

Real time surgical simulation using a lattice-continuum approach

Implementation and validation

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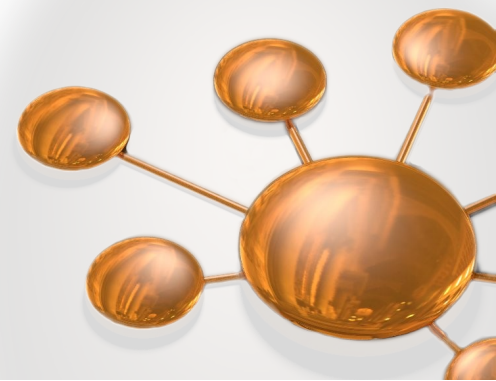
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³ Shacra, Inria

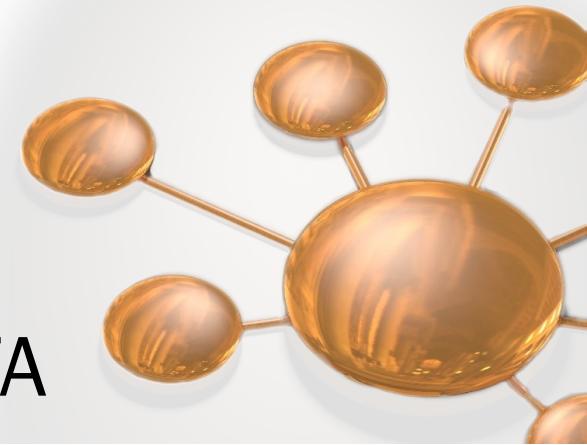
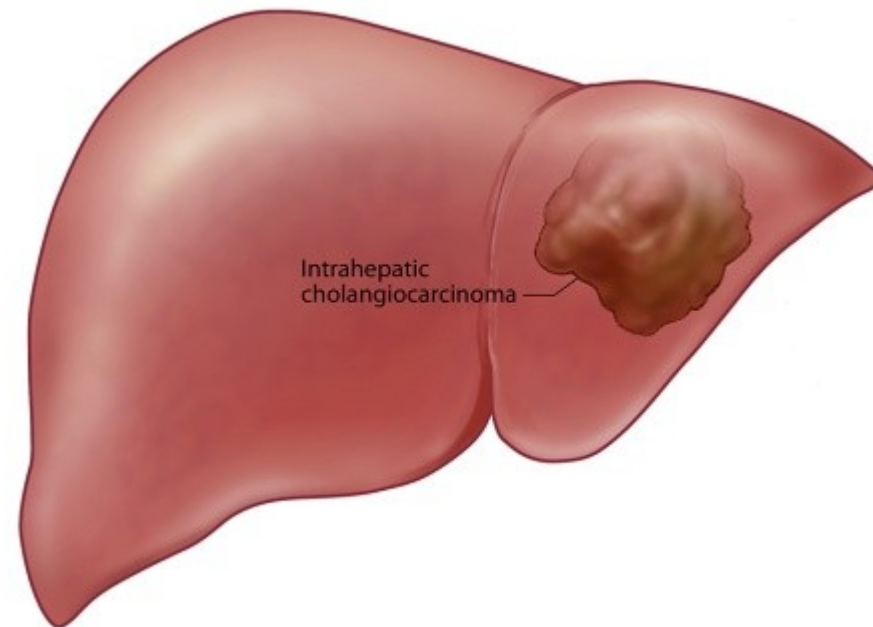


SOFA



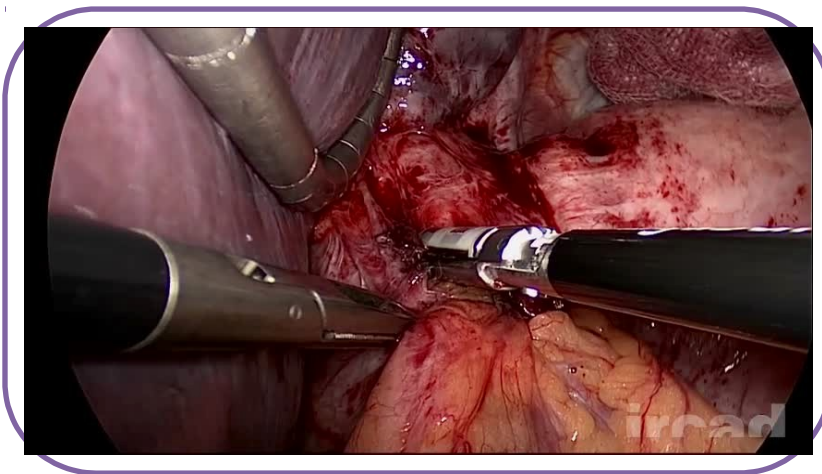
Some words about me

- ▶ PhD at University of Grenoble (November 2013)
Multiscale approach of concrete structure failure
- ▶ Postdoc at 3SR laboratory (2014)
Segmentation of cracks in concrete structure
- ▶ Arrived in Strasbourg (September 2014)

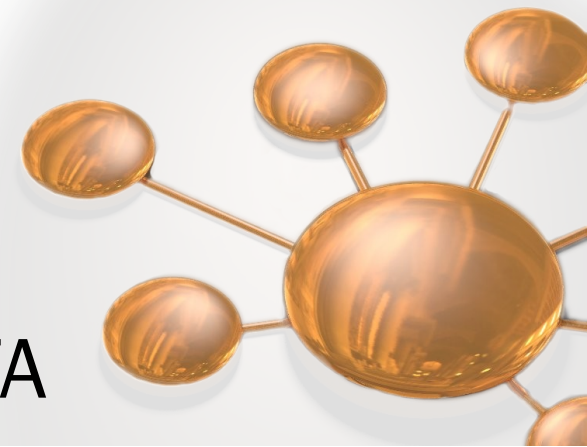


Context

- ▶ Surgery: complex practice
 - ▶ Experiences of surgeons
 - ▶ A number of risks



SOFA



Context

Courtecuisse *et al*, 2013

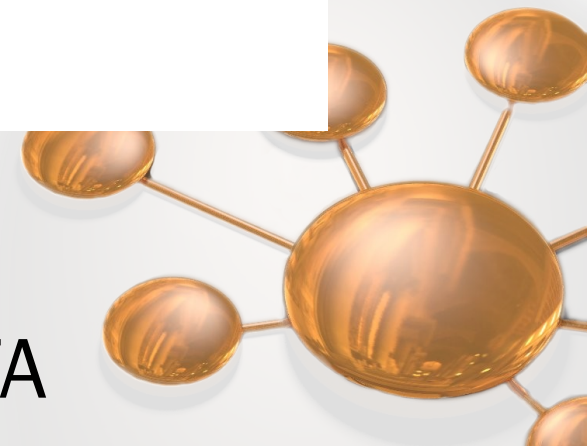
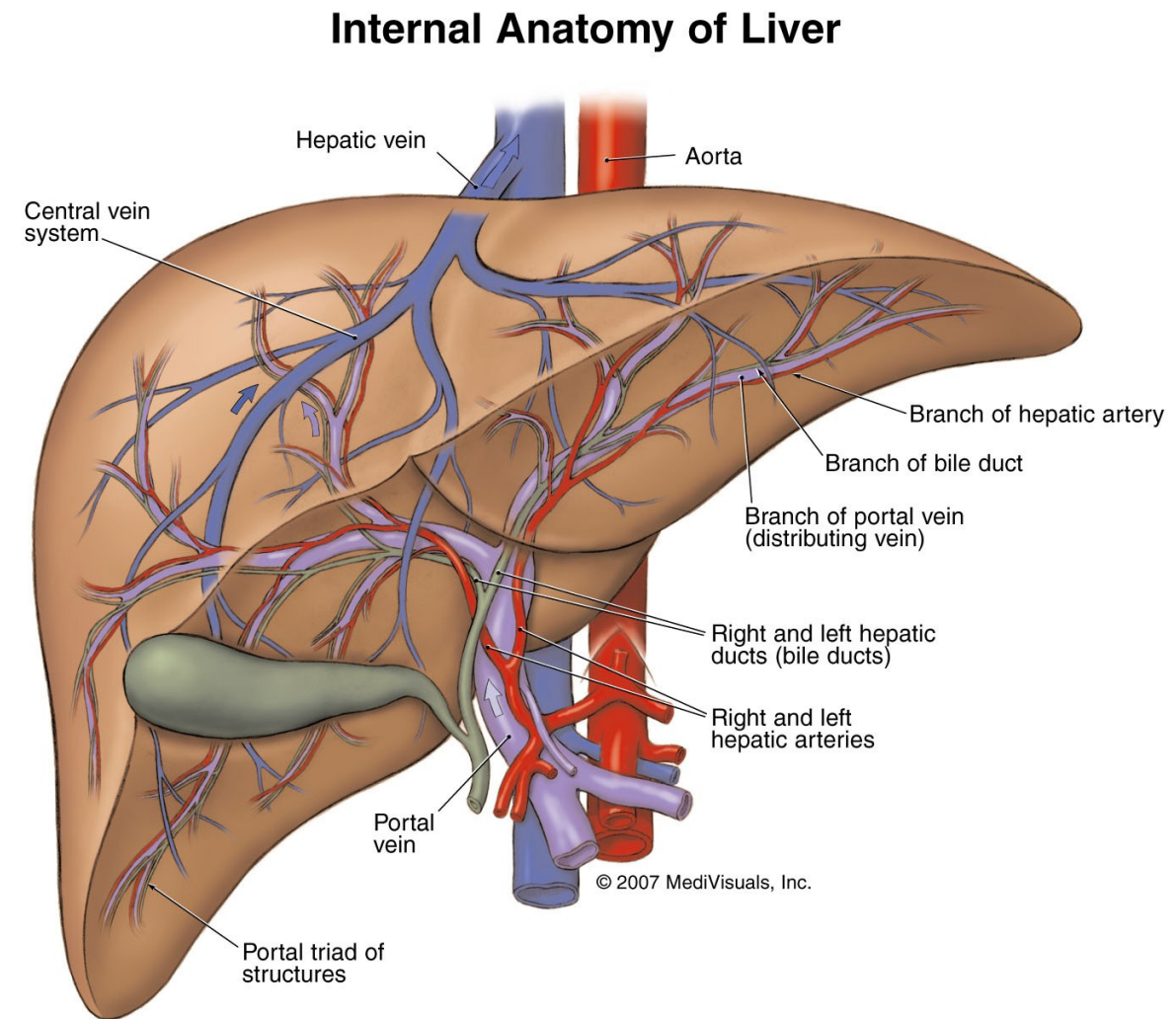
▶ Computer-based simulation

- ▶ Surgical training
- ▶ Guidance
- ▶ Surgical robotics

▶ **Challenges:** cutting, tearing, needle insertion, ...

- ▶ Topological changes
- ▶ Contacts

▶ **Microstructure** of the tissue (discontinuities, holes,)

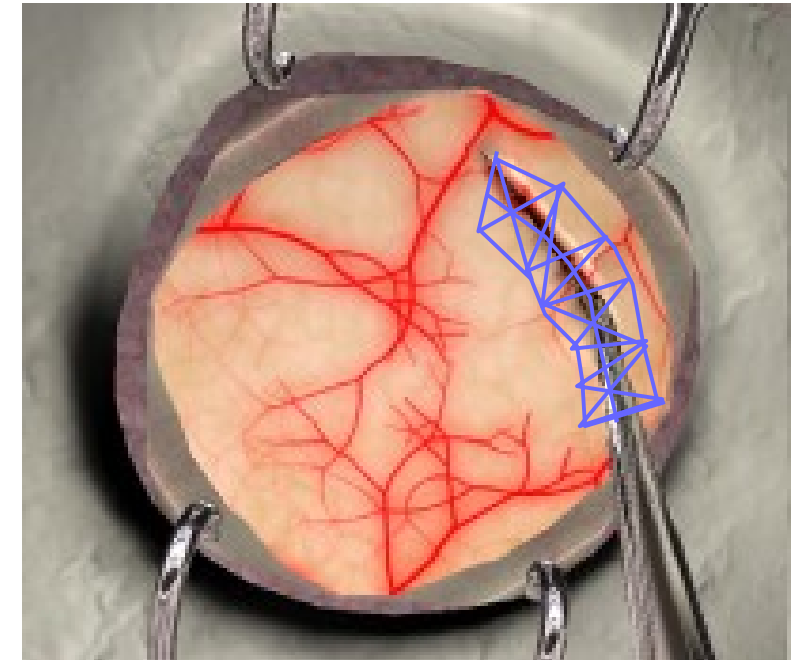


Objectives

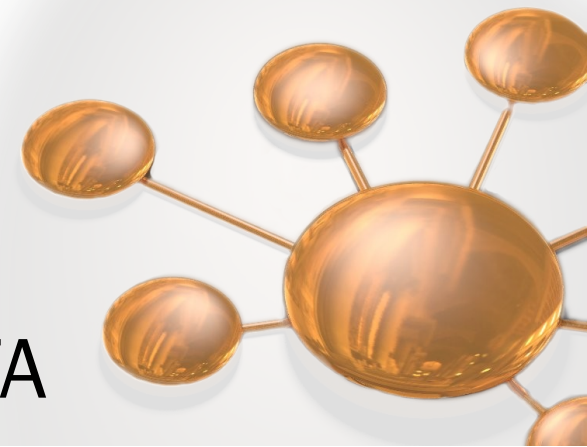
- ▶ Development of numerical tool
 - ▶ Real-time simulation
 - ▶ **Multi-domain**: continuum-lattice approach
 - ▶ **Multiscale**: macro, mesoscopic scale (material scale)

- ⇒
- ▲ Computational gains
 - ▲ Increase the quality of the cut

- ▶ The algorithm is implemented into SOFA framework

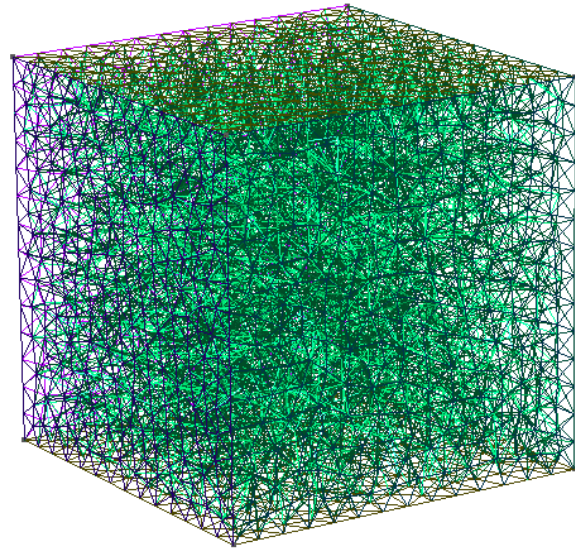


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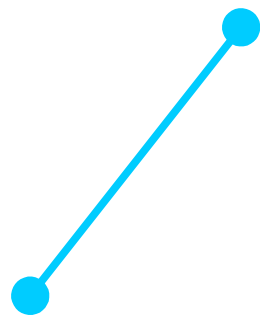
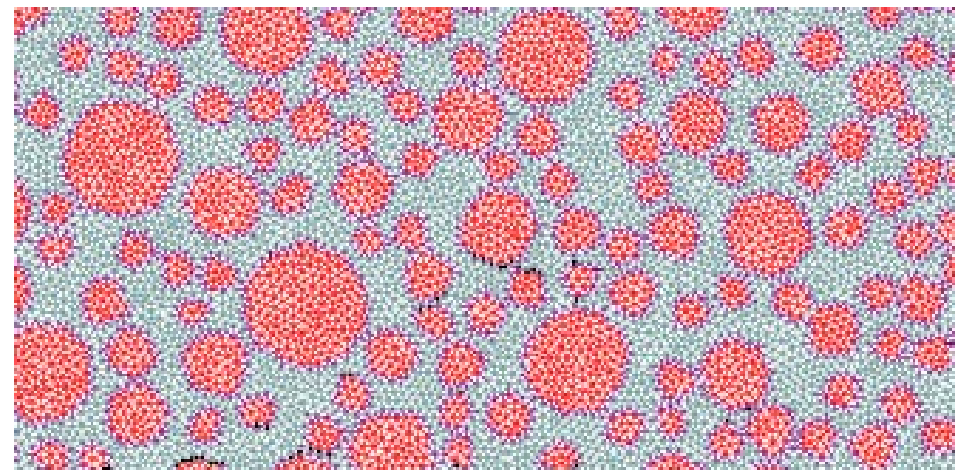


Lattice approach

- ▲ Discrete model: suitable for discontinuity problems
- ▲ Simplicity to incorporate fracture, cutting
- ▲ Modeling of material heterogeneity



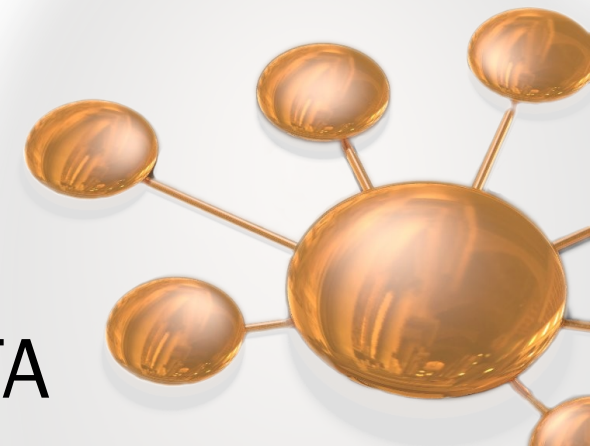
Discretization by 1D elements



○ Beam element

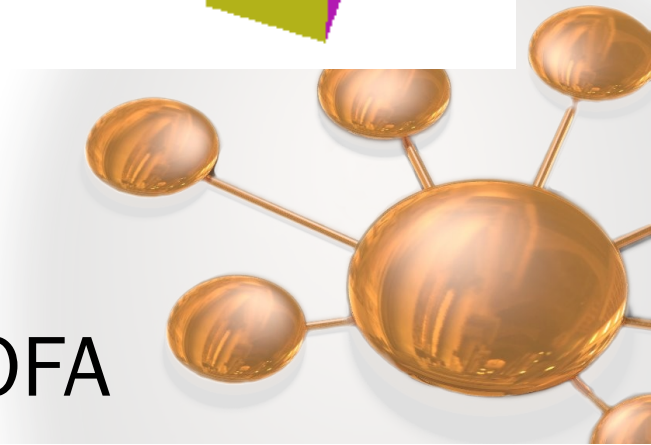
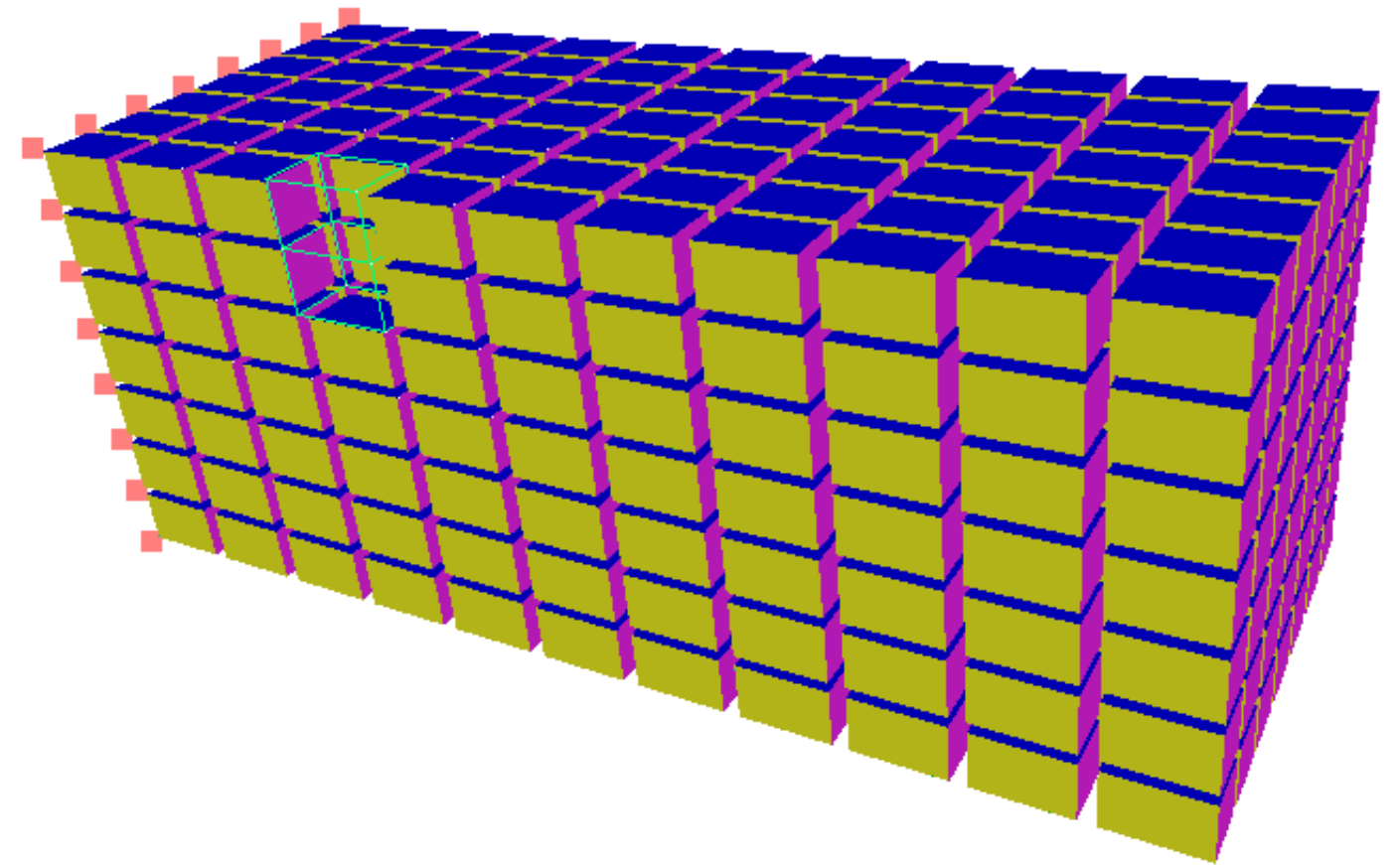
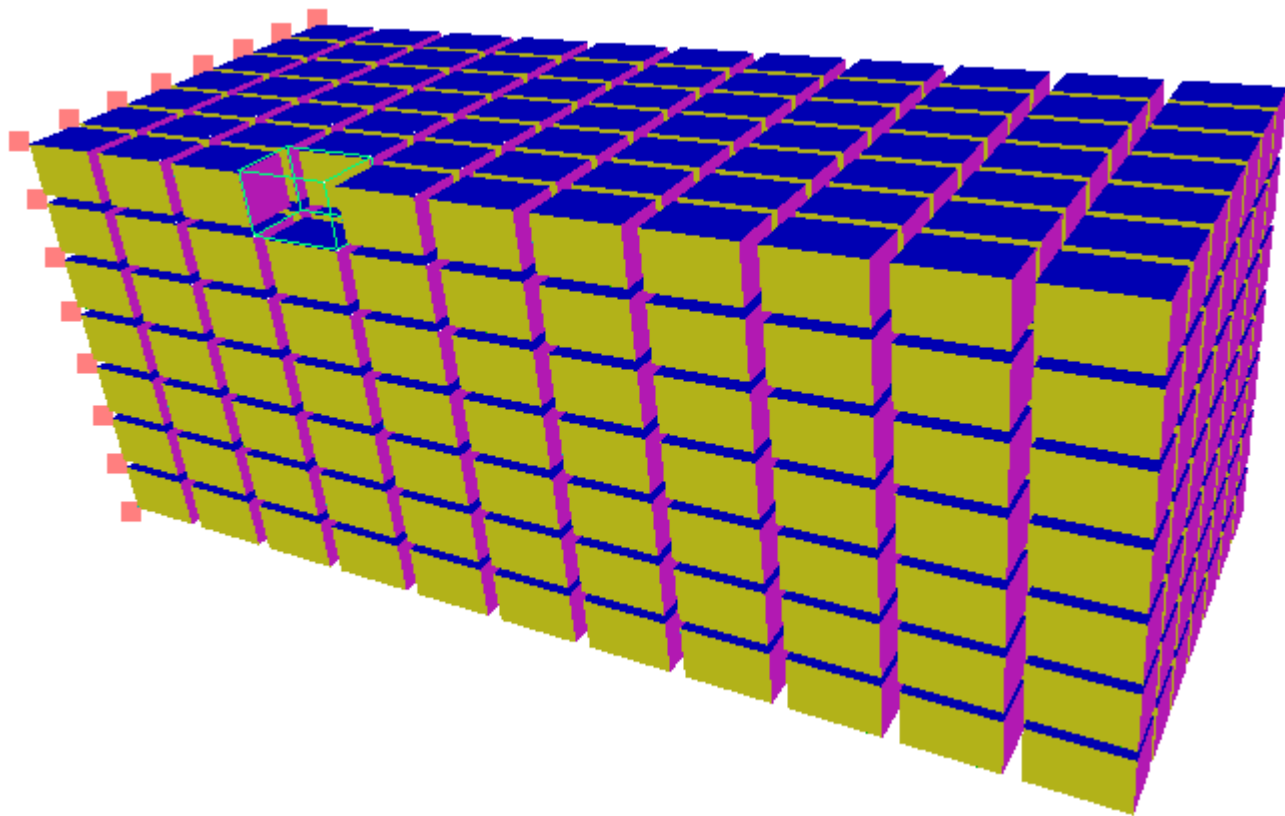
○ Truss element

▼ Computational cost

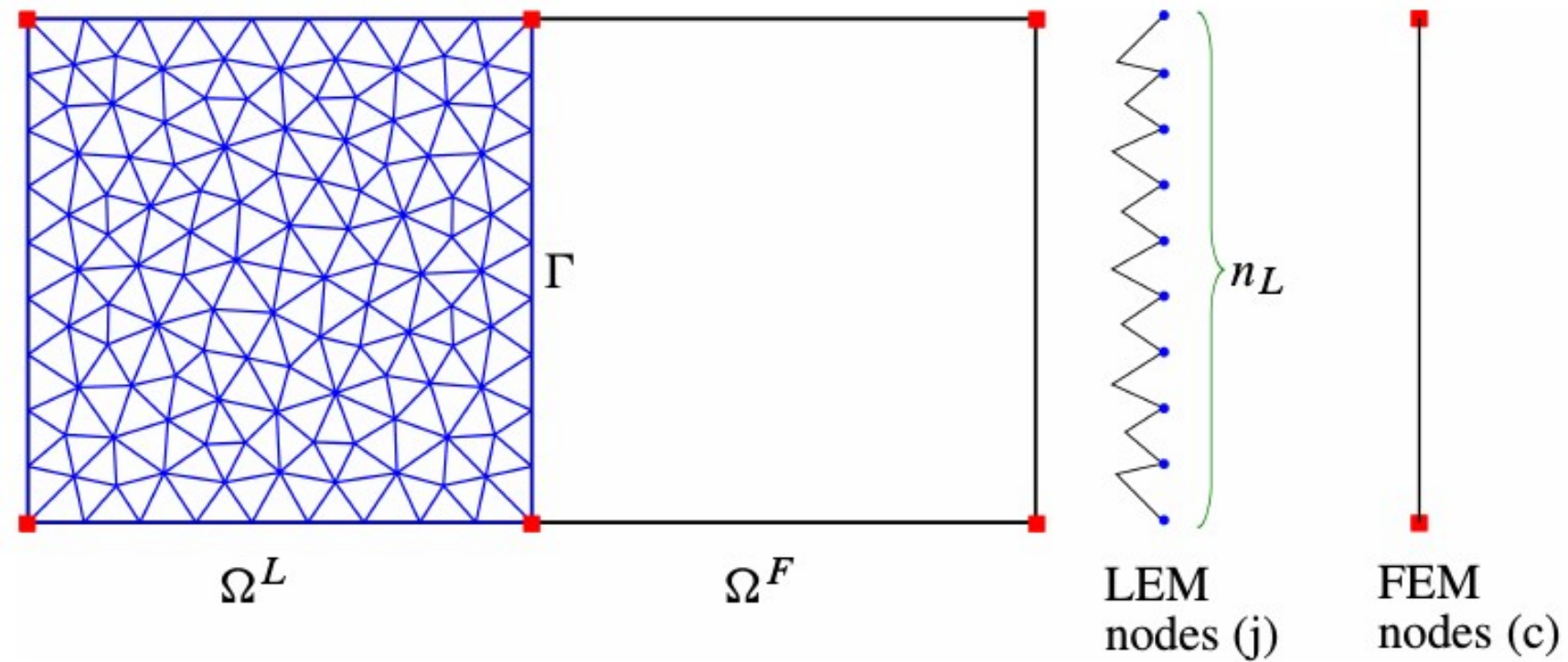


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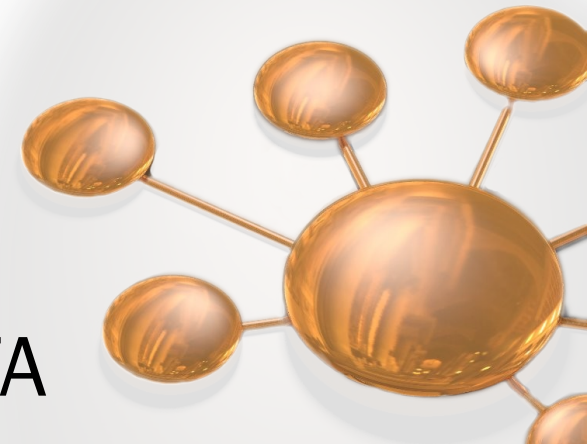
Continuum-lattice approach



Continuum-lattice approach



$$\mathbf{u}_j^L = \mathbf{N} \cdot \mathbf{u}_c^F = N_c(\mathbf{x}_j) \cdot u_c, \forall j = \{1, 2, \dots, n_L\}$$



Continuum-lattice approach

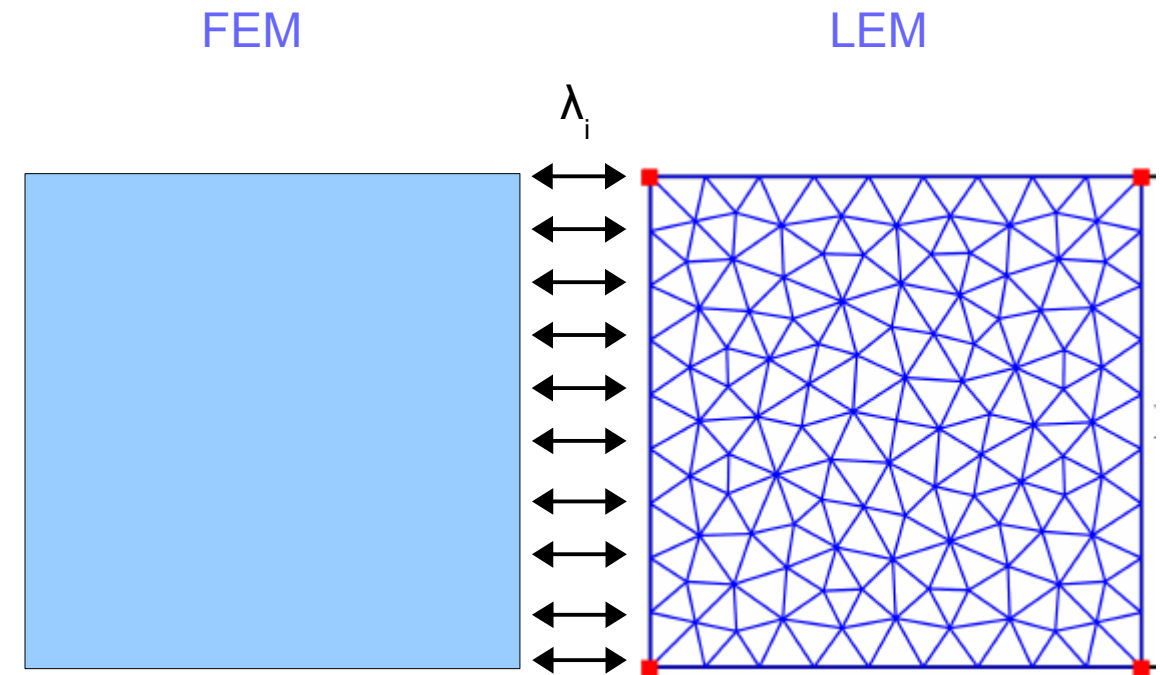
Constraint-based solution

Courtecuisse *et al*, 2013
Duriez *et al*, 2006

FEM $\mathbf{A}_1 \mathbf{x}_1 = \mathbf{b}_1 + h \mathbf{H}_1^T \lambda$

LEM $\mathbf{A}_2 \mathbf{x}_2 = \mathbf{b}_2 + h \mathbf{H}_2^T \lambda$

Interface With Lagrange multiplier λ such that $\mathbf{u}_j^L = \mathbf{N} \cdot \mathbf{u}_c^F$

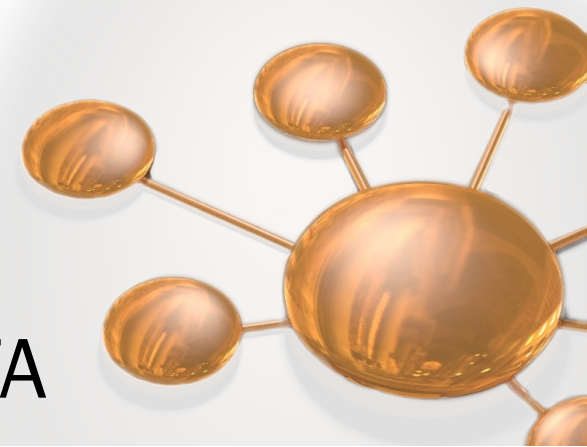


Step 1: Free motions $\mathbf{x}_1^{\text{free}}, \mathbf{x}_2^{\text{free}}$ $\mathbf{A} \mathbf{x} = \mathbf{b}$ with $\lambda = 0$

Step 2: Corrective motions $\mathbf{x}_1^{\text{cor}}, \mathbf{x}_2^{\text{cor}}$ $\mathbf{A} \mathbf{x} = h \mathbf{H} \lambda$ with $\mathbf{b} = 0$

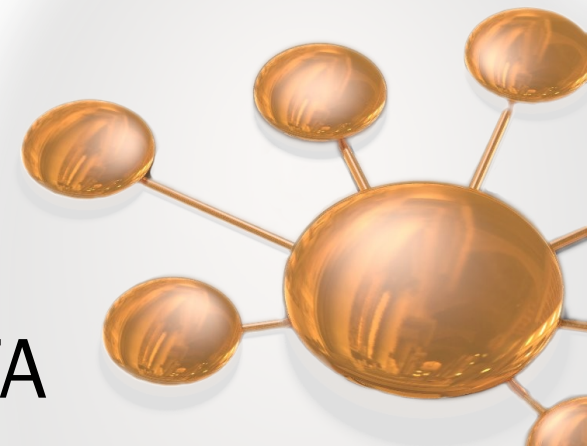
Step 3: Apply correction $\mathbf{x} = \mathbf{x}^{\text{free}} + \mathbf{x}^{\text{cor}}$

Asynchronous preconditioner
using sparse \mathbf{LDL}^T factorization

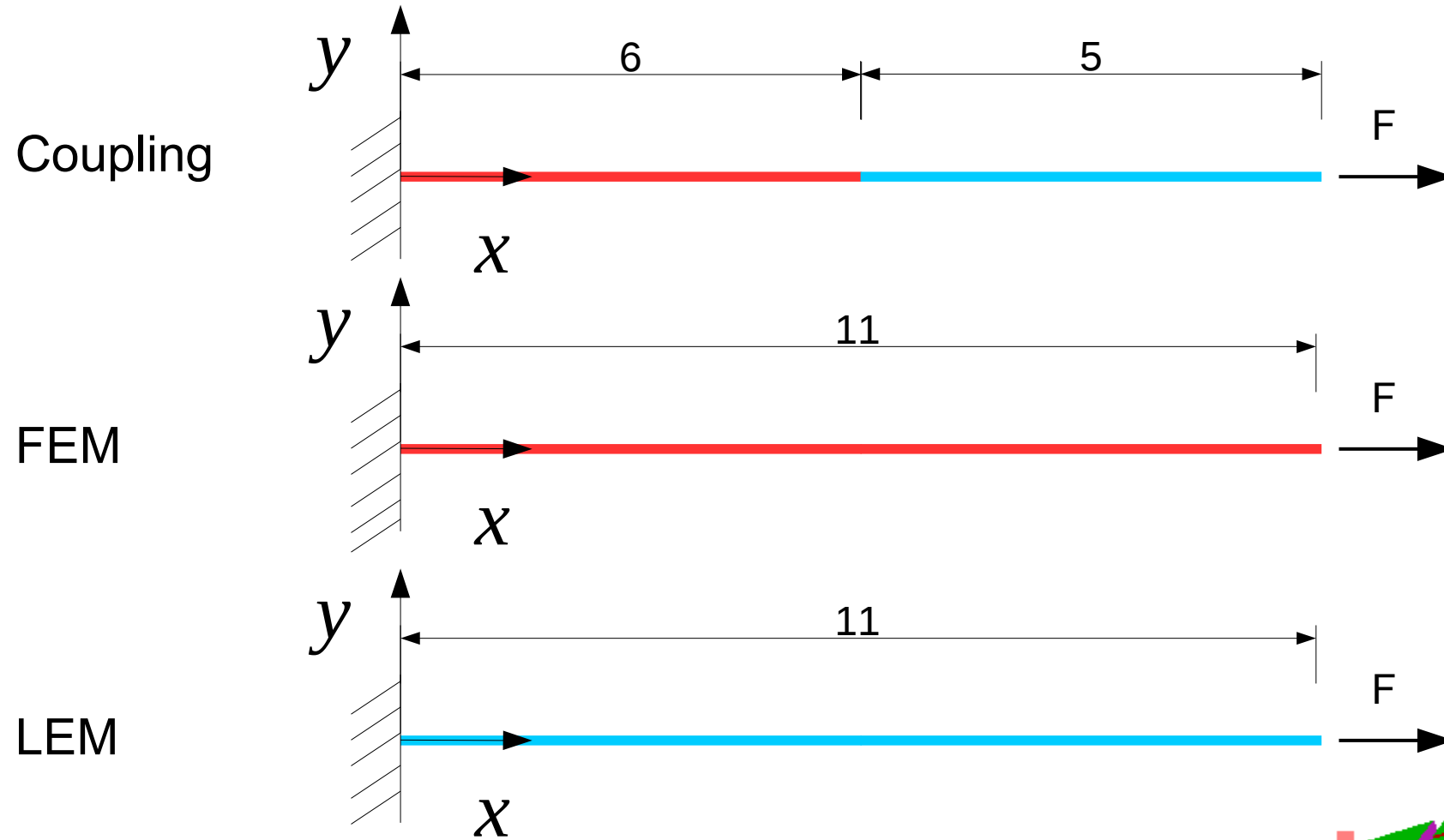


SOFA

Validation tests



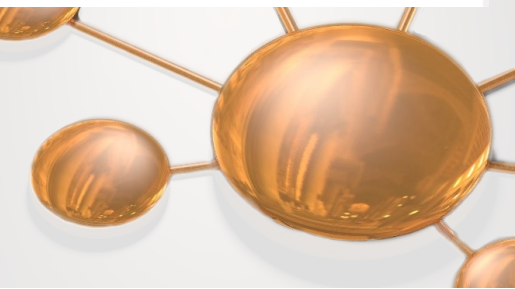
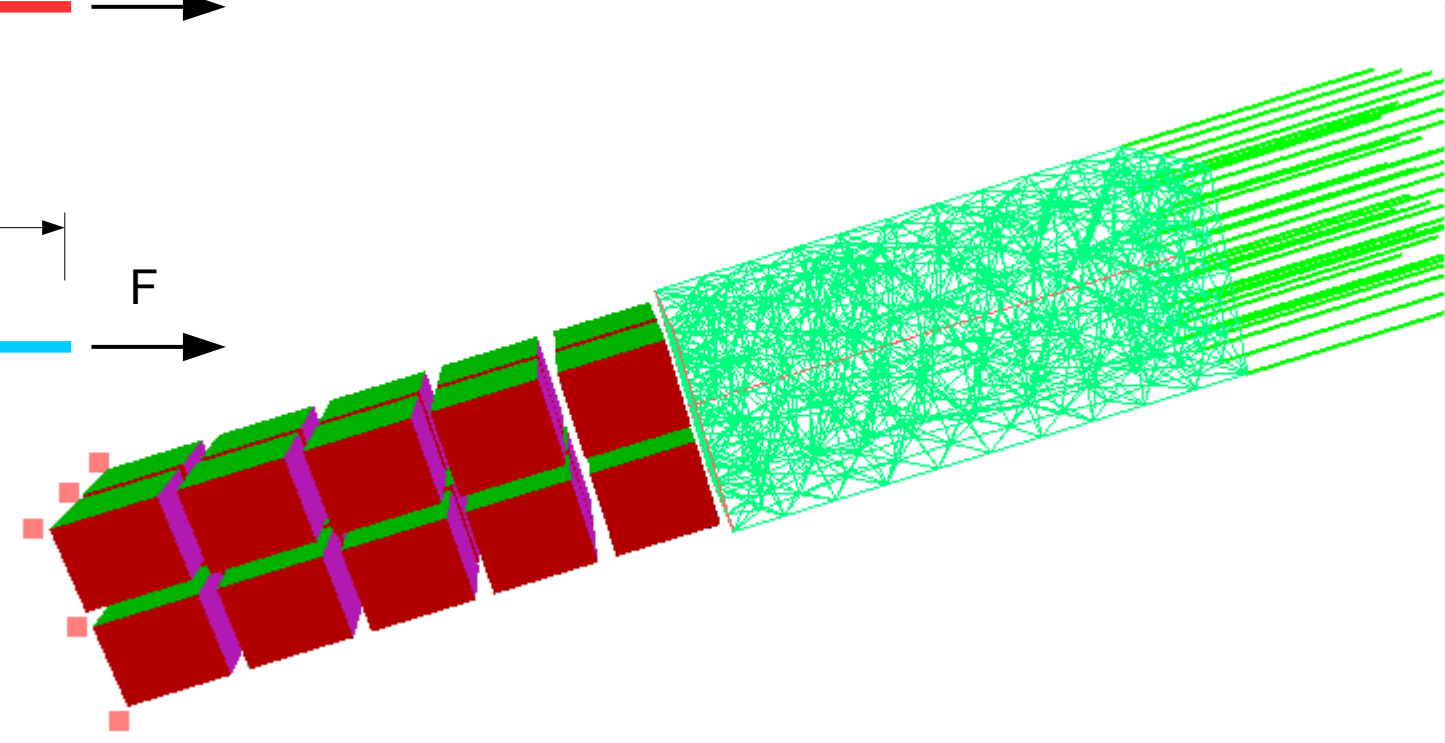
Validation tests: 3D tensile test



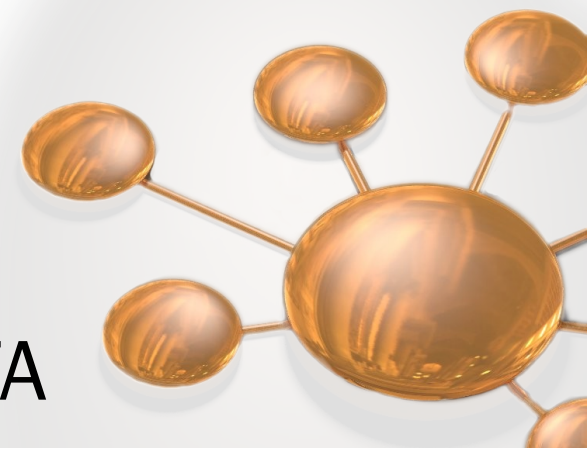
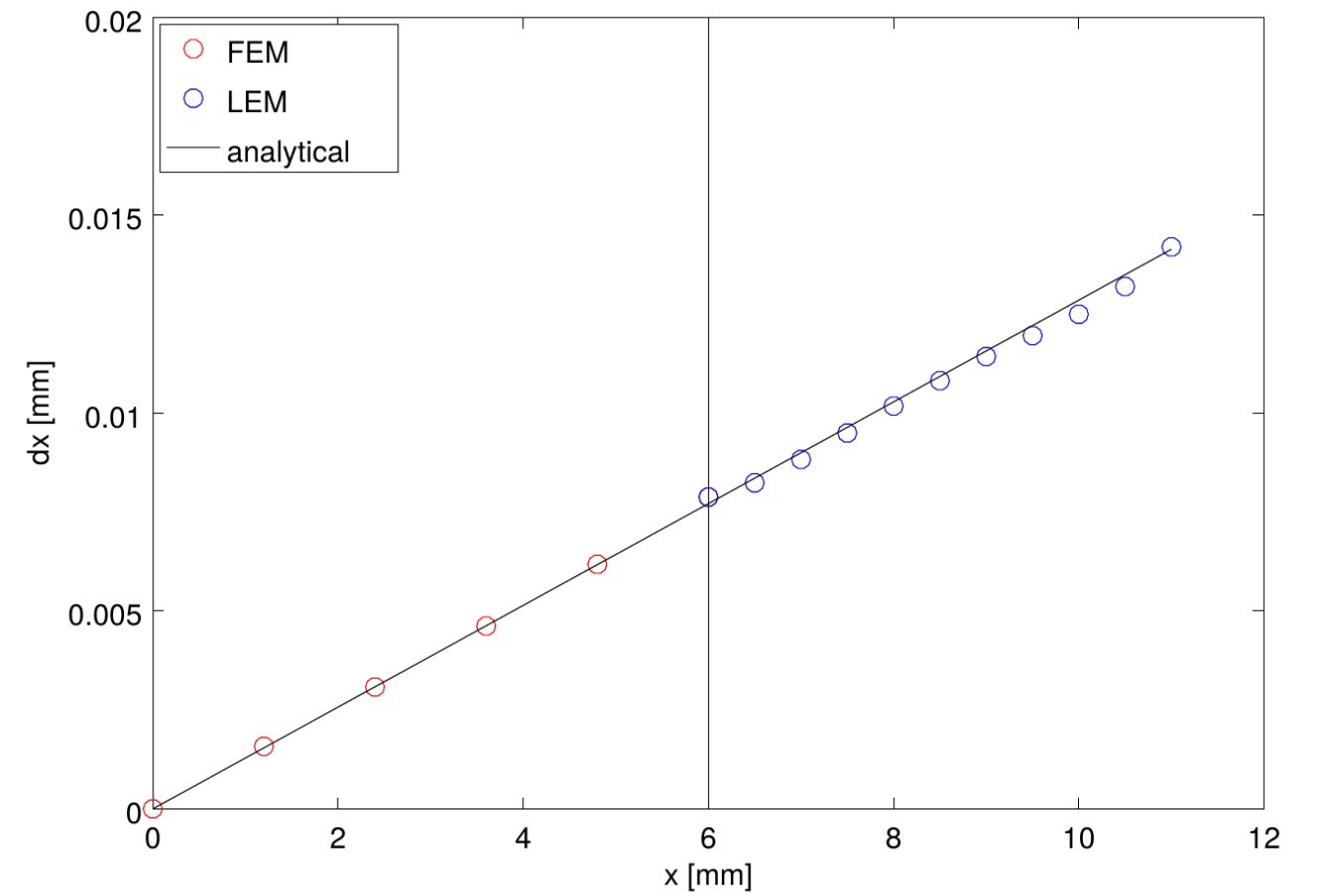
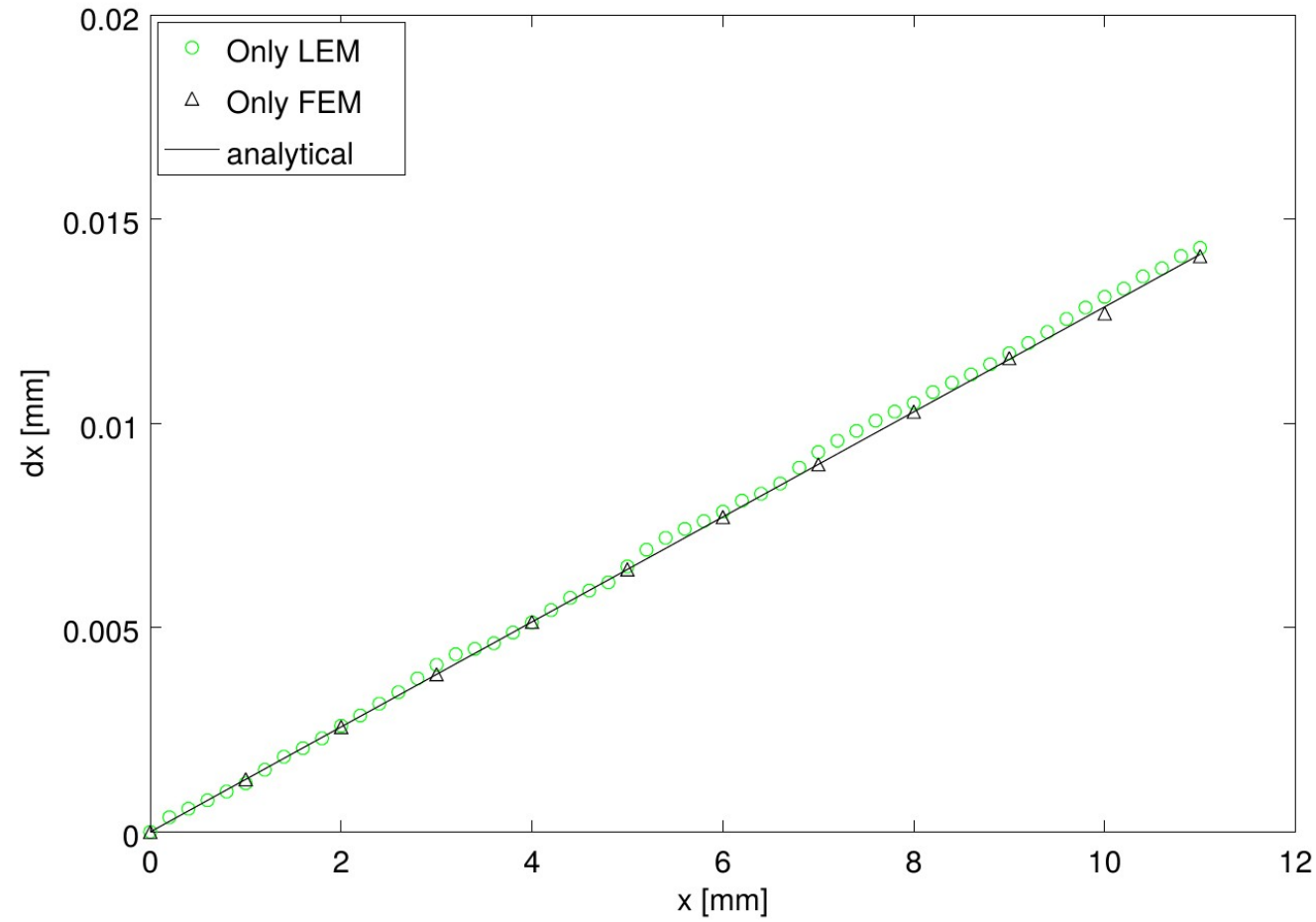
$E = 19.5 \text{ GPa}$
 $\nu = 0.1$
 $bxh = 2 \times 2 \text{ mm}$
 $F = 100 \text{ N}$

Analytical solution

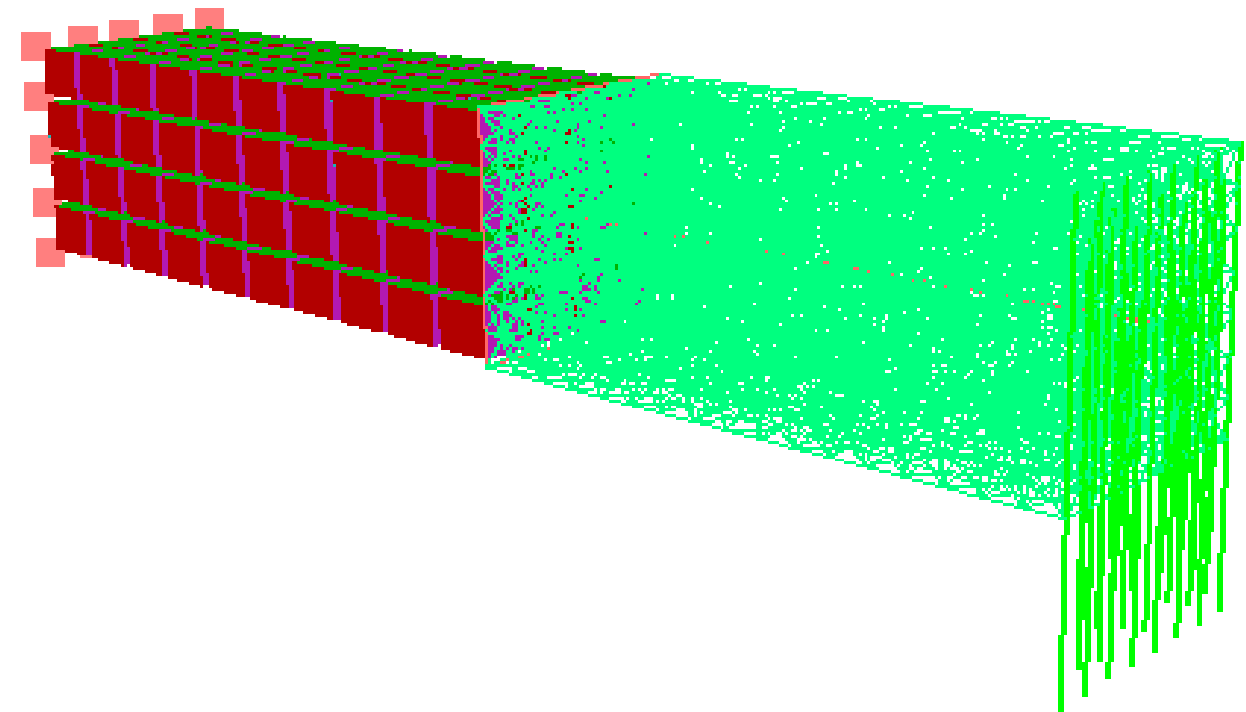
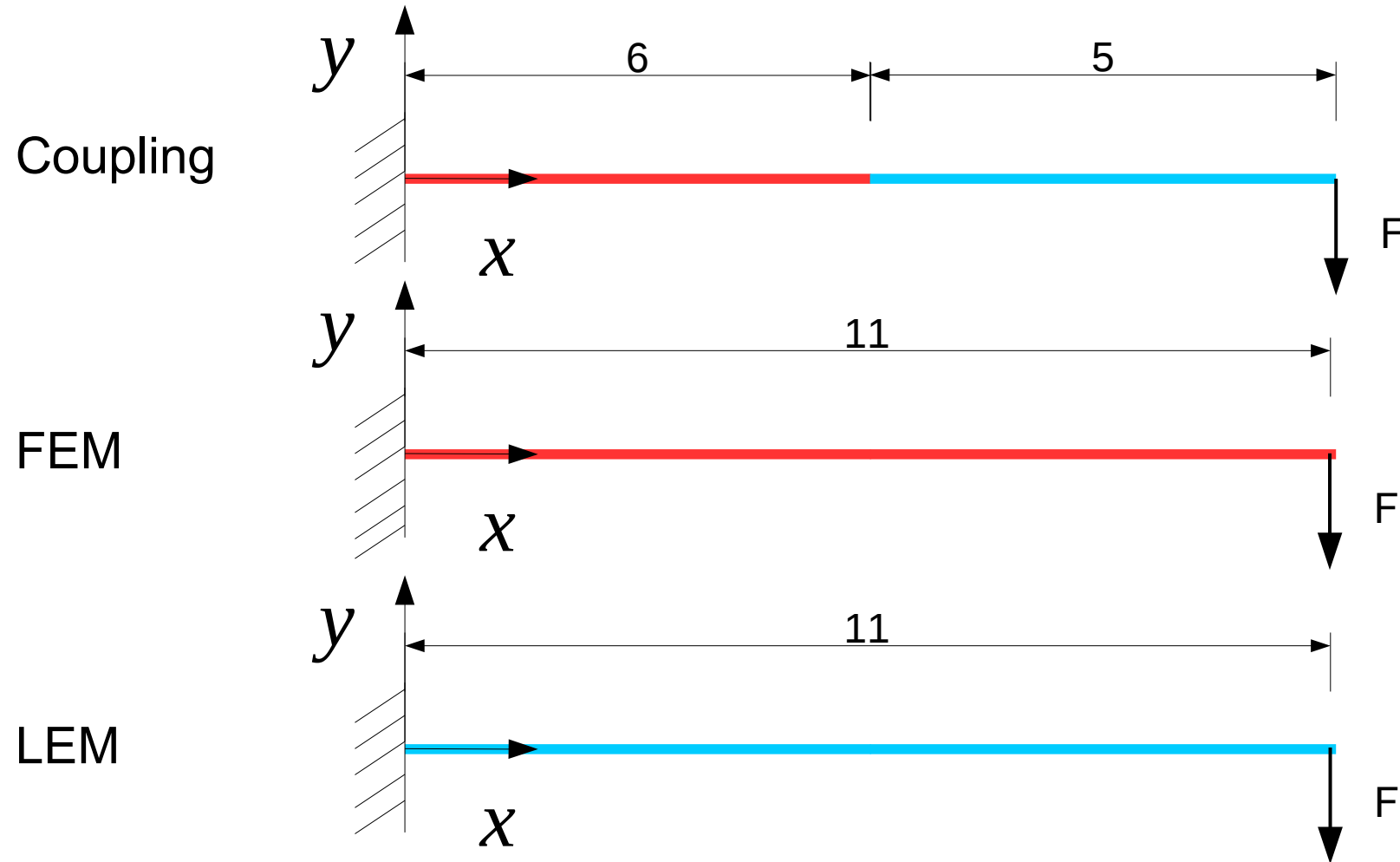
$$u(x) = \int \frac{F}{EA} dx = \frac{F}{EA} x$$



Validation tests: 3D tensile test

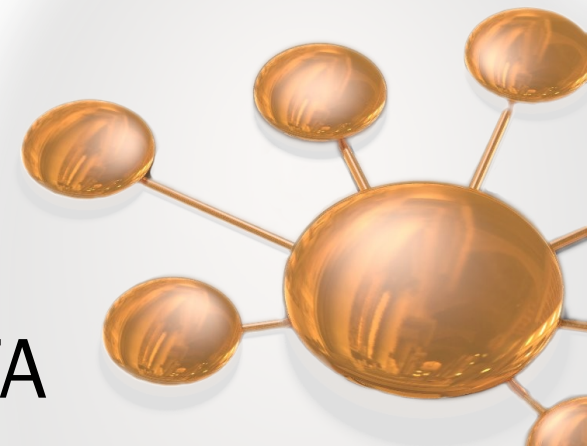


Validation tests: 3D bending test



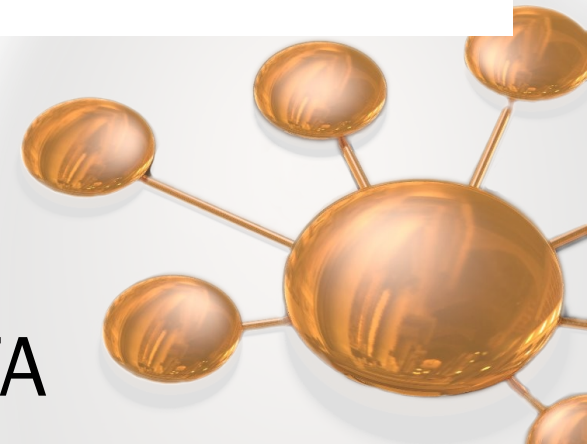
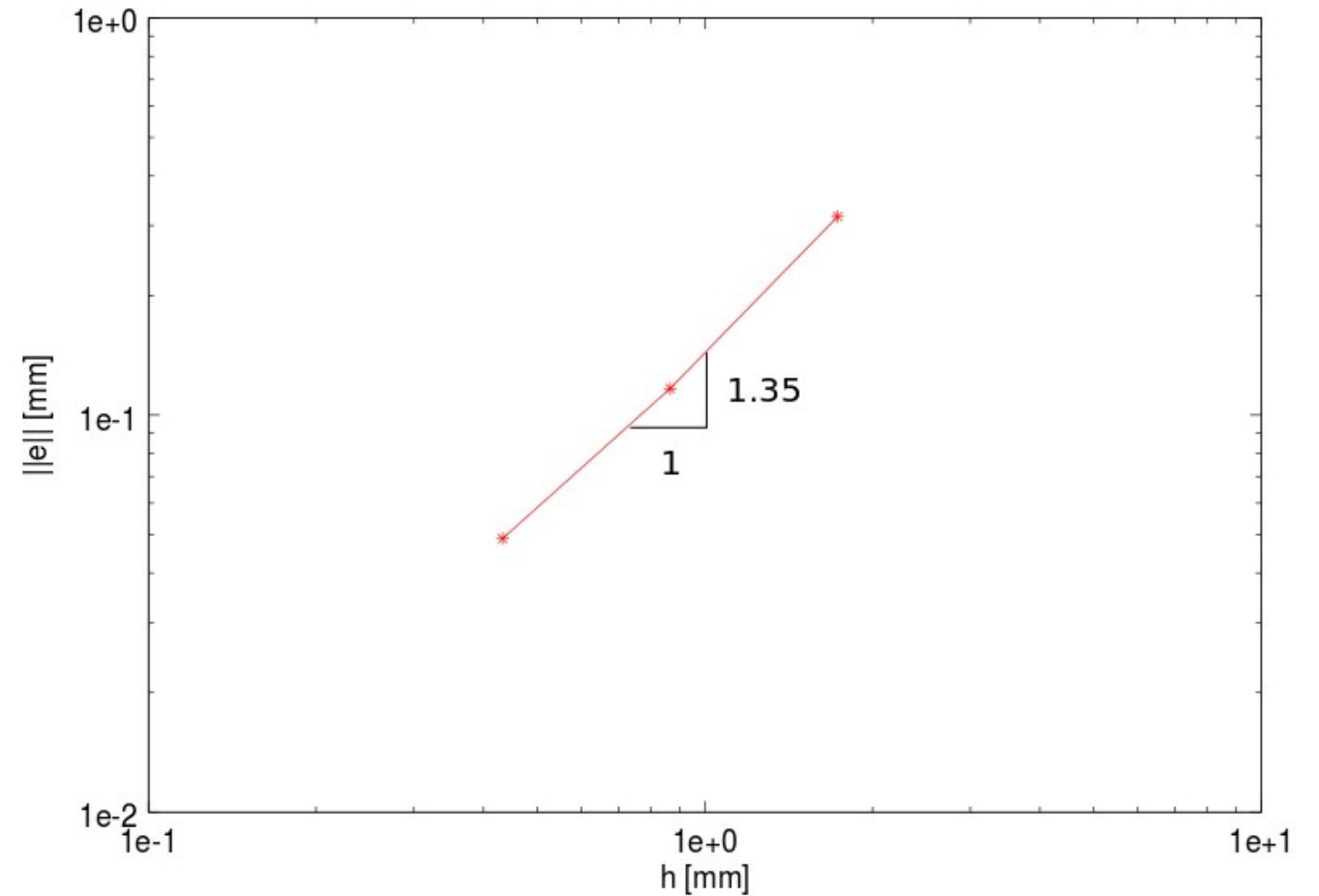
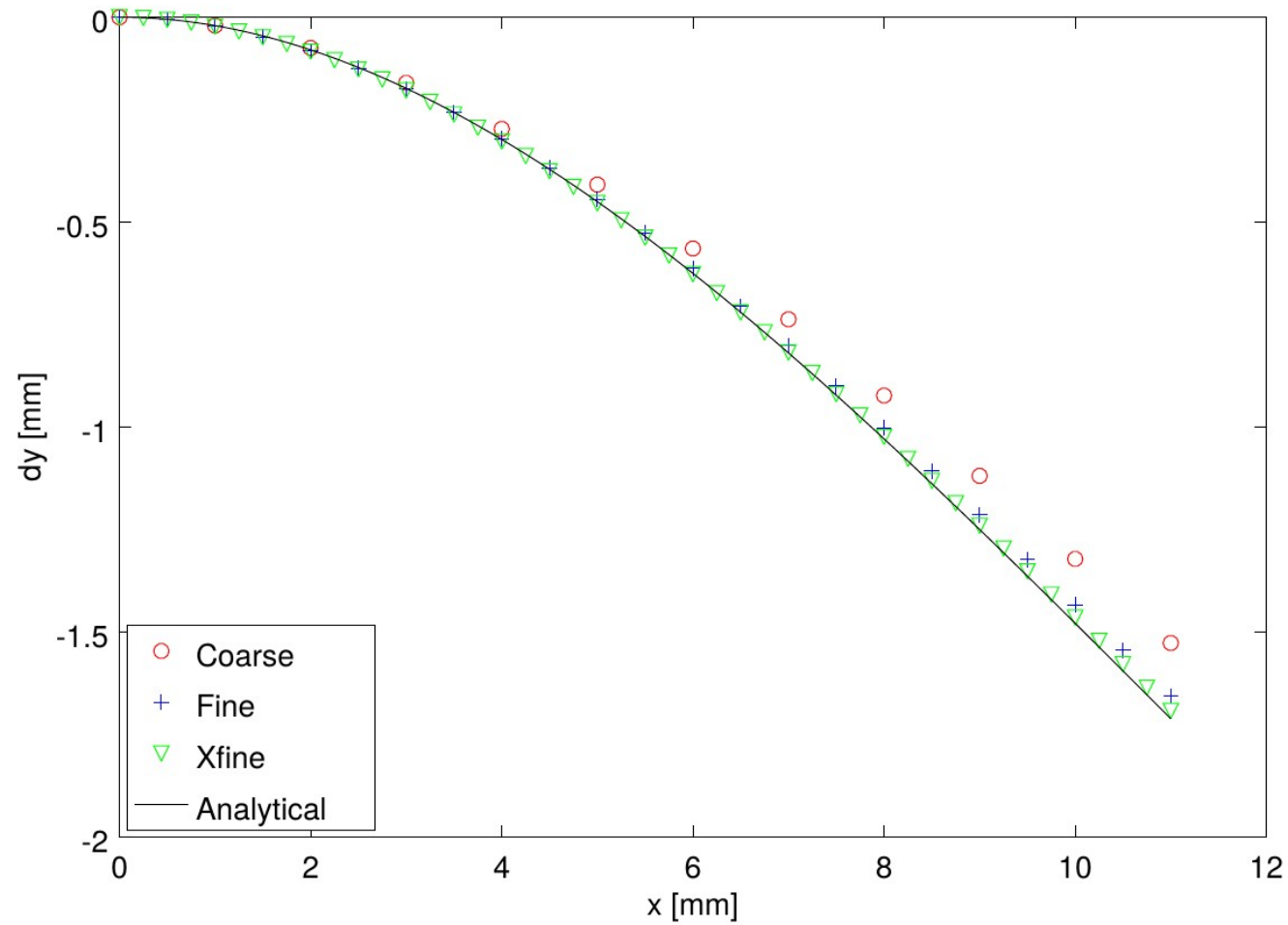
Analytical solution

$$v(x) = \frac{-Fx^2}{6EI} (3L - x)$$

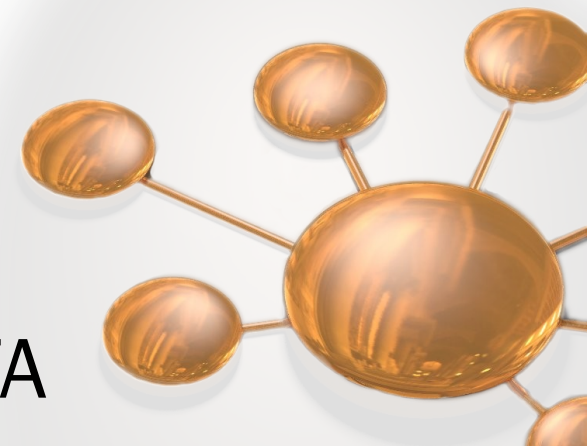
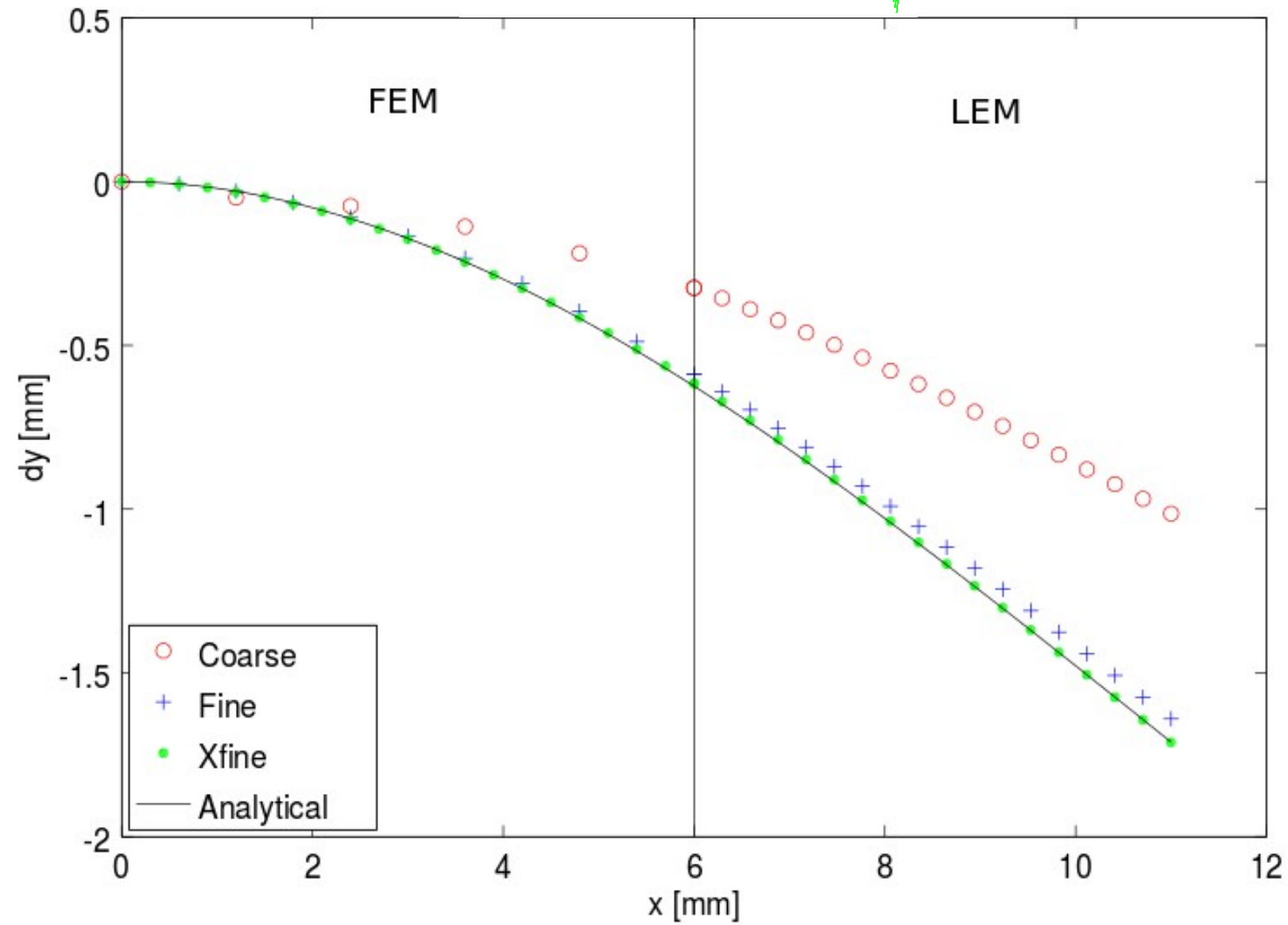
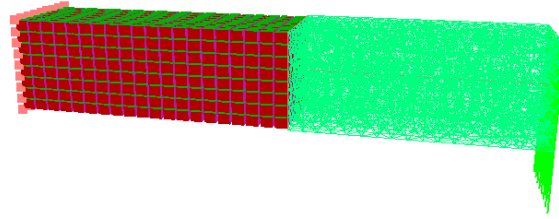


Bending test: FEM approach

$$\|e\|_{L_2} < Ch^{(p+1)}$$

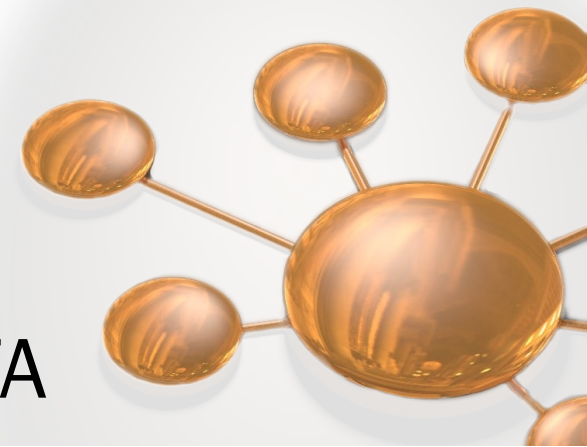
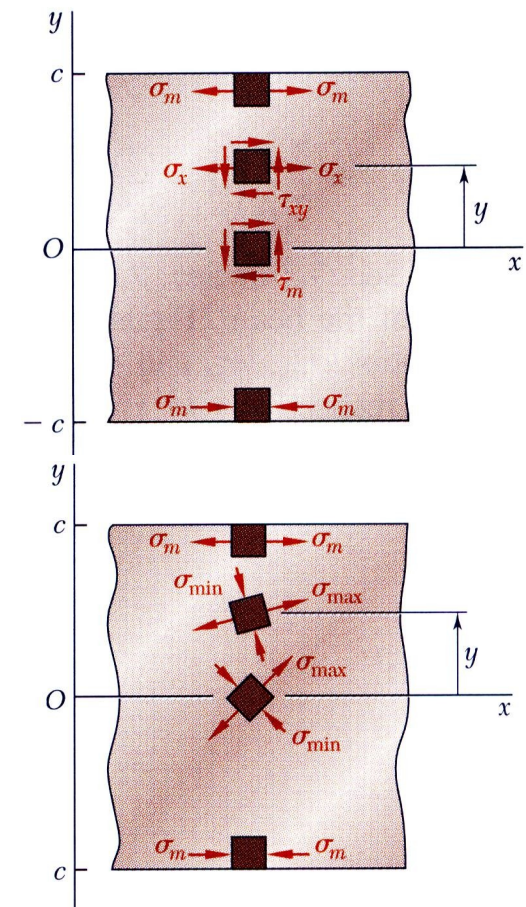
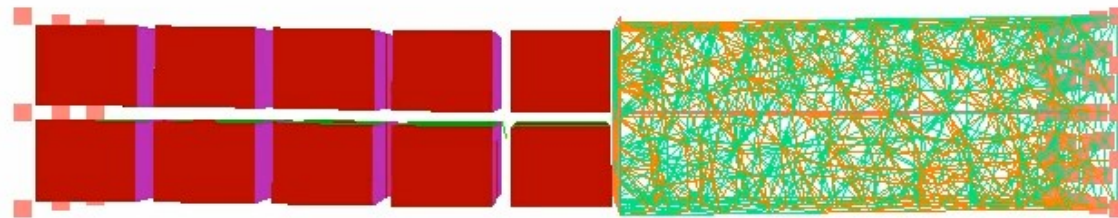


Bending test: FEM-LEM approach

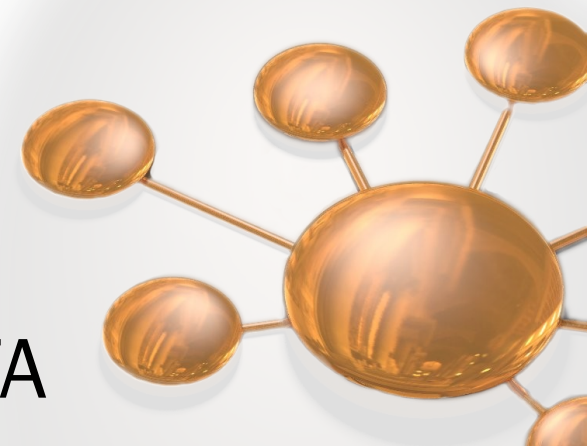
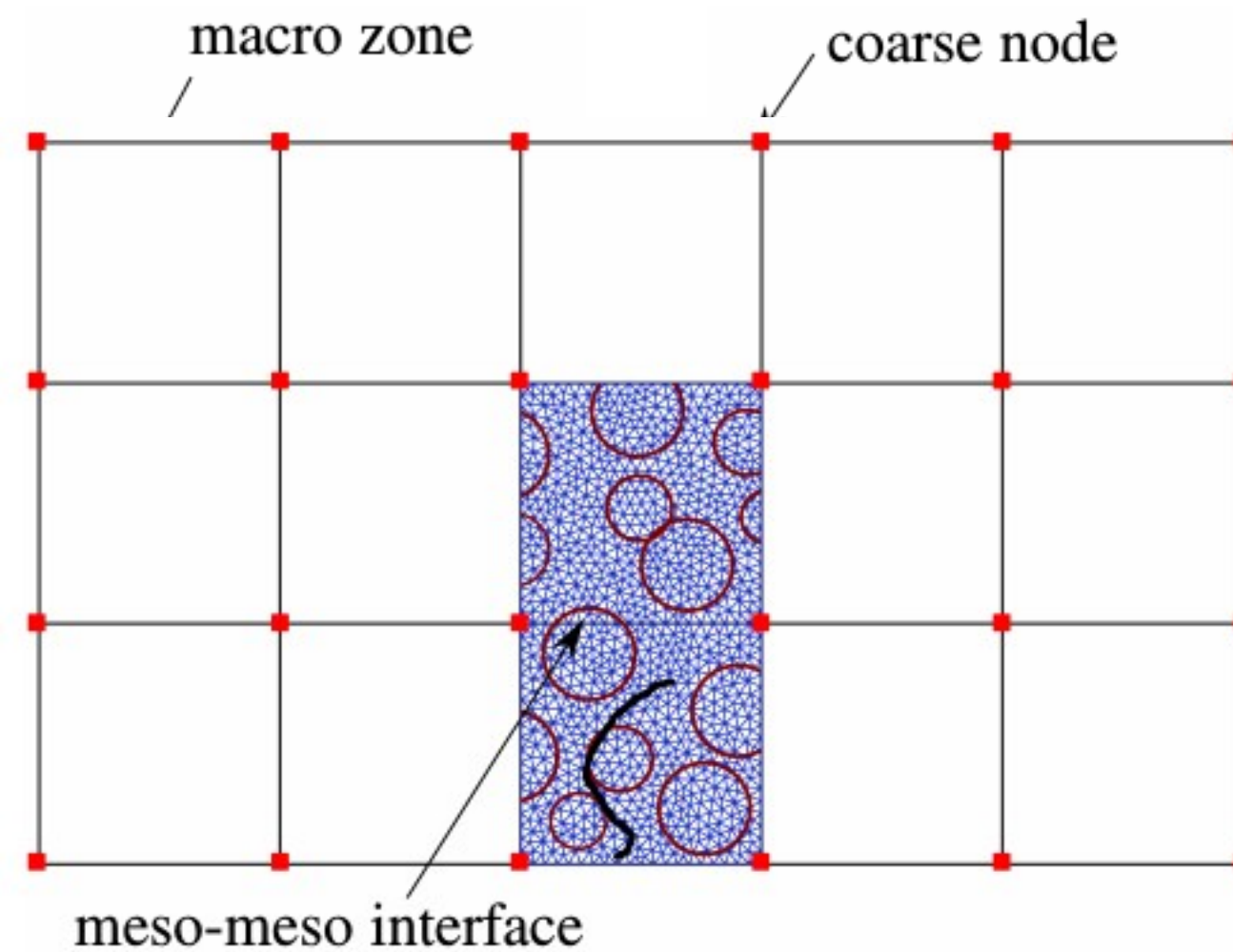


Fracture application

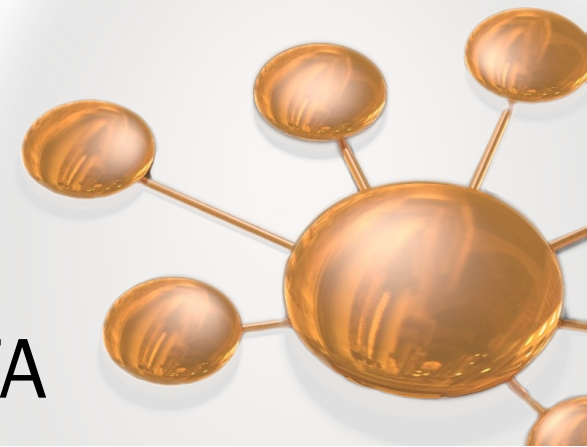
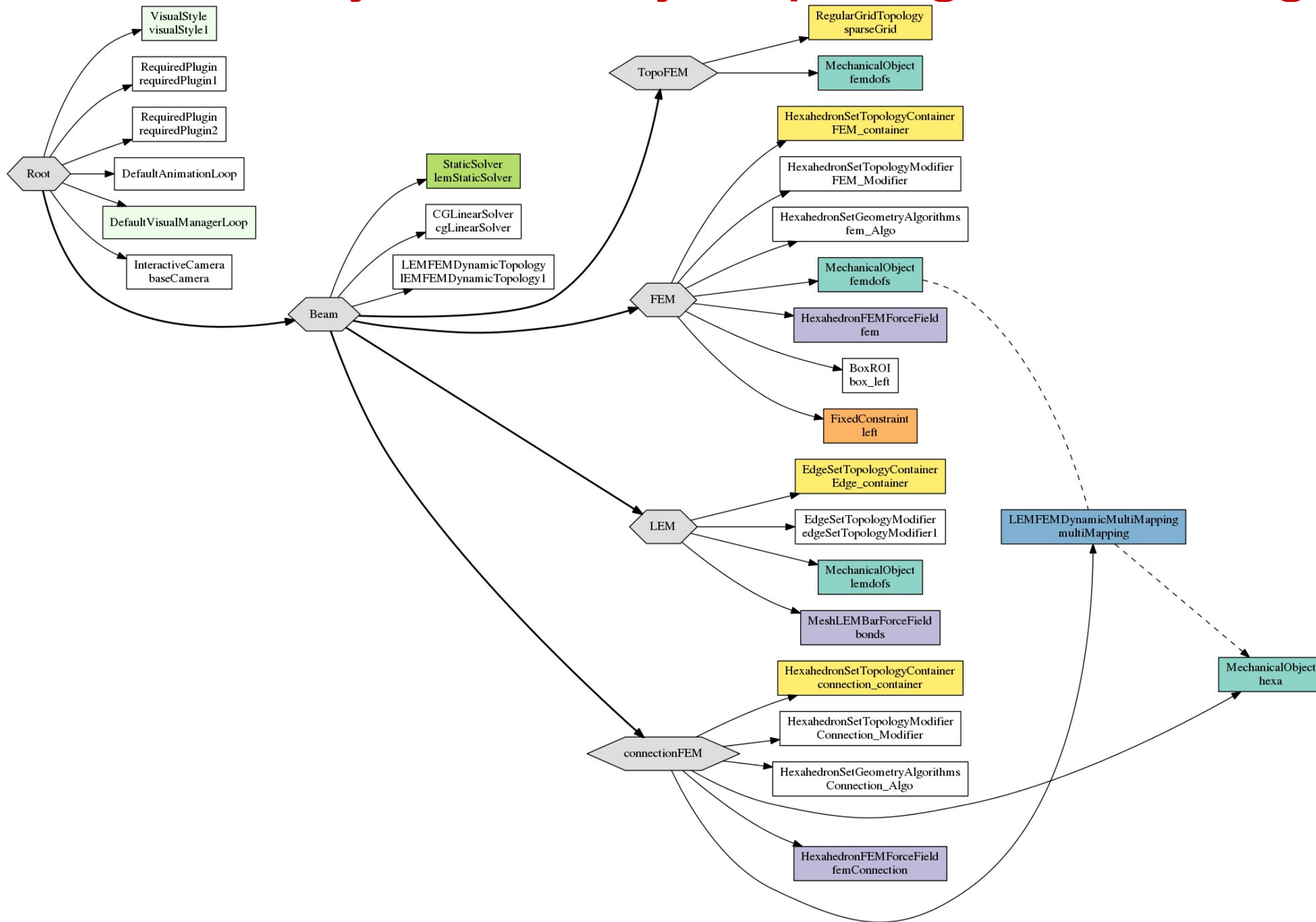
Failure due to tearing



Dynamically Topological Changes



Dynamically Topological Changes



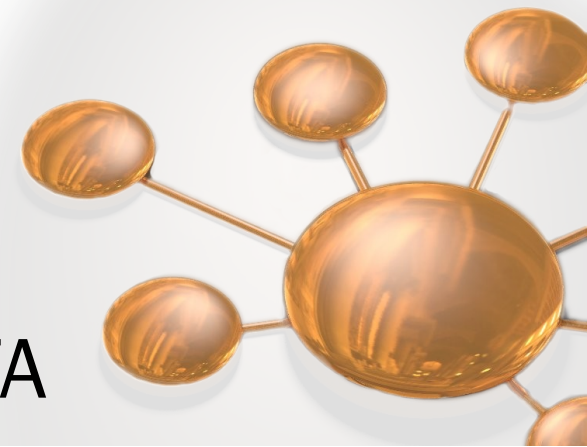
Conclusions & Perspectives

Conclusions

- ☺ Continuum-lattice coupling is valid
- ☺ Fracture simulation

Perspectives

- ☹ Dynamic topological changes
- ☹ Cutting of soft tissue
- ☹ Implementation on GPUs



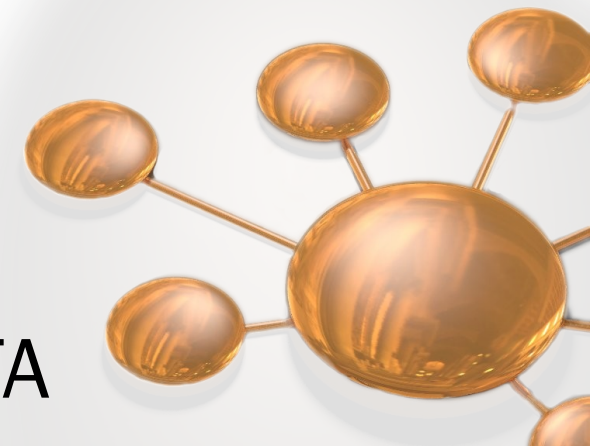
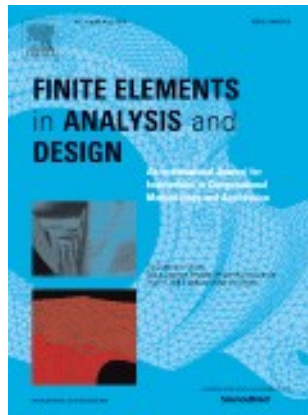
Conclusion & Perspectives

Outlook

▶ A paper on SOFA implementation with validation tests

▶ A paper on fracture results

▶ A paper on real-time cutting



Thank you very much for your kind attention

