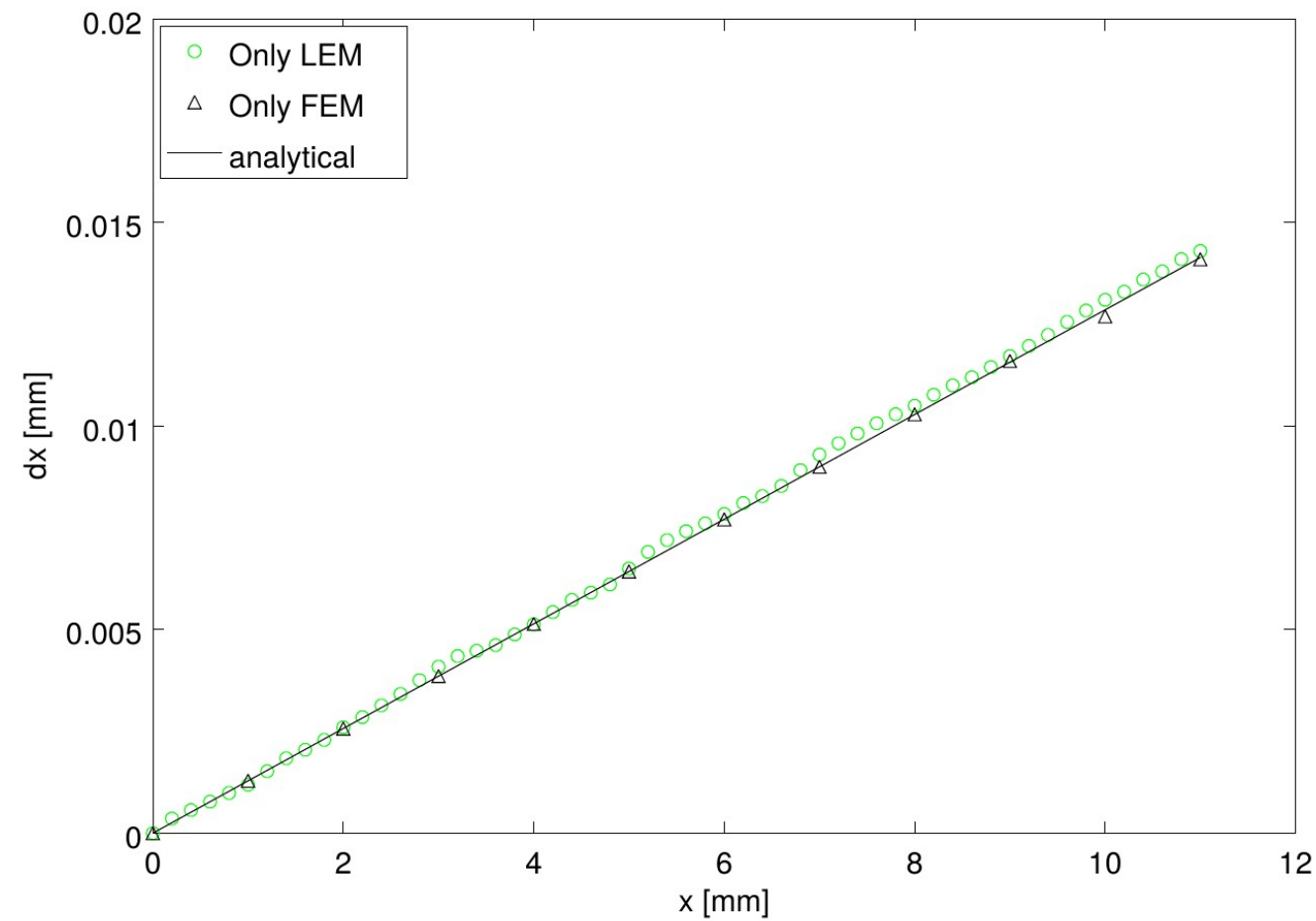
$E = 19.5 \text{ GPa}$
 $\nu = 0.1$
 $b \times h = 2 \times 2 \text{ mm}$
 $F = 100 \text{ N}$

Analytical solution

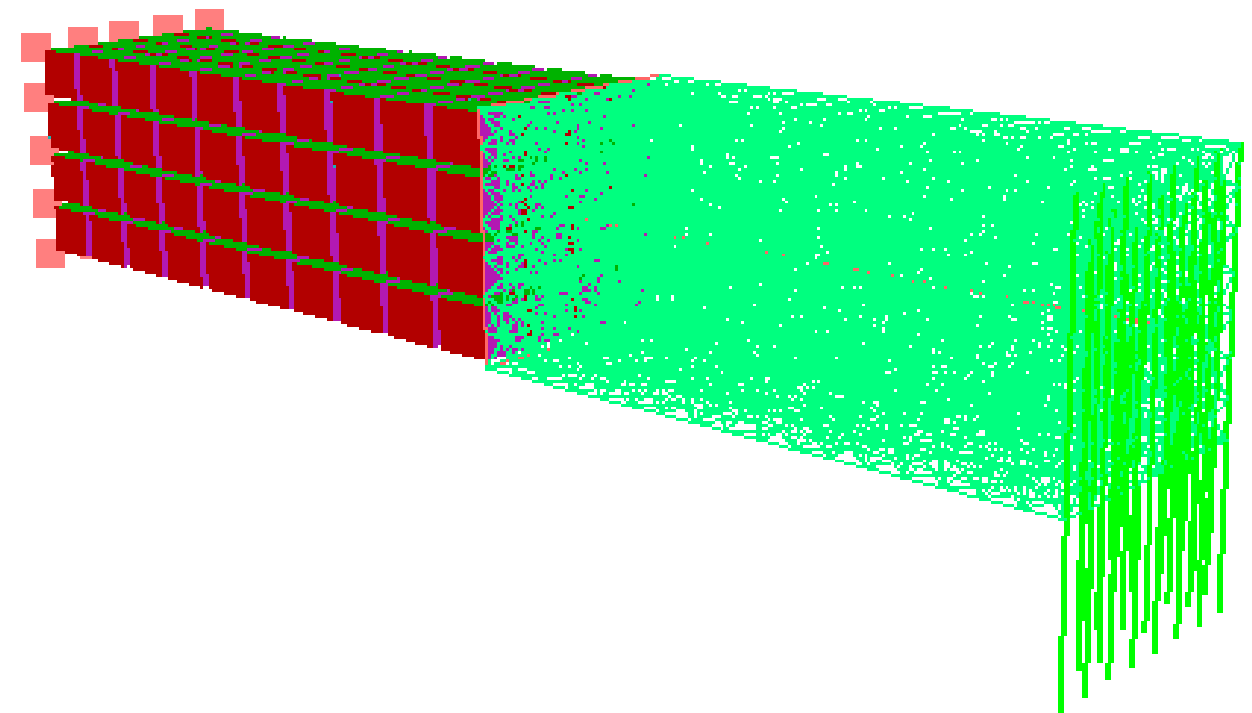
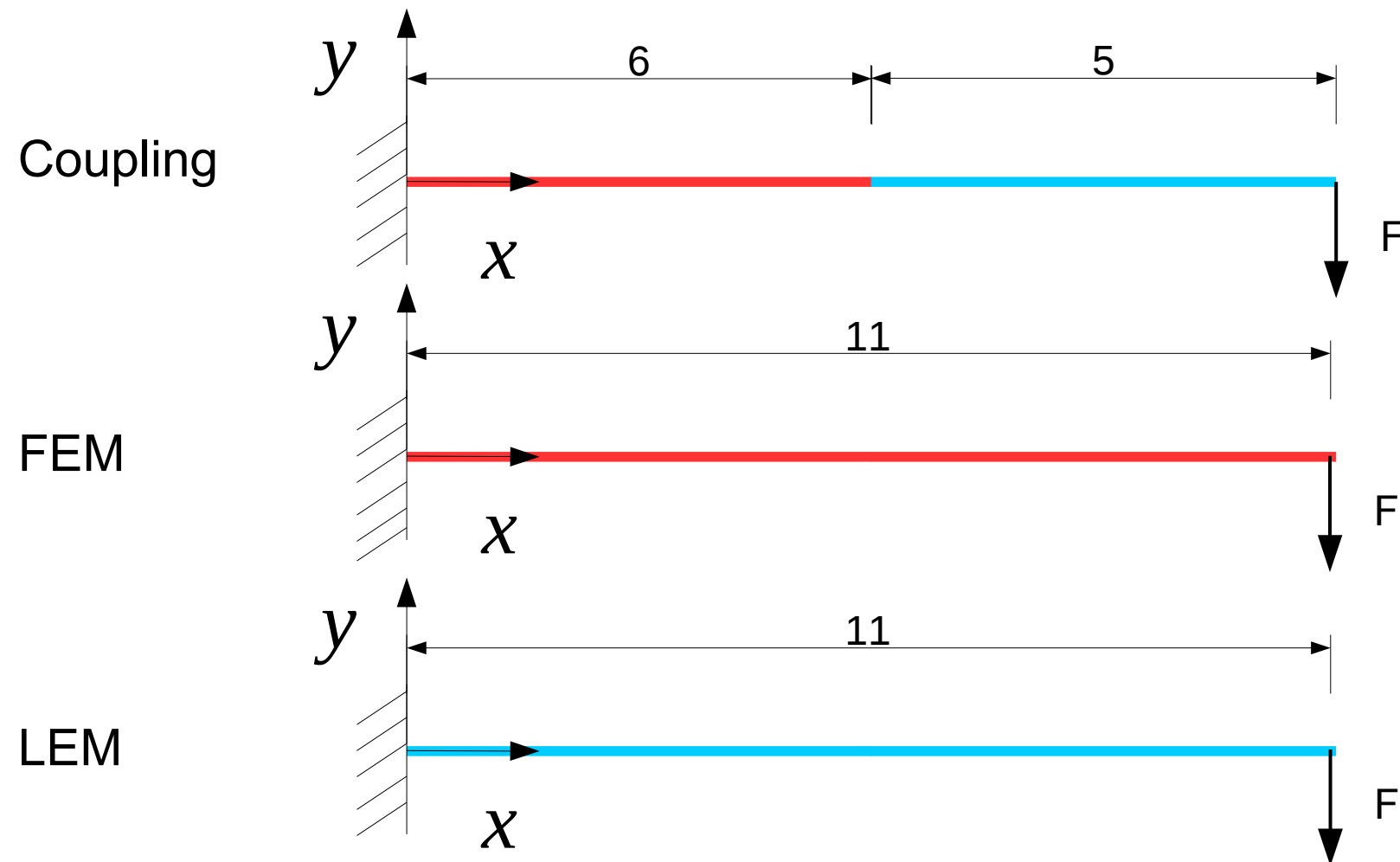
$$u(x) = \int \frac{F}{EA} dx = \frac{F}{EA} x$$



Verification tests: 3D tensile test

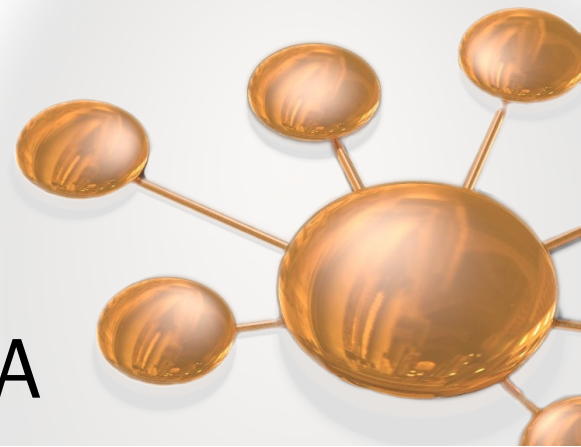


Validation tests: 3D bending test

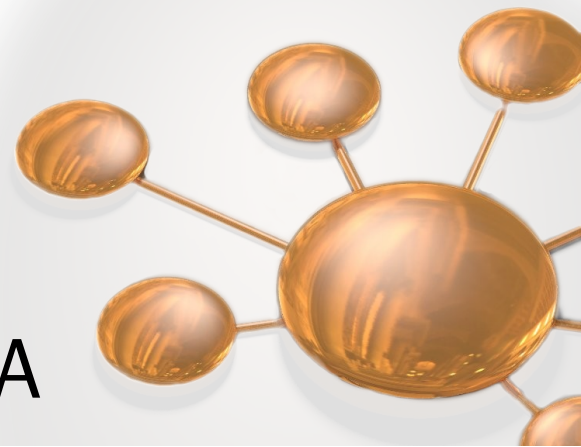
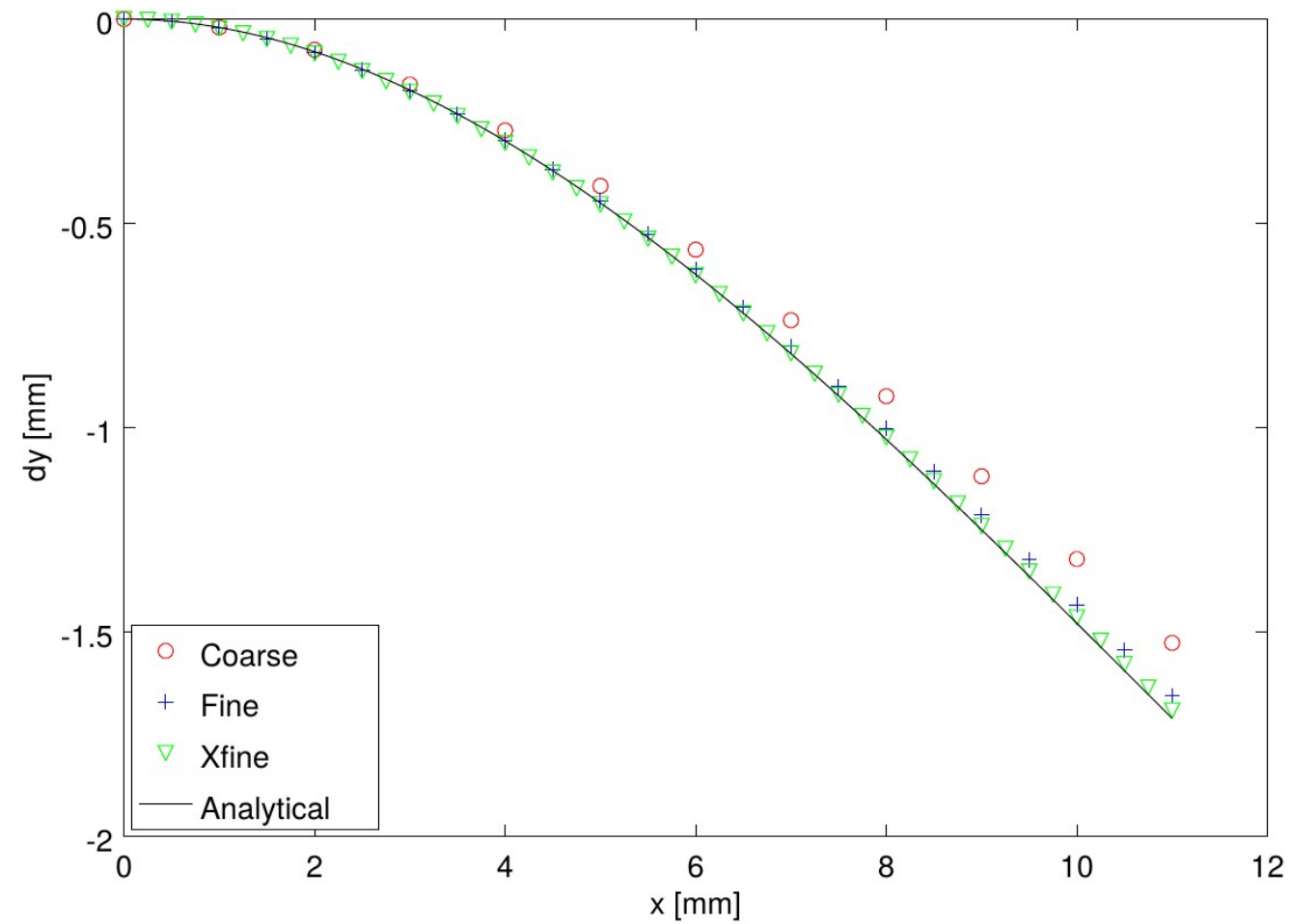


Analytical solution

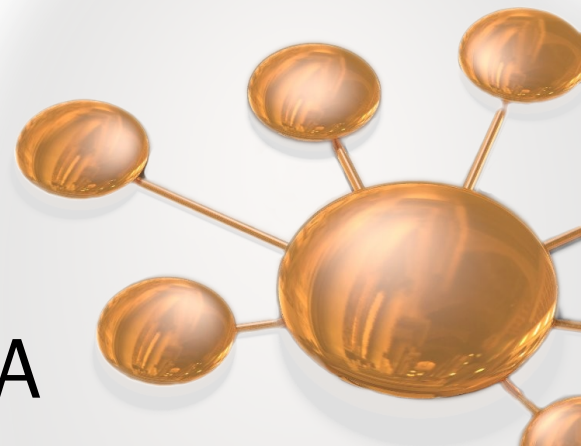
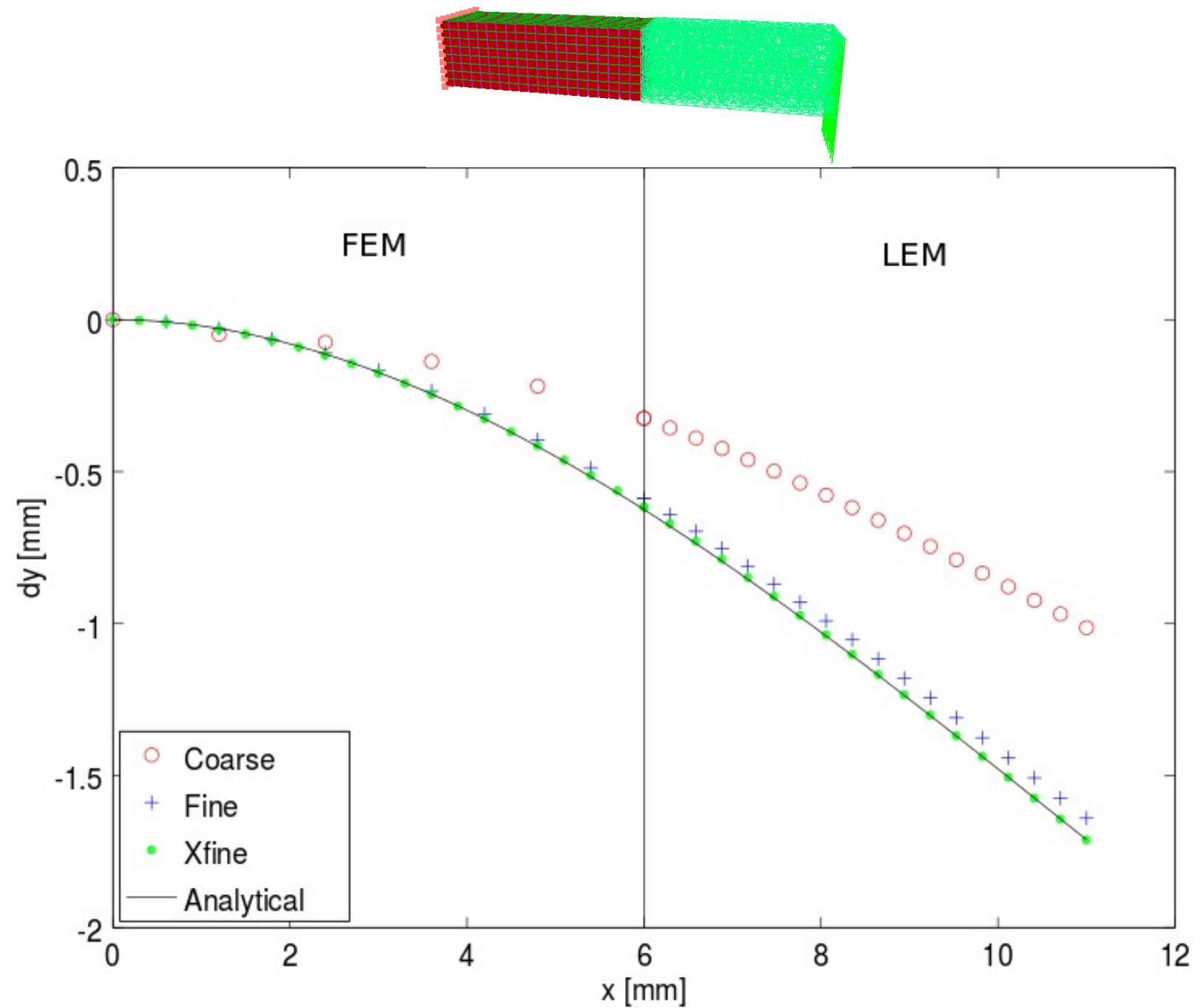
$$v(x) = \frac{-Fx^2}{6EI}(3L - x)$$



Bending test: FEM approach

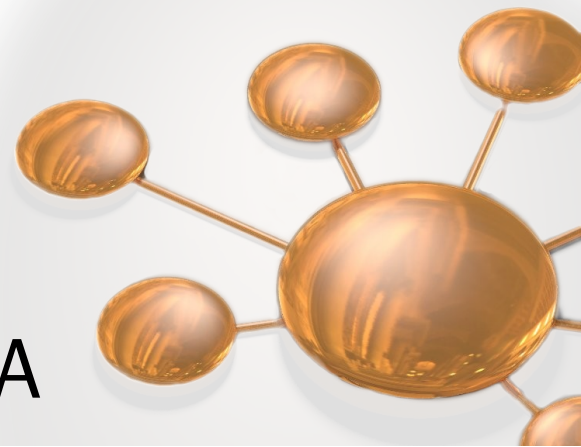
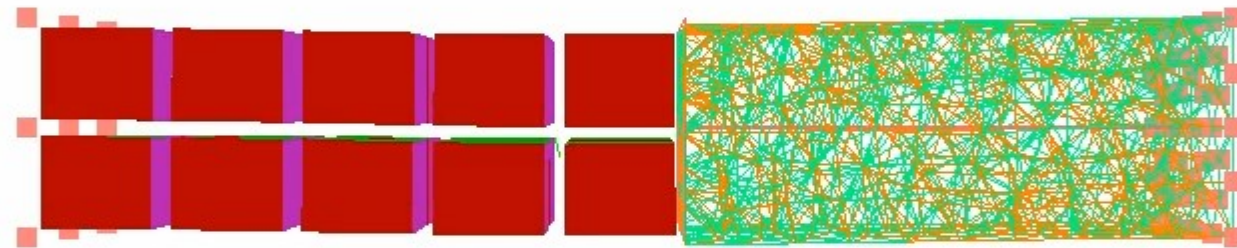


Bending test: FEM-LEM approach

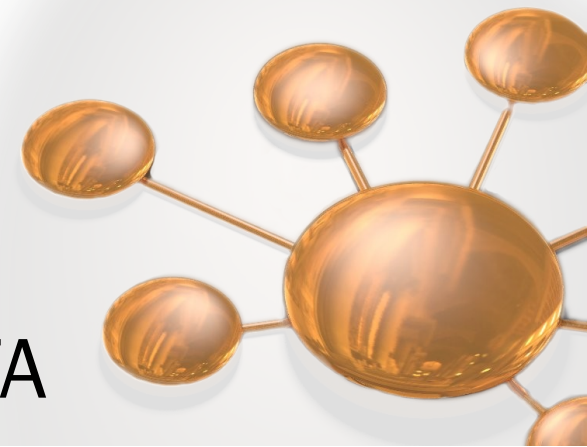
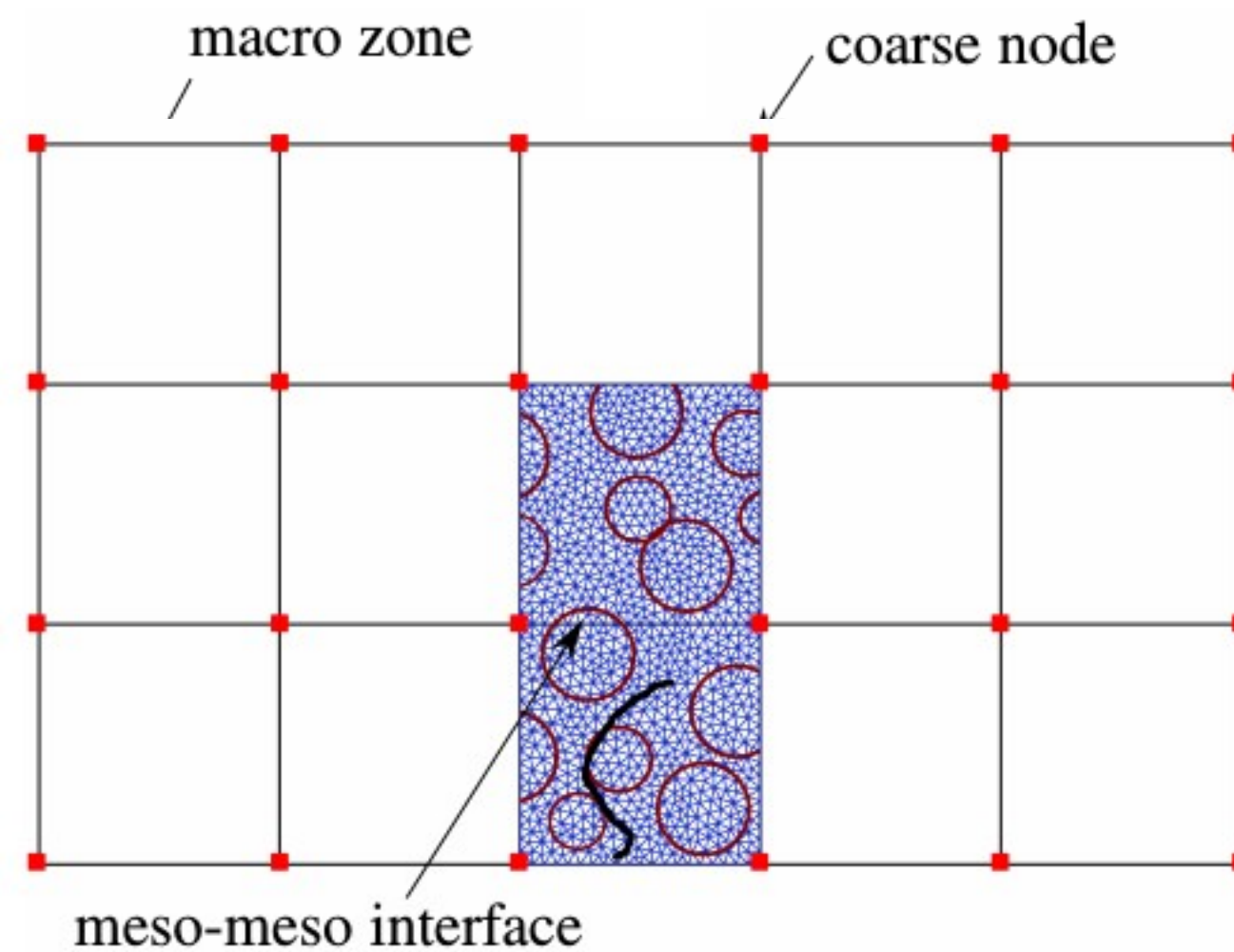


Fracture application

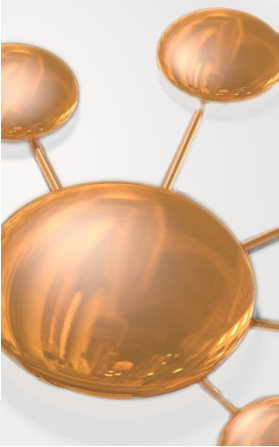
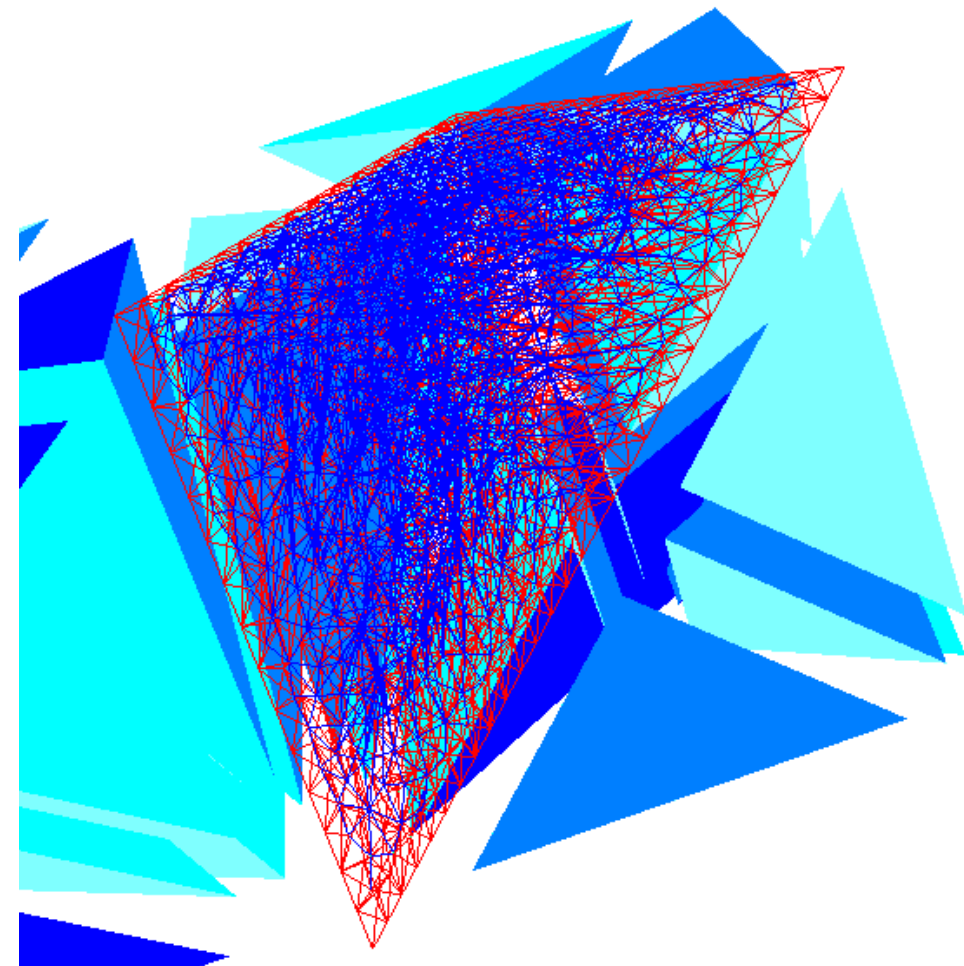
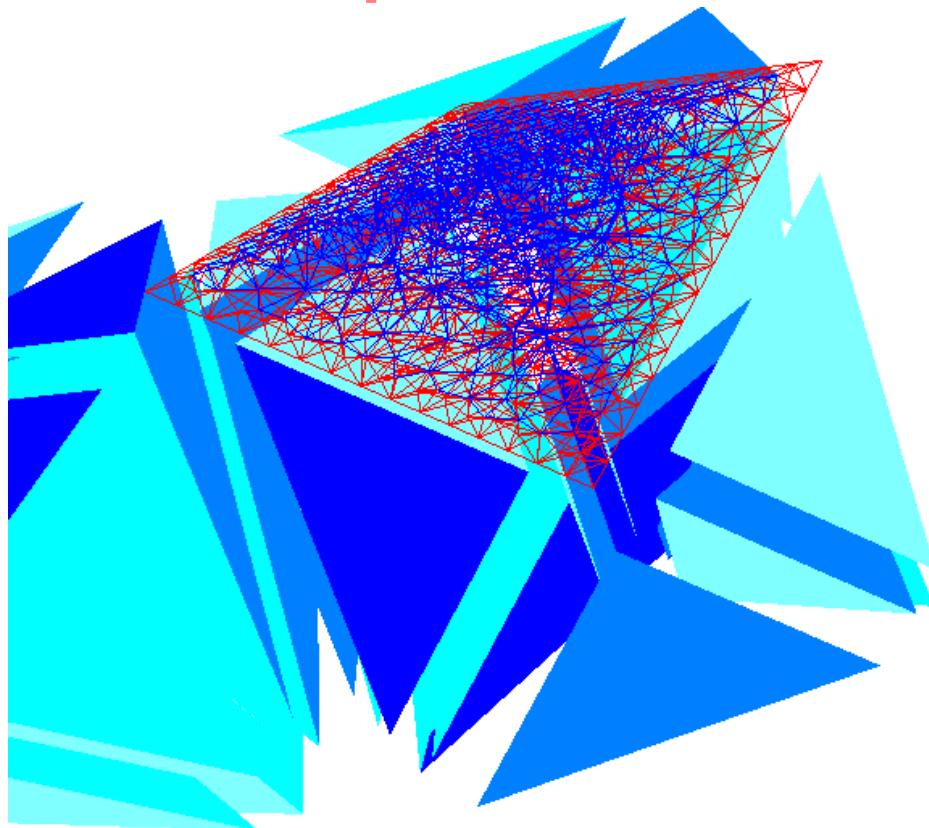
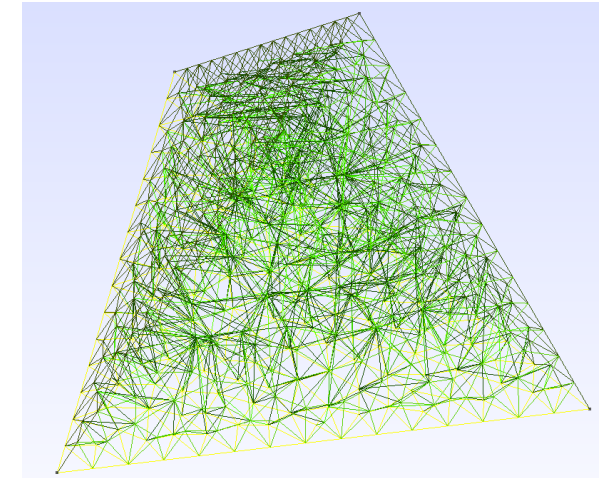
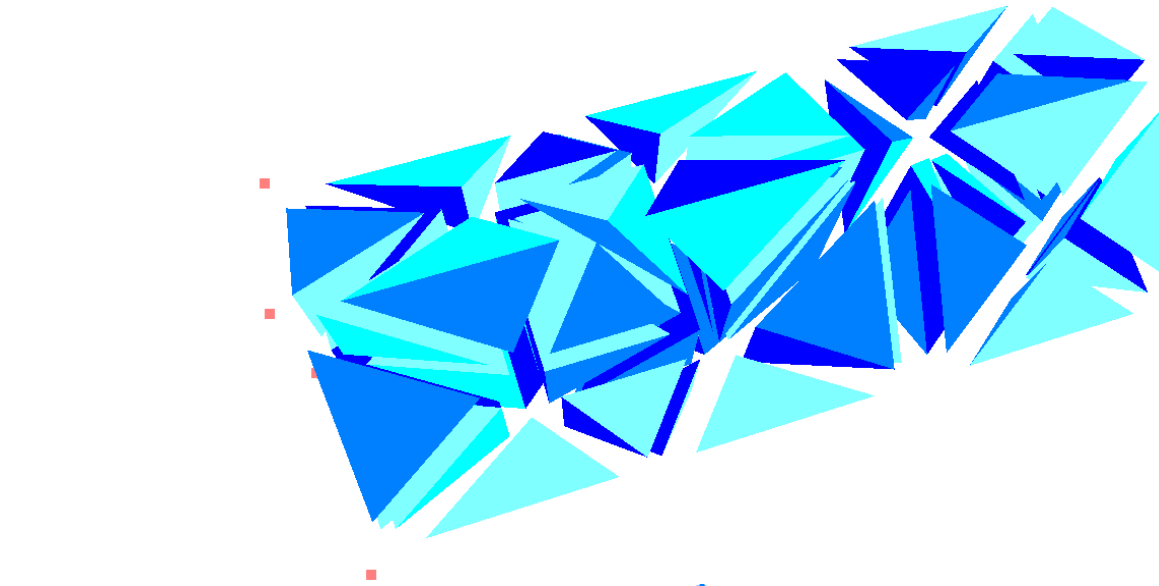
Failure due to tearing



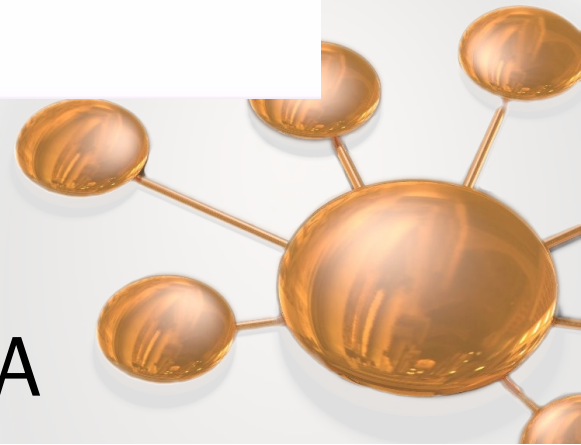
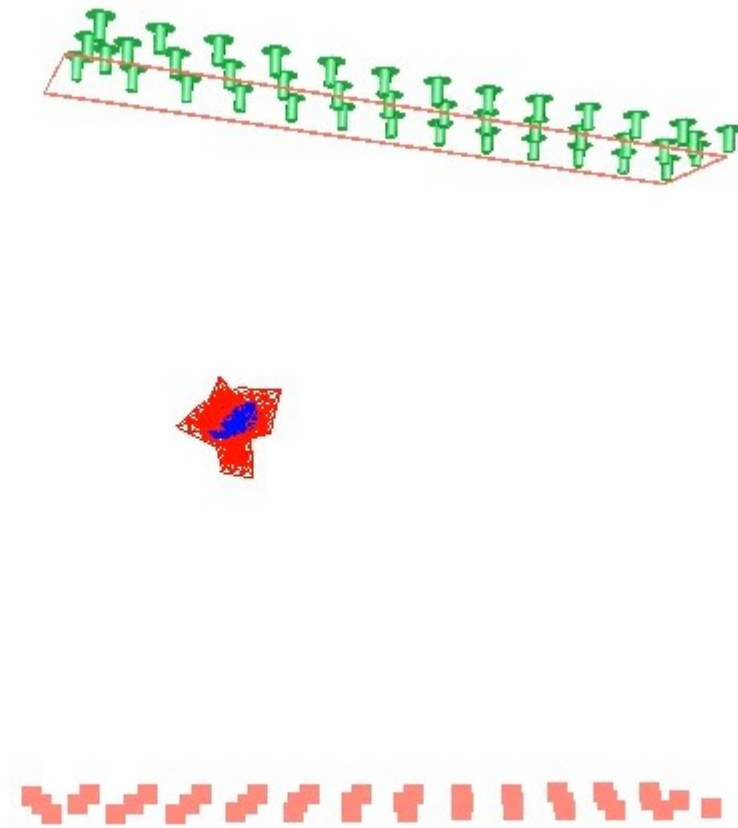
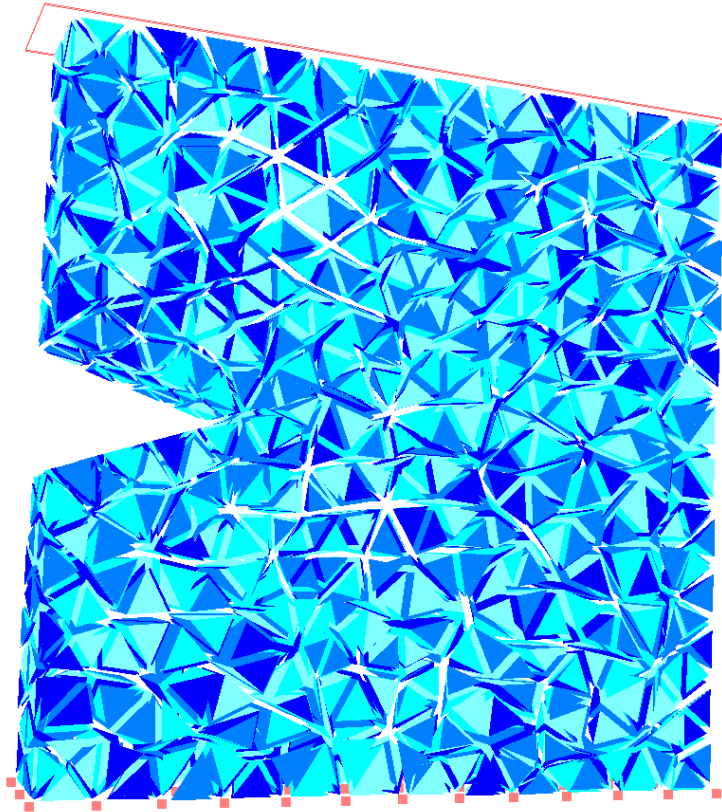
Dynamically Topological Changes



Dynamically Topological Changes



Dynamically Topological Changes



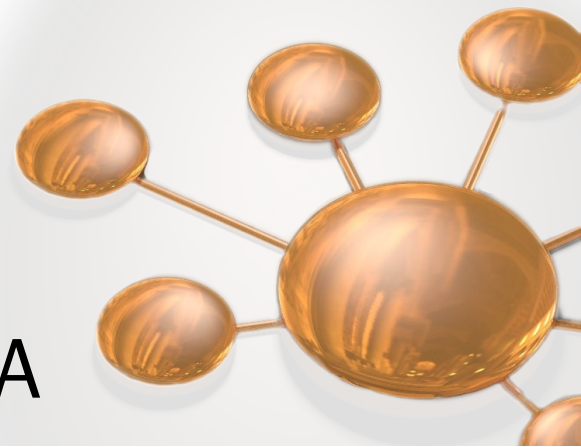
Conclusions & Perspectives

Conclusions

- ☺ Continuum-lattice coupling is verified
- ☺ Fracture simulation

Perspectives

- ☹ Cutting of soft tissue
- ☹ Implementation on GPUs



Thank you for your attention!

