

Sensing-Throughput Tradeoff for Cognitive Radio Systems with Unknown Received Power

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Abstract. Understanding the performance of the cognitive radio systems is of great interest. Different paradigms have been extensively analyzed in the literature to perform secondary access to the licensed spectrum. Of these, Interweave System (IS) has been widely investigated for performance analysis. According to IS, sensing is employed at the Secondary Transmitter (ST) that protects the Primary Receiver (PR) from the interference induced. Thus, in order to control the interference at the PR, it is required to sustain a certain level of probability of detection. In this regard, ST requires the knowledge of the received power. However, in practice, this knowledge is not available at the ST. Thereby performing analysis considering the prior knowledge of the received power is too idealistic, thus, do not depict the actual performance of the IS. Motivated by this fact, an estimation model that includes received power estimation is proposed. Considering a sensing-throughput tradeoff, we apply this model to characterize the performance of the IS. Most importantly, the proposed model captures the estimation error to determine the distortion in the system performance. Based on analysis, it is illustrated that the ideal model overestimates the performance of the IS. Finally, it is shown that with an appropriate choice of the estimation time, the severity in distortion can be effectively regulated.

1 Introduction

For future wireless technologies, cognitive radio communication is emerging as a possible solution to the problem of spectrum scarcity. The available cognitive radio paradigms in the literature can be categorized into interweave, underlay and overlay [1]. In Interweave Systems (IS), the Secondary Users (SUs) utilize the licensed spectrum opportunistically by exploiting spectral holes in different domains such as time, frequency, space and polarization, whereas in Underlay Systems (US), SUs are allowed to use the primary spectrum as long as they respect the interference constraints of the Primary Receivers (PRs). On the other hand, Overlay Systems (OS) allow the spectral coexistence of two or more wireless networks by employing advanced transmission and coding strategies.

Due to its ease in deployment, IS is mostly preferred for performing analysis among these paradigms. In this context, this paper focuses on the performance analysis of the ISs considering a hardware deployment where sensing is employed at the Secondary Transmitter (ST).

1.1 Motivation

Sensing is an integral part of the IS. At the ST, sensing is necessary for detecting the presence and absence of a primary signal, thereby protecting the PRs against harmful interference. Sensing at the ST is accomplished by listening to the transmission from the PT. For detecting a primary signal, several techniques such as Energy Detection (ED), matched filtering, cyclostationary and feature-based detection exist [2, 3]. Because of its versatility towards unknown primary signals, ED has been extensively investigated in the literature [4, 5, 6, 7, 8]. According to ED, the decision is accomplished by comparing the power received at the ST to a threshold. In reality, the ST encounters a variation in the received power due to the thermal noise at the receiver and fading in the channel. This leads to sensing errors described as misdetection or false alarm. The characterization of sensing errors as probability of detection and probability of false alarm has been studied in [9]. These sensing errors limit the performance of the IS.

In particular, probability of detection is critical for the primary system because it precludes the PR from the interference induced by the ST. On the other side, probability of false alarm accounts for the throughput attained by the secondary system at the Secondary Receiver (SR). In this regard, ST has to sustain a desired probability of detection and optimize its throughput. This phenomenon is characterized as a sensing-throughput tradeoff by Liang *et al.* [10]. According to it, the ST is able to determine a suitable sensing time that achieves an optimum throughput for a given received power. Several contributions have considered the performance of IS based on sensing errors [10, 11, 12]. However, the analysis described in the literature is too idealistic and not feasible for deployment, as it considers the perfect knowledge of the received power at the ST.

With the presence of channel and noise in the system, the received power is never known accurately, thus, needs to be estimated at the ST. Considering a hardware deployment, it is important to determine the performance of the IS based on received power estimation. A similar analysis is performed in [13], where the authors employ the received power estimation to control transmit power at the ST deployed as an underlay system. However, in this paper, we intend to capture the effect of estimation on the performance of an IS. Now, to realize received power estimation at the ST, it is necessary to allocate a certain time interval for the estimation within the frame duration. With the introduction of this estimation time, the system performance differs from its ideal behaviour. Additionally, the employed estimation process itself induces a certain level of error in the system. Hence, in order to understand the performance of the IS, it is necessary to consider the aforementioned aspects.

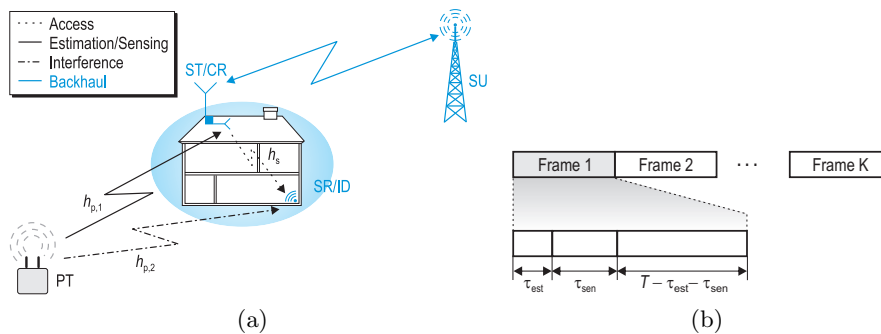


Fig. 1. (a) A scenario demonstrating the interweave paradigm. (b) Frame structure of interweave system with received power estimation.

1.2 Contributions

To realize the received power estimation, we consider a new frame structure. According to it, in a single frame, the ST performs (i) received power estimation, (ii) sensing, and (iii) data transmission. To perform analysis based on this new frame structure, we propose a novel estimation model. Most importantly, we evaluate the system performance with the inclusion of the estimation time and the errors occurred due to estimation. Based on the analytical expressions, we analyze the sensing-throughput tradeoff for the proposed estimation model. Finally, we determine the confidence intervals for the estimated received power. Particularly, based on these intervals, we capture the distortion in the performance based on the upper and lower bounds. This distortion, however, depends on the choice of design parameters depicted as probability of confidence and estimation duration.

1.3 Organization

The rest of the paper is organized as follows: Section 2 describes the system model that includes the interweave scenario and the signal model. Section 3 investigates the sensing-throughput tradeoff for the estimation model and derives upper and lower bounds for the performance parameters. Section 4 analyzes the numerical results based on the obtained expressions. Finally, Section 5 concludes the paper.

2 System Model

2.1 Interweave scenario

Cognitive Relay (CR) [14] characterizes a small cell deployment that fulfills the spectral requirements for indoor devices. Fig. 1a illustrates a snapshot of a CR scenario to depict the interaction between the CR with PT and indoor device, where CR and indoor device represent ST and SR, respectively. In [14], the challenges involved while deploying the CR as an IS were presented. For

simplification, a constant false alarm rate was considered in the system model. Now, we extend the analysis to employ a constant detection rate.

The medium access for the IS is slotted, where the time axis is segmented into frames of length T . The frame structure is analog to the one illustrated in [10]. However, unlike [10], the proposed frame structure uses τ_{est} to estimate and τ_{sen} to sense the received power, where $\tau_{\text{est}}, \tau_{\text{sen}}$ correspond to time intervals and $\tau_{\text{est}} + \tau_{\text{sen}} < T$, cf. Fig. 1b. To incorporate the effect of fading in the model, we assume that the channel remains constant for T . Hence, characterized by the fading process, each frame witnesses a different received power. Therefore, to sustain a desired probability of detection, it is important to perform estimation τ_{est} followed by sensing τ_{sen} for each frame. The remaining time $T - (\tau_{\text{est}} + \tau_{\text{sen}})$ is utilized for data transmission.

2.2 Signal model

In the estimation and sensing phase, the received signal at the ST is sampled with a sampling frequency of f_s for given hypotheses, that depicts the presence (\mathcal{H}_1) and absence (\mathcal{H}_0) of the primary signal, is given by

$$y_{\text{rcvd}}[n] = \begin{cases} \sqrt{h_{p,1}} \cdot x_p[n] + w[n] & : \mathcal{H}_1 \\ w[n] & : \mathcal{H}_0, \end{cases} \quad (1)$$

where $x_p[n]$ corresponds to a discrete sample at the PT, $h_{p,1}$ represents the power gain for the channel and $w[n]$ is circularly symmetric Additive White Gaussian Noise (AWGN) at the ST. $x_p[n]$ is an i.i.d. (independent and identically distributed) random process. As the channel $h_{p,1}$ is independent to x_p and $w[n]$ is an i.i.d. Gaussian random process with zero mean and variance $\mathbb{E}[|w[n]|^2] = \sigma^2$, therefore, $y_{\text{rcvd}}[n]$ corresponds to an i.i.d. random process. The true received power is defined as

$$\bar{P}_{\text{rcvd}} = \mathbb{E}[|\sqrt{h_{p,1}} \cdot x_p[n]|^2]. \quad (2)$$

Based on (2), the received SNR at the ST is $\gamma_{\text{rcvd}} = \frac{\bar{P}_{\text{rcvd}}}{\sigma^2} - 1$.

Now, the data transmission at the ST is conditioned over the probability of detection (P_d). In this context, the received signal at the SR is given by

$$y_s[n] = \begin{cases} \sqrt{h_s} \cdot x_s[n] + \sqrt{h_{p,2}} \cdot x_p[n] + w[n] & : 1 - P_d \\ \sqrt{h_s} \cdot x_s[n] + w[n] & : P_d, \end{cases} \quad (3)$$

where $x_s[n]$ is an i.i.d. random process and corresponds to discrete signal transmitted by the ST. Further, h_s and $h_{p,2}$ represent the power gains for channel, cf. Fig. 1a. The received SNRs over the links ST-SR and PT-ST are $\gamma_s = \frac{\mathbb{E}[|\sqrt{h_s} \cdot x_s[n]|^2]}{\sigma^2}$ and $\gamma_p = \frac{\mathbb{E}[|\sqrt{h_{p,2}} \cdot x_p[n]|^2]}{\sigma^2}$.

In the estimation phase, the estimated power received at the ST is given as [4]

$$P_{\text{rcvd}} = \frac{1}{\tau_{\text{est}} f_s} \sum_n^{\tau_{\text{est}} f_s} |y_{\text{rcvd}}[n]|^2. \quad (4)$$

P_{rcvd} determined in (4) using $\tau_{\text{est}} f_s$ samples follows a non central chi-squared distribution [15]. Considering large number of samples, thereby following similar approach as in [9], we apply the central limit theorem to approximate the distribution for P_{rcvd} as Gaussian distribution

$$P_{\text{rcvd}} \sim \mathcal{N} \left(\bar{P}_{\text{rcvd}}, \frac{2}{\tau_{\text{est}} f_s} \bar{P}_{\text{rcvd}}^2 \right). \quad (5)$$

Following the estimation of the received power, the ST performs sensing for a duration of τ_{sen} , cf. Fig. 1b. The test statistics $T(\mathbf{y})$ at the ST is evaluated as

$$T(\mathbf{y}) = \frac{1}{\tau_{\text{sen}} f_s} \sum_n^{\tau_{\text{sen}} f_s} |y_{\text{rcvd}}[n]|^2 \underset{\mathcal{H}_0}{\overset{\mathcal{H}_1}{\geq}} \epsilon, \quad (6)$$

where ϵ is the threshold and \mathbf{y} is a vector with $\tau_{\text{sen}} f_s$ samples. The probability of detection P_d and the probability of false alarm P_{fa} corresponding to (6) are determined as [9]

$$P_d(\epsilon, \tau_{\text{sen}}, \bar{P}_{\text{rcvd}}) = \mathcal{Q} \left(\frac{\epsilon - \bar{P}_{\text{rcvd}}}{\sqrt{\frac{2}{\tau_{\text{sen}} f_s} \bar{P}_{\text{rcvd}}}} \right), \quad (7)$$

$$P_{\text{fa}}(\epsilon, \tau_{\text{sen}}) = \mathcal{Q} \left(\frac{\epsilon - \sigma^2}{\sqrt{\frac{2}{\tau_{\text{sen}} f_s} \sigma^2}} \right), \quad (8)$$

where $\mathcal{Q}(\cdot)$ represents the Q-function [16]. Subsequently, by sustaining the P_d above a certain desired level \bar{P}_d

$$P_d(\epsilon, \tau_{\text{sen}}, \bar{P}_{\text{rcvd}}) \geq \bar{P}_d, \quad (9)$$

the ST precludes the interference to the primary system. Consequently, an optimum performance is achieved when the ST operates at the desired level, i.e., $P_d = \bar{P}_d$. Hence, using (7) and (9), the threshold is evaluated as

$$\epsilon(\bar{P}_d, \tau_{\text{sen}}, \bar{P}_{\text{rcvd}}) = \left(\mathcal{Q}^{-1}(\bar{P}_d) \sqrt{\frac{2}{\tau_{\text{sen}} f_s}} + 1 \right) \bar{P}_{\text{rcvd}}. \quad (10)$$

2.3 Assumptions

As a preliminary step, for the proposed model, we consider only the estimation of \bar{P}_{rcvd} at the ST. Hence, in this paper, it is assumed that the ST acquires the perfect knowledge about γ_p and γ_s from the SR over a feedback channel. The

inclusion of the imperfect knowledge of γ_p and γ_s in the proposed model poses an interesting research direction. Moreover, we consider that all transmitted signals are subjected to distance dependent path loss and the small scale fading gains. The coherence time for the channel gain is greater than the frame duration. However, we may still encounter scenarios where the coherence time exceeds the frame duration, in such cases our characterization depicts a lower performance bound. With no loss of generality, we consider that the channel gain ($h_{p,1}$, $h_{p,2}$ and h_s) includes the distance dependent path loss and the small scale gain. Finally, we target short term performance, according to which the performance parameters are optimized for each frame.

3 Sensing-Throughput analysis

3.1 Ideal Model (IM)

According to Liang *et al.* [10], the secondary throughput subject to a desired probability of detection \bar{P}_d is given by

$$\begin{aligned} \tilde{R}_s(\tilde{\tau}_{\text{sen}}) = \max_{\tau_{\text{sen}}} R_s(\tau_{\text{sen}}) = \frac{T - \tau_{\text{sen}}}{T} & \left[C_0(1 - P_{\text{fa}}(\epsilon, \tau_{\text{sen}}))P(\mathcal{H}_0) \right. \\ & \left. + C_1(1 - P_d(\epsilon, \tau_{\text{sen}}, \bar{P}_{\text{rcvd}}))P(\mathcal{H}_1) \right], \end{aligned} \quad (11)$$

$$\text{s.t. } P_d(\epsilon, \tau_{\text{sen}}, \bar{P}_{\text{rcvd}}) \geq \bar{P}_d,$$

$$\text{where } C_0 = \log_2(1 + \gamma_s) \text{ and } C_1 = \log_2 \left(1 + \frac{\gamma_s}{\gamma_p + 1} \right).$$

$P(\mathcal{H}_0)$ and $P(\mathcal{H}_1)$ are the probabilities of occurrence for the respective hypothesis. Based on (11), the ST is able to determine the suitable sensing time $\tau_{\text{sen}} = \tilde{\tau}_{\text{sen}}$ such that an optimum throughput $\tilde{R}_s(\tilde{\tau}_{\text{sen}})$ is achieved. According to (11), the performance parameters for the IM are defined as \tilde{R}_s , P_d and P_{fa} .

3.2 Estimation Model (EM)

The system described in [10] is good for performing analysis, however, to determine $\tilde{\tau}_{\text{sen}}$ at the ST requires the knowledge of the received power \bar{P}_{rcvd} . Considering a hardware deployment, this information is not available at the ST. Unless estimated, it is not possible to determine $\tilde{\tau}_{\text{sen}}$. According to the EM, the ST estimates the \bar{P}_{rcvd} for a duration of τ_{est} as P_{rcvd} and based on its value, the ST determines $\tilde{\tau}_{\text{sen}}$ for the given frame. The samples needed for estimation can be utilized for sensing as well. However, for analytical tractability, in the proposed model the estimation and sensing are considered to be disjoint in time. Now, with the introduction of τ_{est} , the actual performance of the IS deviates from its ideal performance. Moreover, the estimation itself causes distortion in the actual performance of the IS. As a part of the proposed model, these aspects are dealt in the following subsections.

3.3 Actual performance

With the introduction of the EM, we first characterize the performance of the IS. To realize this, it is considered that the ST perfectly estimates the P_{rcvd} , that is $P_{\text{rcvd}} = \bar{P}_{\text{rcvd}}$. In accordance with the proposed model, the sensing-throughput tradeoff with perfect estimation is determined as

$$\begin{aligned} \tilde{R}_s^{\text{P}}(\tilde{\tau}_{\text{sen}}^{\text{P}}) &= \max_{\tau_{\text{sen}}} R_s^{\text{P}}(\tau_{\text{sen}}) = \frac{T - (\tau_{\text{est}} + \tau_{\text{sen}})}{T} \left[C_0(1 - \text{P}_{\text{fa}}(\epsilon, \tau_{\text{sen}})) \right. \\ &\quad \left. \text{P}(\mathcal{H}_0) + C_1(1 - \text{P}_{\text{d}}(\epsilon, \tau_{\text{sen}}, \bar{P}_{\text{rcvd}}))\text{P}(\mathcal{H}_1) \right], \quad (12) \\ \text{s.t. } &\text{P}_{\text{d}}(\epsilon, \tau_{\text{sen}}, \bar{P}_{\text{rcvd}}) \geq \bar{P}_{\text{d}}. \end{aligned}$$

According to the (12), for a given \bar{P}_{d} and estimation of \bar{P}_{rcvd} in the interval τ_{est} , ST is able to determine the threshold as $\epsilon(\bar{P}_{\text{d}}, \tau_{\text{sen}}, \bar{P}_{\text{rcvd}})$. Finally, based on the new sensing-throughput tradeoff (12), ST evaluates the suitable sensing time as $\tau_{\text{sen}} = \tilde{\tau}_{\text{sen}}^{\text{P}}$ that achieves the optimum throughput \tilde{R}_s^{P} . However, $\tilde{\tau}_{\text{sen}} \neq \tilde{\tau}_{\text{sen}}^{\text{P}}$ due to the inclusion of the estimation time in the considered sensing-throughput tradeoff. According to the EM, the performance parameters that characterize the actual performance of the IS are \tilde{R}_s^{P} , $\text{P}_{\text{d}}^{\text{P}}$ and $\text{P}_{\text{fa}}^{\text{P}}$. Now, with the perfect estimation of P_{rcvd} , the constraint in (12) is sustained, hence, $\text{P}_{\text{d}} = \bar{P}_{\text{d}}$. However, with $\tilde{\tau}_{\text{sen}} \neq \tilde{\tau}_{\text{sen}}^{\text{P}}$, $\text{P}_{\text{fa}}^{\text{P}}$ and \tilde{R}_s^{P} witness a deviation from their ideal behaviour.

3.4 Distortion

Previously, we determined the effect of estimation time on the performance. In this section, we extend the analysis by considering the influence of estimation error on the system performance. In this context, based on (5), we characterize a confidence interval $[P_{\text{rcvd}}^{\text{L}}, P_{\text{rcvd}}^{\text{U}}]$ for a certain choice of probability of confidence P_{c} and τ_{est} as

$$P_{\text{rcvd}} = \begin{cases} P_{\text{rcvd}}^{\text{L}} = \left(\mathcal{Q}^{-1} \left(\frac{\text{P}_{\text{c}}+1}{2} \right) \sqrt{\frac{2}{\tau_{\text{est}} f_s} + 1} \right) \bar{P}_{\text{rcvd}} \\ P_{\text{rcvd}}^{\text{U}} = \left(\mathcal{Q}^{-1} \left(1 - \frac{\text{P}_{\text{c}}+1}{2} \right) \sqrt{\frac{2}{\tau_{\text{est}} f_s} + 1} \right) \bar{P}_{\text{rcvd}}, \end{cases} \quad (13)$$

where $\mathcal{Q}^{-1}(\cdot)$ is the inverse-Q function [16]. Hence, we utilize this confidence interval to depict the maximum estimation error in the estimated received power, thereby characterizing maximum distortion in the performance parameters $\text{P}_{\text{d}}^{\text{P}}$, $\text{P}_{\text{fa}}^{\text{P}}$ and \tilde{R}_s^{P} . For $\text{P}_{\text{c}} = 0.95$, the $P_{\text{rcvd}}^{\text{L}}$ and $P_{\text{rcvd}}^{\text{U}}$ are equivalent to the lower and upper bounds of the \bar{P}_{rcvd} .

This confidence interval further depicts the distortion in the system parameters ϵ and $\tilde{\tau}_{\text{sen}}^{\text{P}}$. Hence, as an intermediate step, we first characterize the distortion in terms of these system parameters. Subject to the received powers as $P_{\text{rcvd}}^{\text{L}}$ and $P_{\text{rcvd}}^{\text{U}}$, the expressions for the threshold are evaluated as

$$\epsilon^{\text{L}} = \epsilon(\bar{P}_{\text{d}}, \tau_{\text{sen}}, P_{\text{rcvd}}^{\text{L}}) \text{ and } \epsilon^{\text{U}} = \epsilon(\bar{P}_{\text{d}}, \tau_{\text{sen}}, P_{\text{rcvd}}^{\text{U}}). \quad (14)$$

Clearly, due to difference in received power estimated at the ST, the expressions in (14) differ from the one illustrated in (10). By inserting the thresholds ϵ^L and ϵ^U in (12), the suitable sensing times computed at the ST are represented as

$$\tilde{\tau}_{\text{sen}}^L \text{ and } \tilde{\tau}_{\text{sen}}^U. \quad (15)$$

As a result, (14) and (15) clearly illustrates the distortion in the system parameters. Now, as a final step, we characterize the distortion in the performance parameters in terms of the distorted system parameters and the true received power. Consequently, we represent the distortion in \tilde{R}_s^P , P_d^P and P_{fa}^P as a function of $(\tilde{\tau}_{\text{sen}}^L, \epsilon^L)$ and $(\tilde{\tau}_{\text{sen}}^U, \epsilon^U)$ subject to true received power, i.e., \bar{P}_{rcvd} .

Following the above discussion, the distortion in the P_d^P , in terms of upper and lower bounds, due to the inclusion of estimation error in the received power is determined as

$$P_d^P = \begin{cases} P_d^L = P_d(\epsilon^L, \tilde{\tau}_{\text{sen}}^L, \bar{P}_{\text{rcvd}}) \\ P_d^U = P_d(\epsilon^U, \tilde{\tau}_{\text{sen}}^U, \bar{P}_{\text{rcvd}}). \end{cases} \quad (16)$$

It is evident that the distortion in the P_d^P results in the violation of the regulatory constraint, c.f. (9). If this constraint is not sustained, it may result in harmful interference at the PR. Hence, using (16), we are able to characterize the situations where the IS may degrade the performance of the primary system.

On similar basis, the distortion in P_{fa}^P in terms of upper and lower bounds is depicted as

$$P_{fa}^P = \begin{cases} P_{fa}^L = P_{fa}(\epsilon^L, \tilde{\tau}_{\text{sen}}^L) \\ P_{fa}^U = P_{fa}(\epsilon^U, \tilde{\tau}_{\text{sen}}^U). \end{cases} \quad (17)$$

Finally, including the distortion in the probabilities P_d^P and P_{fa}^P from (16) and (17) and the system parameters $(\epsilon, \tilde{\tau}_{\text{sen}}^P)$, the distortion in the optimum throughput \tilde{R}_s^P in terms of upper and lower bounds is determined as

$$\tilde{R}_s^P = \begin{cases} \tilde{R}_s^L = \frac{T - (\tau_{\text{est}} + \tilde{\tau}_{\text{sen}}^L)}{T} \left[C_0(1 - P_{fa}(\epsilon^L, \tilde{\tau}_{\text{sen}}^L))P(\mathcal{H}_0) \right. \\ \left. + C_1(1 - P_d(\epsilon^L, \tilde{\tau}_{\text{sen}}^L, \bar{P}_{\text{rcvd}}))P(\mathcal{H}_1) \right] \\ \tilde{R}_s^U = \frac{T - (\tau_{\text{est}} + \tilde{\tau}_{\text{sen}}^U)}{T} \left[C_0(1 - P_{fa}(\epsilon^U, \tilde{\tau}_{\text{sen}}^U))P(\mathcal{H}_0) \right. \\ \left. + C_1(1 - P_d(\epsilon^U, \tilde{\tau}_{\text{sen}}^U, \bar{P}_{\text{rcvd}}))P(\mathcal{H}_1) \right]. \end{cases} \quad (18)$$

Based on the expressions (16), (17) and (18) characterized by the EM, it is possible to depict the maximum distortion for the IS from its actual performance. Moreover, the severity in distortion can be controlled through P_c and τ_{est} . In particular, it is important to select τ_{est} appropriately such that the distortion in the performance doesn't exceed beyond a certain level. This aspect is investigated more deeply in the next section.

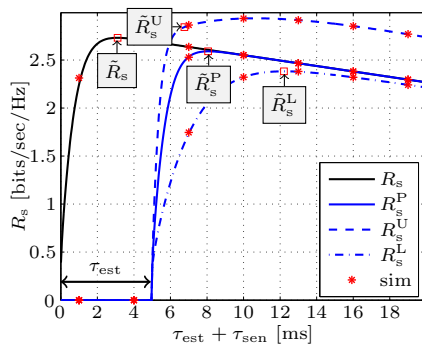


Fig. 2. Sensing-throughput tradeoff for the ideal and estimation models with $\gamma_{\text{rcvd}} = -10$ dB and $\tau_{\text{est}} = 5$ ms.

4 Numerical Analysis

In this section, the performance of the IS for the EM is analyzed. In this regard, we perform simulations to: (i) validate the expressions obtained in Section 3, (ii) provide a mathematical justification to the Gaussian approximation considered in Section 2. Although, the expressions derived using our sensing-throughput analysis are general and applicable to all cognitive radio systems, however, the parameters are selected in such a way that they closely relate to the deployment scenario described in Fig. 1a. Unless stated explicitly, the following choice of the parameters is considered for the analysis, $f_s = 1$ MHz, $h_{p,1} = h_{p,2} = -100$ dB, $h_s = -80$ dB, $T = 100$ ms, $P_c = 0.95$, $P_d = 0.9$, $\sigma^2 = -100$ dBm, $\gamma_{\text{rcvd}} = -10$ dB, $\gamma_p = -10$ dB, $\gamma_s = 10$ dB and $P(\mathcal{H}_1) = 1 - P(\mathcal{H}_0) = 0.2$, $\tau_{\text{est}} = 5$ ms.

Firstly, the analysis in terms of sensing-throughput tradeoff based on (11) and (12) for the IM and the EM is performed. The curves R_s and R_s^P in Fig. 2 depict the throughput based on the IM and the EM (actual performance) at the ST. Due to the inclusion of received power estimation in the frame structure, the ST produces no throughput at the SR for the interval τ_{est} . The sensing times $\tilde{\tau}_{\text{sen}} = 3.11$ ms and $\tilde{\tau}_{\text{sen}}^P = 3.06$ ms are evaluated, which yield the optimum throughputs as $\tilde{R}_s = 2.73$ bits/sec/Hz and $\tilde{R}_s^P = 2.59$ bits/sec/Hz, cf. Fig. 2. This variation is due the inclusion of τ_{est} in the sensing-throughput analysis. Hence, for the given choice of τ_{est} at ST, the ideal model overestimates the optimum throughput by $\approx 5\%$.

Next, sensing-throughput analysis is performed, considering that the \bar{P}_{rcvd} is estimated as P_{rcvd}^L or P_{rcvd}^U at ST. $\gamma_{\text{rcvd}} = -10$ dBm corresponds to $\bar{P}_{\text{rcvd}} = 1.10 \cdot 10^{-10}$ mW. With $P_c = 0.95$ and $\tau_{\text{est}} = 5$ ms, the confidence intervals are determined as $P_{\text{rcvd}}^L = 1.05 \cdot 10^{-10}$ mW and $P_{\text{rcvd}}^U = 1.14 \cdot 10^{-10}$ mW, cf. (13). Fig. 2 demonstrates the throughput corresponding to distorted system parameter ϵ^L and ϵ^U , cf. (14). The suitable sensing times are evaluated as $\tilde{\tau}_{\text{sen}}^L = 7.21$ ms and $\tilde{\tau}_{\text{sen}}^U = 1.76$ ms. Finally, the distortion in the \tilde{R}_s^P corresponding to the distortion in the system parameters is demonstrated. According to (18), the lower bound and upper bound on the optimum throughput \tilde{R}_s^P are determined as

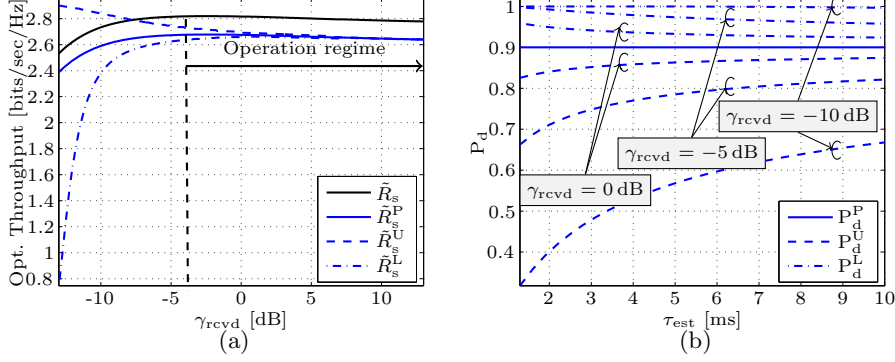


Fig. 3. (a) Distortion in optimum throughput versus the γ_{rcvd} with $P_c = 0.95$ and $\tau_{est} = 5$ ms. (b) Distortion in probability of detection versus the estimation time for different $\gamma_{rcvd} = \{-10, -5, 0\}$ dB.

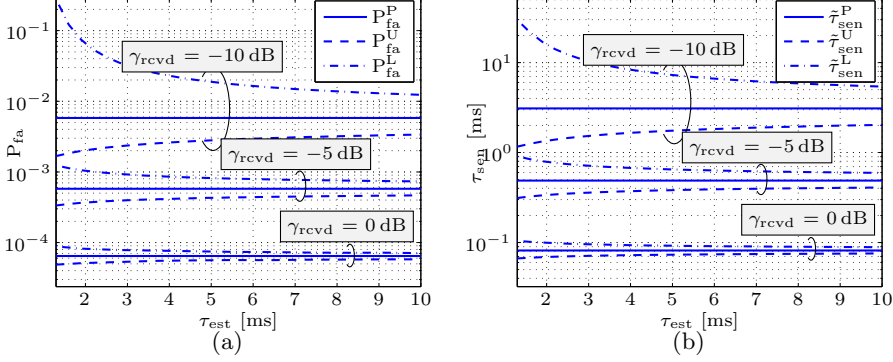


Fig. 4. (a) Distortion in probability of false versus the estimation time for different $\gamma_{rcvd} \in \{-10, -5, 0\}$ dB. (b) Distortion in optimum sensing time versus the estimation time for different $\gamma_{rcvd} \in \{-10, -5, 0\}$ dB.

$\tilde{R}_s^L = 2.38$ bits/sec/Hz and $\tilde{R}_s^U = 2.84$ bits/sec/Hz. It corresponds to 8.10% underestimation and 9.65% overestimation of the actual performance (\tilde{R}_s^P). Therefore, based on the analytical expressions determined under EM, it is possible to determine the severity of distortion in the system performance.

Hereafter, for the analysis, we consider the theoretical expressions and choose to operate at suitable sensing time. Next, we determine the variation of the optimum throughput against the $\gamma_{rcvd} \in [-13, 10]$ dB at ST with $\tau_{est} = 5$ ms. It is evident from Fig. 3a that the distortion in the \tilde{R}_s^P decreases with increase in γ_{rcvd} . For $\gamma_{rcvd} > -5$ dB and $\tau_{est} = 5$ ms, the level of distortion is negligible. This is due to the fact that with increase in P_{rcvd} , P_{fa} shifts to a very low value such that $1 - P_{fa} \approx 1$. Moreover, for large γ_{rcvd} , the sensing-throughput curvature shifts to the right leading to a low $\tilde{\tau}_{sen}^P$, thereby making distortion in terms of $\tilde{\tau}_{sen}^L$, $\tilde{\tau}_{sen}^U$ insignificant. Hence, the system becomes more tolerant due to the reduced distortion in the system parameters. Besides that, by reducing τ_{est} ,

i.e., $\tau_{\text{est}} < 5$ ms, it is possible to minimize the margin between \tilde{R}_s and \tilde{R}_s^P , this however increases the level of distortion for IS. This way, for a given choice of τ_{est} and maximum distortion in the \tilde{R}_s^P , we can define an operation regime for IS in terms of γ_{rcvd} , for example operation regime with $\tau_{\text{est}} = 5$ ms is defined as $\gamma_{\text{rcvd}} \geq -5$ dB, cf. Fig. 3a. Hence, an extension of this regime below -5 dB can be attained by increasing the estimation time beyond 5 ms.

In addition to the \tilde{R}_s^P , it is also important to depict the distortion in P_d . The distortion in P_d^P is characterized using (16). Clearly, P_d^P remains constant, i.e., $P_d^P = \bar{P}_d$ with τ_{est} and for $\gamma_{\text{rcvd}} \in \{-10, -5, 0\}$ dB. Fig. 3b reveals the distortion in P_d^P in terms of P_d^L and P_d^U . It is evident that the distortion is small for a large value of γ_{rcvd} and it decreases with increase in τ_{est} . Most importantly, it is observed that an P_d^U depicted from P_{rcvd}^U forms a lower bound whereas P_d^L forms an upper bound to P_d^P . It is clear from the fact that, the distortion in $P_{\text{rcvd}} \leq P_{\text{rcvd}}^U$ shifts the threshold to its right side $\epsilon \geq \epsilon^U$, whereas the probability density function corresponds to hypothesis \mathcal{H}_1 has a fixed expression subject to \bar{P}_{rcvd} , hence, this shift in threshold causes the probability of detection to decrease, i.e., $P_d^U \leq P_d^P$. Similarly, $\epsilon^L \leq \epsilon$ corresponds to upper bound $P_d^P \leq P_d^L$.

From the perspective of the secondary user, it is interesting to depict the distortion in P_{fa}^P . Fig. 4a analyzes the distortion in P_{fa}^P according to (17) versus τ_{est} for $\gamma_{\text{rcvd}} = \{-10, -5, 0\}$ dB. Clearly, P_{fa}^P decreases with increase in γ_{rcvd} and remains constant with τ_{est} . Analog to P_d^P , $P_{\text{fa}}^U \leq P_{\text{fa}}^P \leq P_{\text{fa}}^L$, hence, P_{fa}^L and P_{fa}^U form an upper and lower bounds, respectively.

Apart from the performance parameters, the optimum sensing time $\tilde{\tau}_{\text{sen}}^P$ is an important system parameter that is closely related to the performance parameters. Hence, Fig. 4b reveals the distortion in the $\tilde{\tau}_{\text{sen}}^P$ versus the τ_{est} for $\gamma_{\text{rcvd}} \in \{-10, -5, 0\}$ dB, cf. (15). Similar to P_d^P and P_{fa}^P , $\tilde{\tau}_{\text{sen}}^L$ and $\tilde{\tau}_{\text{sen}}^U$ represent the upper and lower bound to $\tilde{\tau}_{\text{sen}}^P$. It is obvious from the fact that larger value of estimated received power P_{rcvd}^U shifts the curvature in the sensing-throughput, that depicts the optimum sensing time, to a lower value, therefore, $\tilde{\tau}_{\text{sen}}^U \leq \tilde{\tau}_{\text{sen}}^P \leq \tilde{\tau}_{\text{sen}}^L$, cf. Fig. 4b.

5 Conclusion

In this paper, we considered the deployment of a cognitive radio as an interweave system. For sustaining a minimum probability of detection, it requires the knowledge of the received power at the ST. To acquire this knowledge, an estimation has been included within the frame duration. In this regard, we proposed an estimation model that characterizes the actual performance of the IS. More specifically, the distortion in terms of bounds on the performance parameters has been captured based on the analytical expression. Moreover, it has been indicated that the severity in distortion can be confined by regulating the estimation time. Through theoretical and numerical analysis, it has been demonstrated that for a given choice of estimation time, the distortion in the performance parameters limits the operation regime, defined in terms of the received signal to noise ratio, at the ST.

In future, we plan to depict the exact expression of distortion instead of performance bounds. To pursue this, an outage constraint will be applied on the probability of detection in place of received power, that is $P(P_d \leq \bar{P}_d)$. In this way, we shall determine the estimation time subject to the new outage constraint.

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