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Author for correspondence:

E. Atroshchenko

e-mail: eatroshch@gmail.com,
eatroshchenko@ing.uchile.cl

Fundamental Solutions and Dual Boundary Element Methods for Fracture in Plane Cosserat Elasticity

Elena Atroshchenko¹, Stéphane P.A.
Bordas^{2,3}

¹Department of Mechanical Engineering, University of
Chile, Santiago, 8370448, Chile

²Research Unit in Engineering, Faculté des Sciences,
de la Technologie et de la Communication 6, University
of Luxembourg, Luxembourg

³School of Engineering, Institute of Mechanics and
Advanced Materials, Cardiff University, Cardiff CF24
3AA

In this paper, both singular and hypersingular fundamental solutions of plane Cosserat elasticity are derived and given in a ready-to-use form. The hypersingular fundamental solutions allow to formulate the analogue of Somigliana stress identity, which can be used to obtain the stress and couple stress fields inside the domain from the boundary values of the displacements, microrotation and stress and couple stress tractions. Using these newly derived fundamental solutions, the boundary integral equations of both types are formulated and solved by the boundary element method. Simultaneous use of both types of the equations (approach known as the dual BEM) allows to treat problems where parts of the boundary are overlapping, such as crack problems, and to do this for general geometry and loading conditions. The high accuracy of the boundary element method for both types of equations is demonstrated for a number of benchmark problems, including a Griffith crack problem and a plate with an edge crack. The detailed comparison of the BEM-results and the analytical solution for a Griffith crack and an edge crack is given, particularly, in terms of stress and couple stress intensity factors, as well as the crack opening displacements and microrotations on the crack faces and the angular distributions of stresses and couple stresses around the crack tip.

1. Introduction

This paper presents both a complete derivation of the fundamental solutions arising in plane Cosserat elasticity and a demonstration of their use within a boundary element framework based on the simultaneous use of two types of boundary integral equations on the crack faces.

Cosserat (also known as micropolar) theory of elasticity was first introduced by the Cosserat brothers [1] and further developed by Eringen [2], Nowacki [3] and others as a generalization of the classical elasticity, which takes into account the effects of material's microstructure by enriching material infinitesimal elements with additional rotational degrees of freedom and introducing material internal length scale parameters directly into the constitutive equations. This theory is known to represent well a number of natural and engineered materials, e.g. fiber-reinforced composites, metal foams, concrete, synthetic polymers, and human bones.

A number of analytical and numerical methods, that have been successfully used to treat boundary value problems in classical elasticity, have been developed for micropolar elasticity as well. While the finite element method remains the most popular tool of numerical analysis, the boundary element method (BEM) is evolving as an efficient alternative, especially in modelling problems with discontinuities.

The mathematical foundation of BEM is the boundary integral equation (BIE) method, which has been introduced in [4], [5] to study the solvability of boundary value problems in plane micropolar elasticity. It has been shown that the solutions of these boundary value problems can be found in terms of the single layer and double layer potentials, i.e. in the form of an integral of the product of the unknown densities and the kernel functions, known as the fundamental solutions. This representation allows one to reduce a boundary value problem to the systems of weakly singular, singular and hyper-singular boundary integral equations, which can be subsequently solved by the BEM.

The BEM for singular integral equations, which are also known as displacement/microrotation boundary integral equations (DBIEs), was developed in [7], [8], [9]. To the authors' knowledge, no BEM-solutions for the traction boundary integral equations (TBIEs) of micropolar elasticity have been published yet. This might be attributed to the fact that the hyper-singular fundamental solutions are available in the literature only in an implicit form, which requires additional derivations before it can be implemented into a computer code. However, application of the DBIE-based BEM to crack problems results in a singular system matrix, due to the coincident crack surfaces, and therefore it is limited to the problems with symmetry [10], which avoid use of one of the coincident boundaries. The most common approach to overcome this difficulty, which has been successfully used in classical elasticity, is known as the dual BEM and it consists in simultaneous use of the both types of the BIEs on the crack surfaces.

For this purpose, in the present work, the BEM is developed for the BIEs of both types and its accuracy is demonstrated in various numerical examples, including problems with cracks. Only a limited amount of research in Cosserat fracture has been available in the literature and it has been limited to the studies of some specific cases (see, for example, [11], [12], [13], [14]). The present work contains the first BEM-approach to a general case of a crack problem in Cosserat elasticity. For the sake of comparison with the analytical solution, a classical problem of a Griffith crack is chosen as a numerical example. The obtained data is shown to be in an excellent agreement with the exact solutions in terms of stress and couple stress intensity factors and the crack opening displacements and microrotations along the crack faces.

The BEM-results are also compared with the analytical asymptotical solutions and the finite element data obtained in [14] for an edge crack problem in mode I and mode II in terms of angular distributions of the stresses and couple stresses around the crack tip.

The paper is organized as follows. Section 2 contains mathematical foundations of Cosserat elasticity, in section 3 the boundary integral equations are formulated, in section 4 the boundary element method is outlined. Numerical examples are presented in section 5 and the main results are summarized in 6.

2. Mathematical foundations of plane micropolar elasticity

In what follows, a linear homogeneous micropolar elastic solid is considered. The solid occupies an open domain $S \in \mathbb{R}^2$ with the boundary ∂S . The plane strain state is described by two in-plane displacements u_1, u_2 and one out-of-plane microrotation ϕ_3 . In addition to stresses $\sigma_{11}, \sigma_{12}, \sigma_{21}, \sigma_{22}$ (note, that $\sigma_{12} \neq \sigma_{21}$), two couple stresses m_{13}, m_{23} are introduced (Fig.1), and the following constitutive equations hold [4].

$$\begin{aligned}\sigma_{\alpha\beta} &= \lambda u_{\gamma,\gamma} \delta_{\alpha\beta} + (\mu + \kappa)(u_{\alpha,\beta} + u_{\beta,\alpha}) - \kappa(u_{\alpha,\beta} + \varepsilon_{\alpha\beta 3} \phi_3), \\ m_{\alpha 3} &= \gamma \phi_{3,\alpha}.\end{aligned}\quad (2.1)$$

In eq.(2.1) and throughout the paper it is assumed that Greek indices take values 1,2, while Latin indices vary from 1 to 3, δ_{ij} is the Kronecker delta, ε_{ijk} is the alternating symbol and $\lambda, \mu, \kappa, \gamma$ are material parameters.

In absence of body forces and body couples, the equilibrium equations [4] are given as

$$\begin{aligned}\sigma_{\alpha\beta,\alpha} &= 0, \\ m_{\alpha 3,\alpha} + \varepsilon_{\alpha\beta 3} \sigma_{\alpha\beta} &= 0.\end{aligned}\quad (2.2)$$

In this work we use the same notations for the main equations of plane micropolar elasticity in the matrix and operator form, as originally introduced in [28] and employed, for example, in [5], [10], [29] and others. In order to introduce a unified approach to displacements and microrotations, it is convenient to denote $u_3 = \phi_3$ and introduce a vector of generalized displacements $\mathbf{u} = (u_1, u_2, u_3)^T$ and generalized tractions $\mathbf{t} = (t_1, t_2, t_3)^T$, where boundary tractions t_1, t_2 and a couple traction t_3 are defined as

$$t_\alpha = \sigma_{\beta\alpha} n_\beta, \quad t_3 = m_{\alpha 3} n_\alpha, \quad (2.3)$$

where $\mathbf{n} = (n_1, n_2)^T$ is a unit outward normal to ∂S .

The equations of equilibrium (2.2) then can be rewritten in the form

$$L(\partial_x) \mathbf{u} = 0, \quad (2.4)$$

where the matrix differential operator $L(\partial_x) = L(\xi_\alpha)$ is given by [5]

$$L(\xi_\alpha) = \begin{pmatrix} (\lambda + \mu)\xi_1^2 + (\mu + \kappa)\Delta & (\lambda + \mu)\xi_1\xi_2 & \kappa\xi_2 \\ (\lambda + \mu)\xi_1\xi_2 & (\lambda + \mu)\xi_2^2 + (\mu + \kappa)\Delta & -\kappa\xi_1 \\ -\kappa\xi_2 & \kappa\xi_1 & \gamma\Delta - 2\kappa \end{pmatrix}, \quad (2.5)$$

with $\xi_\alpha = \partial/\partial x_\alpha$ and $\Delta = \partial^2/\partial x_1^2 + \partial^2/\partial x_2^2 = \xi_1^2 + \xi_2^2$.

Together with $L(\xi_\alpha)$ the boundary stress operator $T(\partial_x) = T(\xi_\alpha)$ is considered [5], which is defined by the following equation:

$$T(\xi_\alpha) = \begin{pmatrix} (\lambda + 2\mu + \kappa)\xi_1 n_1 + (\kappa + \mu)\xi_2 n_2 & \lambda\xi_2 n_1 + \mu\xi_1 n_2 & \kappa n_2 \\ \mu\xi_2 n_1 + \lambda\xi_1 n_2 & (\mu + \kappa)\xi_1 n_1 + (\lambda + 2\mu + \kappa)\xi_2 n_2 & -\kappa n_1 \\ 0 & 0 & \gamma\xi_\alpha n_\alpha \end{pmatrix} \quad (2.6)$$

Operator $T(\partial_x)$ is defined according to (2.1),(2.3) in such a way that

$$\mathbf{t} = T(\partial_x) \mathbf{u}. \quad (2.7)$$

Then the boundary value problem (Fig.2) is formulated as follows:

$$\begin{aligned}L(\partial_x) \mathbf{u} &= 0 \quad \text{in } S, \\ \mathbf{u} &= \hat{\mathbf{u}} \quad \text{on } \partial S_u, \\ \mathbf{t} &= \hat{\mathbf{t}} \quad \text{on } \partial S_t,\end{aligned}\quad (2.8)$$

where $\hat{\mathbf{u}} = (\hat{u}_1, \hat{u}_2, \hat{u}_3)^T$ consists of the displacements \hat{u}_1, \hat{u}_2 and the microrotation $\hat{u}_3 = \hat{\phi}_3$ prescribed on Dirichlet boundary ∂S_u , and $\hat{\mathbf{t}} = (\hat{t}_1, \hat{t}_2, \hat{t}_3)^T$ consists of the tractions \hat{t}_1, \hat{t}_2 and the couple traction \hat{t}_3 prescribed on Neumann boundary ∂S_t .

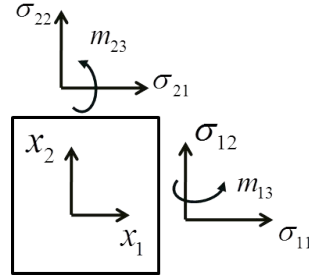


Figure 1. Stresses $\sigma_{\alpha\beta}$ and couple stresses $m_{\alpha\beta}$ acting on a material element in plane micropolar elasticity.

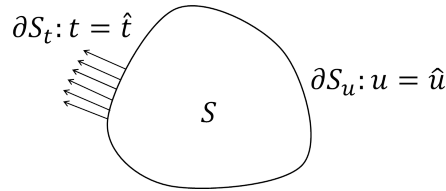


Figure 2. Boundary value problem defined by eq.(2.8)

Together with $\lambda, \mu, \kappa, \gamma$ the following (engineering) micropolar material constants are introduced in [15]:

$$\begin{aligned}
 E &= \frac{(2\mu + \kappa)(3\lambda + 2\mu + \kappa)}{2\lambda + 2\mu + \kappa} && \text{Young's modulus} \\
 G &= \frac{2\mu + \kappa}{2} && \text{shear modulus} \\
 \nu &= \frac{\lambda}{2\lambda + 2\mu + \kappa} && \text{Poisson's ratio} \\
 l &= \sqrt{\frac{\gamma}{2(2\mu + \kappa)}} && \text{characteristic length (bending)} \\
 N &= \sqrt{\frac{\kappa}{2(\mu + \kappa)}} && \text{coupling number } 0 \leq N \leq 1.
 \end{aligned} \tag{2.9}$$

When $N = 0$ or $l = 0$ the micropolar theory reduces to classical elasticity. Case $N = 1$ corresponds to well-known so-called "couple stress theory", which has been studied independently, for example, in [16], [17], [20], [21]. In this theory, the couple stresses are taken into consideration; however, the microrotations are constrained, i.e. defined analogously to macrorotations in classical elasticity.

Two typical approaches to determine Cosserat material constants are experimental methods ([15], [22], [23]) and analytical derivation, based on various homogenization schemes for materials with periodic microstructure, which have been proposed, for example, in [24], [25], [26], [27].

3. Boundary integral equations

In what follows, a source point is denoted by $\mathbf{x} = (x_1, x_2)$ and a field point by $\mathbf{y} = (y_1, y_2)$.

The matrix of fundamental solutions $D = D(\mathbf{x}, \mathbf{y})$ of system (2.4) is derived in [5], in the implicit form, using the method of associated matrices, described in [28], in the form

$$D(\mathbf{x}, \mathbf{y}) = L^*(\partial_x) t(\mathbf{x}, \mathbf{y}), \quad (3.1)$$

where $L^*(\partial_x)$ is the adjoint of $L(\partial_x)$ (matrix consisting of cofactors of $L(\partial_x)$) and $t(\mathbf{x}, \mathbf{y})$ is given as

$$t(\mathbf{x}, \mathbf{y}) = \frac{a}{8\pi k^4} \left\{ [k^2 |\mathbf{x} - \mathbf{y}|^2 + 4] \log |\mathbf{x} - \mathbf{y}| + 4K_0(k|\mathbf{x} - \mathbf{y}|) \right\} \quad (3.2)$$

and constants a, k are defined by

$$a^{-1} = \gamma(\lambda + 2\mu + \kappa)(\mu + \kappa), \quad k^2 = \frac{\kappa(2\mu + \kappa)}{\gamma(\mu + \kappa)}, \quad (3.3)$$

where K_0 is the modified Bessel function of order zero. The full expression of matrix D in polar coordinates

$$y_1 = x_1 + \rho \cos \theta, \quad y_2 = x_2 + \rho \sin \theta \quad (3.4)$$

is given, for example, in [18] and [19]. In view of (3.1) and (3.2)

$$D(\mathbf{x}, \mathbf{y}) = (D(\mathbf{y}, \mathbf{x}))^T. \quad (3.5)$$

Along with D the matrix of singular solutions $P = P(\mathbf{x}, \mathbf{y}; \mathbf{n}_y)$ is introduced by

$$P(\mathbf{x}, \mathbf{y}; \mathbf{n}_y) = (T(\partial_y) D(\mathbf{y}, \mathbf{x}))^T, \quad (3.6)$$

where notation ∂_y implies that in eq.(2.6) $\xi_\alpha = \partial/\partial y_\alpha$ and normal \mathbf{n}_y is applied at the point \mathbf{y} . The full expression of matrix P is given, for example, in [18]. It can be verified by direct differentiation that the columns of $D(\mathbf{x}, \mathbf{y})$ and $P(\mathbf{x}, \mathbf{y}; \mathbf{n}_y)$ satisfy (2.4) at all $\mathbf{x}, \mathbf{y} \in \mathbb{R}^2, \mathbf{x} \neq \mathbf{y}$.

In order to formulate traction boundary integral equations, two more matrices are required. Namely, matrix $H = H(\mathbf{x}, \mathbf{y}; \mathbf{n}_x)$ and $S = S(\mathbf{x}, \mathbf{y}; \mathbf{n}_x, \mathbf{n}_y)$ which are obtained by applying stress operator $T(\partial_x)$ to matrices $D(\mathbf{x}, \mathbf{y})$ and $P(\mathbf{x}, \mathbf{y}; \mathbf{n}_y)$:

$$H(\mathbf{x}, \mathbf{y}; \mathbf{n}_x) = T(\partial_x) D(\mathbf{x}, \mathbf{y}), \quad S(\mathbf{x}, \mathbf{y}; \mathbf{n}_x, \mathbf{n}_y) = T(\partial_x) P(\mathbf{x}, \mathbf{y}; \mathbf{n}_y) \quad (3.7)$$

The full derivation of matrices D, P, H, S is presented in [19] with the final expressions in a ready-to-use form in both, symbolic and C/C++ formats.

In order to investigate the behavior of matrices D, P, H, S in the vicinity of $\mathbf{x} = \mathbf{y}$, they are expanded in Taylor series in polar coordinates (3.4). Straightforward derivations show that as $\rho \rightarrow 0$, the weakly-singular terms of D are [4]

$$D_{11,22} = -\frac{b}{2\pi} \ln \rho + O(1), \quad D_{33} = -\frac{1}{2\pi\gamma} \ln \rho + O(1), \quad (3.8)$$

where

$$b = \frac{1+\nu}{E} \left(\frac{3-4\nu}{2(1-\nu)} - N^2(1+\nu) \right), \quad \frac{1}{\gamma} = \frac{1+\nu}{2El^2}. \quad (3.9)$$

The components of matrices P and H with the highest order of singularity being ρ^{-1} are listed below:

$$\begin{aligned} P_{12,21} &= \pm \frac{\mu'}{2\pi} \frac{n_2^y \cos \theta - n_1^y \sin \theta}{\rho} + O(1), \\ H_{12,21} &= \mp \frac{\mu'}{2\pi} \frac{n_2^x \cos \theta - n_1^x \sin \theta}{\rho} + O(1), \end{aligned} \quad (3.10)$$

where $\mu' = \frac{1-2\nu}{2(1-\nu)} - N^2$ [4]. Components $P_{\alpha 3}, P_{3\alpha}, H_{\alpha 3}, H_{3\alpha}$ are weakly-singular, i.e. of order $\ln \rho$.

For matrix S as $\rho \rightarrow 0$ the expansion is

$$\begin{aligned} S_{11,22} &= \frac{\mu''}{2\pi} \frac{1}{\rho^2} + O(\ln \rho), \quad S_{33} = \frac{\gamma}{2\pi} \frac{1}{\rho^2} + O(\ln \rho), \\ S_{13,31} &= \pm \frac{\mu'''}{2\pi} \frac{\sin \theta}{\rho} + O(\ln \rho), \quad S_{23,32} = \mp \frac{\mu'''}{2\pi} \frac{\cos \theta}{\rho} + O(\ln \rho) \end{aligned} \quad (3.11)$$

where $\mu'' = E \left(\frac{1}{1-\nu^2} + 2N^2 \right)$, $\mu''' = \frac{EN^2}{1+\nu}$ and components S_{12}, S_{21} are of order $\ln \rho$.

The derivation of the boundary integral equations in plane Cosserat elasticity is based on the following analogue of Somigliana identity [5]

$$u_i(\mathbf{x}) = \int_{\partial S} [D_{ij}(\mathbf{x}, \mathbf{y}) t_j(\mathbf{y}) - P_{ij}(\mathbf{x}, \mathbf{y}; \mathbf{n}_y) u_j(\mathbf{y})] ds_y \quad \mathbf{x} \in S \quad (3.12)$$

Analogously to the classical theory, the displacement boundary integral equation (DBIE) is obtained from (3.12) by letting point \mathbf{x} tend to the boundary ∂S . Removing a small vicinity of a singular point \mathbf{x} and using the Taylor series expansions of the kernel functions, a straightforward derivation yields:

$$\frac{1}{2} u_i(\mathbf{x}) + \oint_{\partial S} P_{ij}(\mathbf{x}, \mathbf{y}; \mathbf{n}_y) u_j(\mathbf{y}) ds_y - \int_{\partial S} D_{ij}(\mathbf{x}, \mathbf{y}) t_j(\mathbf{y}) ds_y = 0, \quad \mathbf{x} \in \partial S \quad (3.13)$$

Sign \oint indicates that the integrals containing P_{12}, P_{21} are singular and understood as Cauchy principal values. Factor $\frac{1}{2}$ in (3.13) is known in classical elasticity as the "jump term", which remains equal to $\frac{1}{2}$ on a smooth piece of the boundary in Cosserat elasticity for both, displacements u_1, u_2 and microrotation u_3 .

In order to derive the traction boundary integral equation, first operator $T(\partial_x)$ is applied to eq. (3.12) (with arbitrary direction $\mathbf{n}(\mathbf{x})$) to obtain the following analogue of Somigliana's stress identity:

$$T_{ij}(\partial_x) u_j(\mathbf{x}) = \int_{\partial S} [H_{ij}(\mathbf{x}, \mathbf{y}; \mathbf{n}_x) t_j(\mathbf{y}) - S_{ij}(\mathbf{x}, \mathbf{y}; \mathbf{n}_x, \mathbf{n}_y) u_j(\mathbf{y})] ds_y \quad \mathbf{x} \in S \quad (3.14)$$

Then, taking $\mathbf{n}(\mathbf{x})$ to be the normal to ∂S and performing limiting process analogously to the procedure described above for DBIE, the following TBIE is obtained:

$$\frac{1}{2} t_i(\mathbf{x}) - \oint_{\partial S} H_{ij}(\mathbf{x}, \mathbf{y}; \mathbf{n}_x) t_j(\mathbf{y}) ds_y + \int_{\partial S} S_{ij}(\mathbf{x}, \mathbf{y}; \mathbf{n}_x, \mathbf{n}_y) u_j(\mathbf{y}) ds_y = 0, \quad \mathbf{x} \in \partial S, \quad (3.15)$$

where integrals containing $H_{12}, H_{21}, S_{13}, S_{23}, S_{31}, S_{32}$ are singular and sign \oint indicates, that the integrals with S_{11}, S_{22}, S_{33} are hyper-singular and understood as Hadamard finite part integrals.

4. Boundary element method formulation

In the present work, the standard BEM discretisation with the quadratic Lagrange basis is applied to equations (3.13), (3.15), which makes use of the following set of shape functions:

$$N_1(\xi) = \frac{\xi(\xi - \lambda_0)}{2\lambda_0^2}, \quad N_2(\xi) = -\frac{(\xi + \lambda_0)(\xi - \lambda_0)}{\lambda_0^2}, \quad N_3(\xi) = \frac{\xi(\xi + \lambda_0)}{2\lambda_0^2}. \quad (4.1)$$

The boundary ∂S is discretized with N elements ∂S_n and the shape functions (4.1) with $\lambda_0 = 1$, while the solutions $u_i(\mathbf{y})$, $t_i(\mathbf{y})$ are approximated with the discontinuous basis with $\lambda_0 = \frac{2}{3}$ and the three nodal values at each element. All weakly singular integrals, arising from such discretization are calculated using Telles transform [30]. Singular and hyper-singular integrals are calculated by means of so-called singularity subtraction technique [31], [32], which makes use of the Taylor expansion of the fundamental solutions in the vicinity of a collocation point, given by eq.(3.10),(3.11). Then the collocation point is placed subsequently at every node at each element, yielding a system of $9N$ linear algebraic equations for the unknown nodal values of generalized displacements and tractions.

5. Numerical results

In this section four numerical examples are shown. In the first example, the problem of a bending plate is considered, and it is shown that the exact solution, given by the polynomials of second degree, can be reproduced with a good accuracy by BEM on a coarse mesh.

In the second example, the problem of the stress concentration around a circular hole is studied. The stress concentration factors obtained from both types of the equations and the stress and couple stress field on the boundary and inside the domain are compared with the analytical solutions.

In the third example, the classical problem of a Griffith crack is solved by means of the dual BEM with use of both types of boundary integral equations. The BEM-solution is compared with the analytical data for stress and couple stress intensity factors, as well as for the displacements and microrotations at the crack faces.

In the fourth example, the dual BEM formulation is applied to the problem of an edge crack in both loading modes. The BEM-results are shown to be in a good agreement with the analytical and FEM-solutions, available in the literature for the distribution of stresses and couple-stresses around the crack tip, as well as the stress and couple stress intensity factors.

(a) A square plate under pure bending

As a first example, a square micropolar plate under pure bending is considered (Fig.3). The following boundary conditions are prescribed:

$$\begin{aligned} u_1 &= 0, \quad t_2 = 0, \quad u_3 = 0 \quad \text{at } x_1 = 0, \\ t_1 &= t_2 = t_3 = 0 \quad \text{at } x_2 = \pm h, \\ t_1 &= \sigma_0 x_2, \quad t_2 = 0, \quad t_3 = -m_0 \quad \text{at } x_1 = 2h, \end{aligned} \quad (5.1)$$

where

$$\sigma_0 = \frac{2G}{1-\nu} \frac{M_0}{D + \gamma h}, \quad m_0 = \frac{\gamma M_0}{D + \gamma h}, \quad D = \frac{Gh^3}{6(1-\nu)}. \quad (5.2)$$

The analytical solution $\mathbf{u}^A = (u_1^A, u_2^A, u_3^A)^T$ for this problem was first derived in [6] as

$$u_1^A = \frac{M_0 x_1 x_2}{D + \gamma h}, \quad u_2^A = -\frac{1}{2} \frac{M_0}{D + \gamma h} \left(x_1^2 + \frac{\nu}{1-\nu} x_2^2 \right), \quad u_3^A = -\frac{M_0 x_1}{D + \gamma h} \quad (5.3)$$

In [7] this problem, but for a rectangular geometry, was solved by BEM for the following values of the parameters, which we used in the present study as well:

$$M_0 = 1000 \text{ N}, \quad h = 0.1 \text{ m}, \quad G = 5.1768 \times 10^7 \frac{\text{N}}{\text{m}}, \quad \nu = 0.3 \quad (5.4)$$

The relative error e_i of every component of the BEM-solution $\mathbf{u}^B = (u_1^B, u_2^B, u_3^B)^T$ is defined as:

$$e_i = \frac{\max |u_i^B - u_i^A|}{\max |u_i^A|} \quad (5.5)$$

The boundary was discretized with 4 elements, or 36 degrees of freedom, as show in Fig.4. Since the polynomial form of the solution approximation can represent the solution exactly, the main source of error in the BEM-results is the integration error. In contrast to the BEM of classical elasticity, accuracy of integration in the Cosserat case depends significantly on the material constants due to the presence of small parameter l in the Bessel functions in the fundamental solutions. Therefore in order to capture the behavior of the kernels, the order of Gaussian quadrature was chosen depending on material parameter l (increasing for decreasing values of l), and it was kept the same for different values of N corresponding to the same value of l . The results for both types of the BIEs are shown in table 1. The obtained relative errors, as defined by eq.(5.5), are of order between 10^{-10} and 10^{-4} . It was observed, that for the same values of material parameters and the order of Gaussian quadrature, TBIEs perform slightly better than DBIEs.

In [7] the solution at the corner point was shown to have an accuracy of order 10^{-4} for the boundary discretization with 8-20 elements, which is comparable with the errors obtained in the present work for the singular boundary integral equations with the use of 4 elements.

		DBIEs			TBIEs		
		$N=0.1$	$N=0.5$	$N=0.9$	$N=0.1$	$N=0.5$	$N=0.9$
$l/(2h)=10^{-2}$	e_1	2×10^{-7}	4×10^{-6}	2×10^{-5}	4×10^{-9}	3×10^{-7}	2×10^{-6}
	e_2	3×10^{-7}	6×10^{-6}	3×10^{-5}	6×10^{-9}	6×10^{-7}	3×10^{-6}
	e_3	2×10^{-5}	2×10^{-4}	6×10^{-4}	2×10^{-8}	3×10^{-7}	1×10^{-6}
$l/(2h)=10^{-1}$	e_1	5×10^{-7}	7×10^{-7}	1×10^{-5}	5×10^{-9}	6×10^{-8}	2×10^{-7}
	e_2	1×10^{-6}	8×10^{-7}	2×10^{-5}	5×10^{-8}	2×10^{-7}	1×10^{-6}
	e_3	9×10^{-6}	8×10^{-6}	4×10^{-5}	1×10^{-8}	7×10^{-8}	6×10^{-7}
$l/(2h)=10^0$	e_1	2×10^{-6}	6×10^{-7}	1×10^{-6}	1×10^{-7}	5×10^{-8}	6×10^{-8}
	e_2	2×10^{-6}	8×10^{-7}	3×10^{-6}	7×10^{-7}	4×10^{-7}	6×10^{-7}
	e_3	7×10^{-7}	9×10^{-6}	1×10^{-6}	1×10^{-9}	6×10^{-8}	3×10^{-8}
$l/(2h)=10^1$	e_1	3×10^{-5}	5×10^{-5}	4×10^{-5}	3×10^{-6}	3×10^{-6}	7×10^{-7}
	e_2	4×10^{-5}	7×10^{-5}	1×10^{-5}	1×10^{-5}	3×10^{-5}	1×10^{-5}
	e_3	7×10^{-7}	7×10^{-7}	7×10^{-7}	2×10^{-10}	4×10^{-9}	4×10^{-9}

Table 1. A plate under pure bending: relative errors e_1 , e_2 , e_3 , as defined by eq.(5.5), for both types of the BIEs for various values of the coupling number N and ratio of the material length l to the size of the plate $2h$.

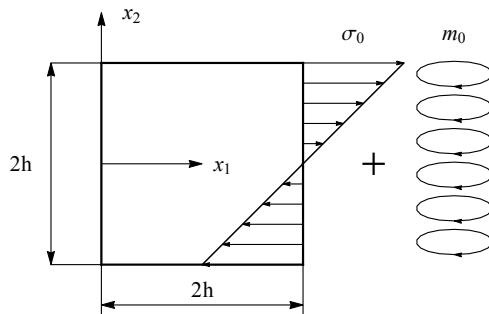


Figure 3. A micropolar plate under pure bending.

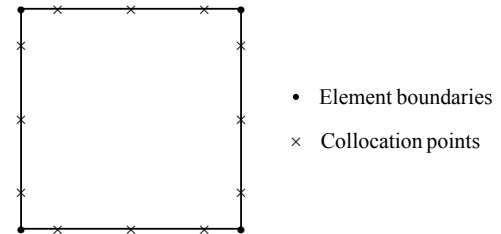


Figure 4. A plate under pure bending: coarse mesh of the boundary.

(b) A circular hole in an infinite plate

In the second example, the problem of an infinite plate in tension, weakened by a circular hole of radius a , is considered (Fig.5). The full analytical solution for all stresses and couple-stresses is given in [33]. In order to demonstrate the performance of the method for the non-straight boundaries as well as non-polynomial boundary conditions, the problem is modeled as a finite quarter-plate of size $L \times L$, $L = 4a$ with the analytical tractions and couple tractions, given by rational functions, prescribed at $x = L$ and $y = L$ (Fig.6).

In tables 2,3 the stress concentration factors (SCFs) are presented for two values of the material length l : $l = a$, $l = 0.1a$ respectively, $\nu = 0.3$ and for different values of the coupling number N , for both types of boundary integral equations. In all cases a mesh consisting of 68 elements, uniformly graded towards the edges of the hole, was used. The number of Gauss points per element was chosen for all cases to be 200. As it is seen from tables 2,3 the SCF-solutions for a circular crack

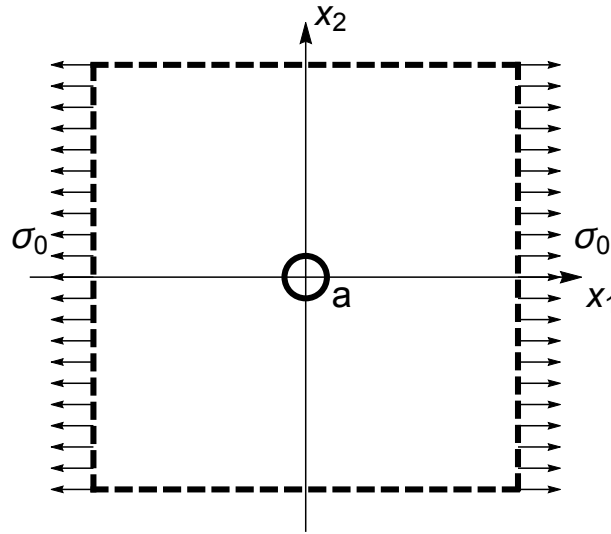


Figure 5. An infinite plate with an circular hole in tension.

N	Analytical	DBIE	e(%)	TBIE	e(%)
0.10	2.9728	2.9720	0.03 %	2.9790	0.21 %
0.25	2.8484	2.8478	0.03 %	2.8532	0.17 %
0.50	2.5490	2.5489	0.01 %	2.5490	0.0006 %
0.75	2.2739	2.2740	0.004 %	2.2683	0.25 %
0.90	2.1416	2.1418	0.007 %	2.1326	0.42 %

Table 2. Stress concentration factors for a circular hole: $l = a$.

can be reproduced by both types of equations with the relative error within 1%. The relative error is defined as

$$e = \frac{|SCF^{BEM} - SCF^{Analyt}|}{SCF^{Analyt}}. \quad (5.6)$$

The detailed BEM-analysis of stress concentration around a hole in a micropolar plate is done in [8]. Case $N = 1$ corresponds to the couple-stress elasticity and it was studied also by means of the boundary element method in [21].

The stress distribution along the edges of the quarter plate is obtained as a direct output of BEM. In fig. (7) distribution of $\sigma_{\theta\theta}$ along $\theta = \frac{\pi}{2}$ is shown for $l = a$, $\nu = 0.3$ and various values of N . Next, the Somigliana stress formula (3.14) is used to obtain the stress distribution inside the domain. In fig.(8),(9), (10) the distribution of normalized stresses $\sigma_{r\theta}$, $\sigma_{\theta r}$ and couple stress m_{rz} respectively, are shown along the line $\theta = \pi/4$ for $l = a$, $\nu = 0.3$ and various values of N . As it can be seen from Figs.(7),(8),(9), (10) the results are in a good agreement with the analytical solution from [33]. Analytical solutions are shown in all plots by solid black lines.

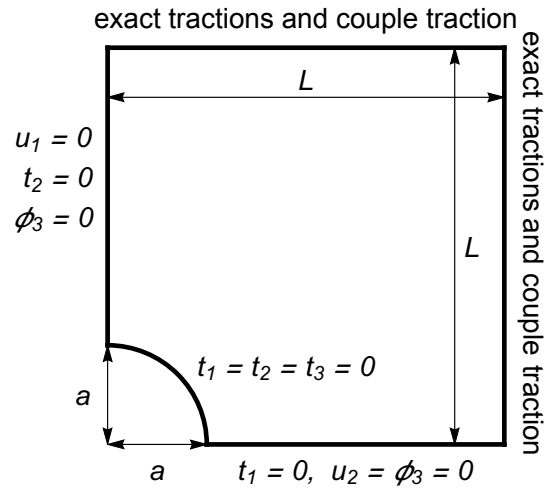


Figure 6. A quarter of a plate with a circular hole, $L = 4a$.

N	Analytical	DBIE	e(%)	TBIE	e(%)
0.10	2.9827	2.9819	0.03 %	2.9888	0.21 %
0.25	2.9528	2.9521	0.02 %	2.9580	0.17 %
0.50	2.9292	2.9289	0.01 %	2.9301	0.03 %
0.75	2.9187	2.9190	0.01 %	2.9113	0.25 %
0.90	2.9149	2.9161	0.04 %	2.9003	0.50 %

Table 3. Stress concentration factors for a circular hole: $l = 0.1a$.

(c) A Griffith crack

In the third example we consider a straight crack in an infinite plane in a uniform tension (Fig.11a) (known as a Griffith crack). The solution to this problem is a superposition of two solutions. The first one corresponds to an infinite uncracked plate in tension (Fig.11b) and the second solution is the one of a crack opened up by a uniform tension applied to the crack faces (Fig.11c). The solution to the first problem is given in [13] as

$$u_1 = \frac{1}{2} \frac{\sigma_0}{G} (-\nu x_1), \quad u_2 = \frac{1}{2} \frac{\sigma_0}{G} (1 - \nu) x_2, \quad \phi_3 = 0. \quad (5.7)$$

$$\sigma_{11} = \sigma_{12} = \sigma_{21} = 0, \quad \sigma_{22} = \sigma_0, \quad m_{13} = m_{31} = m_{23} = m_{32} = 0. \quad (5.8)$$

Therefore we only consider the problem of Fig.11c for BEM-modelling, i.e. the only BEM-boundary corresponds to the crack faces $\partial S = \Gamma = \Gamma_+ \cup \Gamma_-$ (Fig.12) with prescribed tractions:

$$t_1 = 0, \quad t_2 = -\sigma_0, \quad t_3 = 0, \quad -c < x_1 < c, \quad x_2 = 0. \quad (5.9)$$

In order to avoid the degenerated system matrix due to the coincident collocation points, we prescribe DBIE on Γ_+ and TBIE on Γ_- , an approach known as the dual boundary element method. The obtained results are compared with the analytical solutions obtained in [13]. Note, that the notations for N and l in [13] differ from the notations used here by the factor $\sqrt{2}$, therefore we rename material parameters from [13] as l^* , N^* . Therefore, $l^* = \sqrt{2}l$, $N^* = \sqrt{2}N$. We present the BEM-results in the same way as in [13], where the solutions are analyzed depending on two parameters: $\tau = \frac{l^*}{c}$ and $M = \frac{N^*}{\tau}$. The case $M = 1$ and $\nu = 0.25$ is chosen for comparison. In table

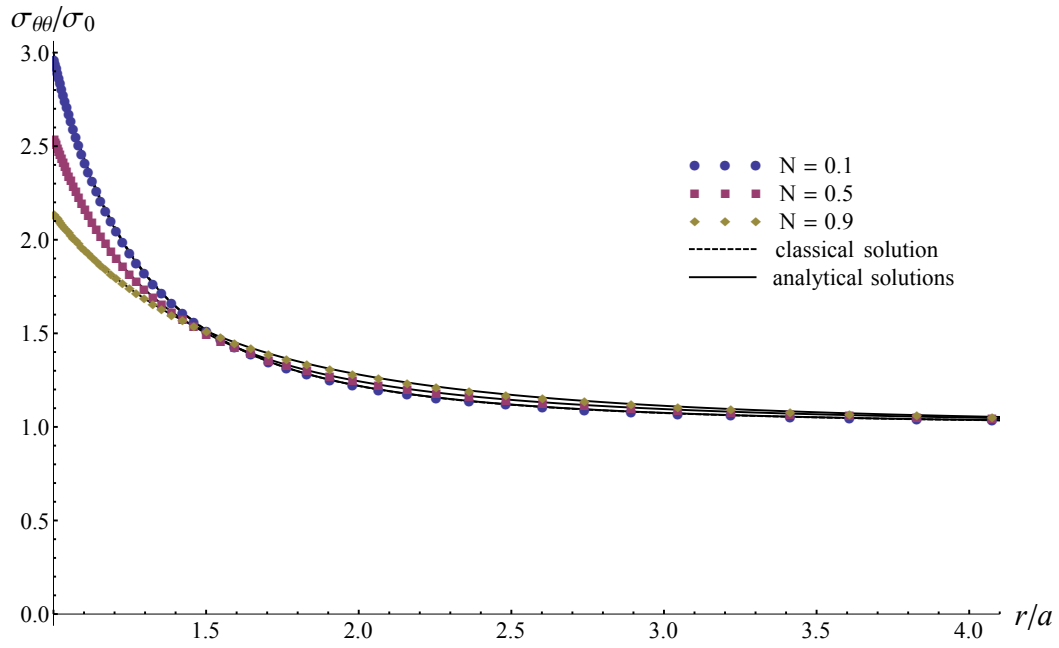


Figure 7. Distribution of normalized $\sigma_{\theta\theta}$ along $\theta = \frac{\pi}{2}$ for various values of coupling number N in comparison with the analytical solution [33].

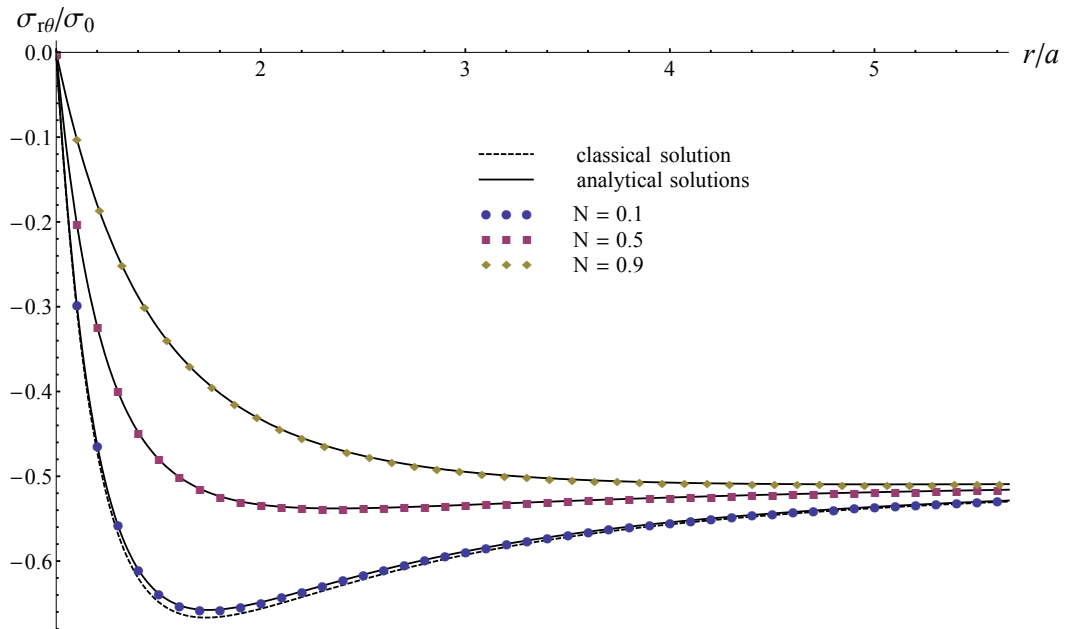


Figure 8. Distribution of normalized $\sigma_{r\theta}$ along $\theta = \frac{\pi}{4}$ for various values of coupling number N in comparison with the analytical solution [33].

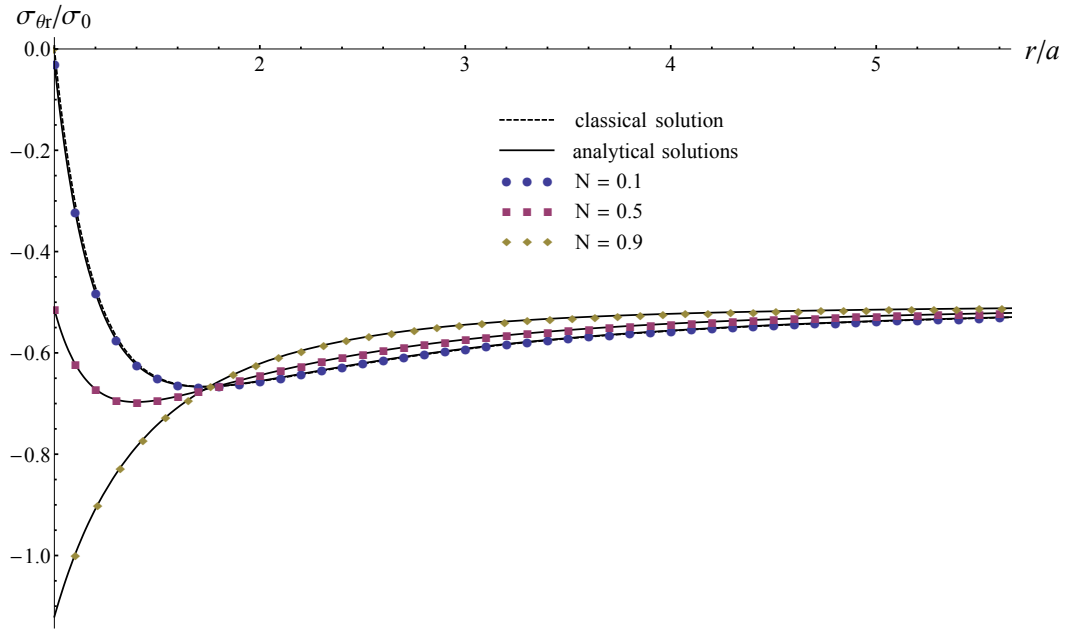


Figure 9. Distribution of normalized $\sigma_{\theta r}$ along $\theta = \frac{\pi}{4}$ for various values of coupling number N in comparison with the analytical solution [33].

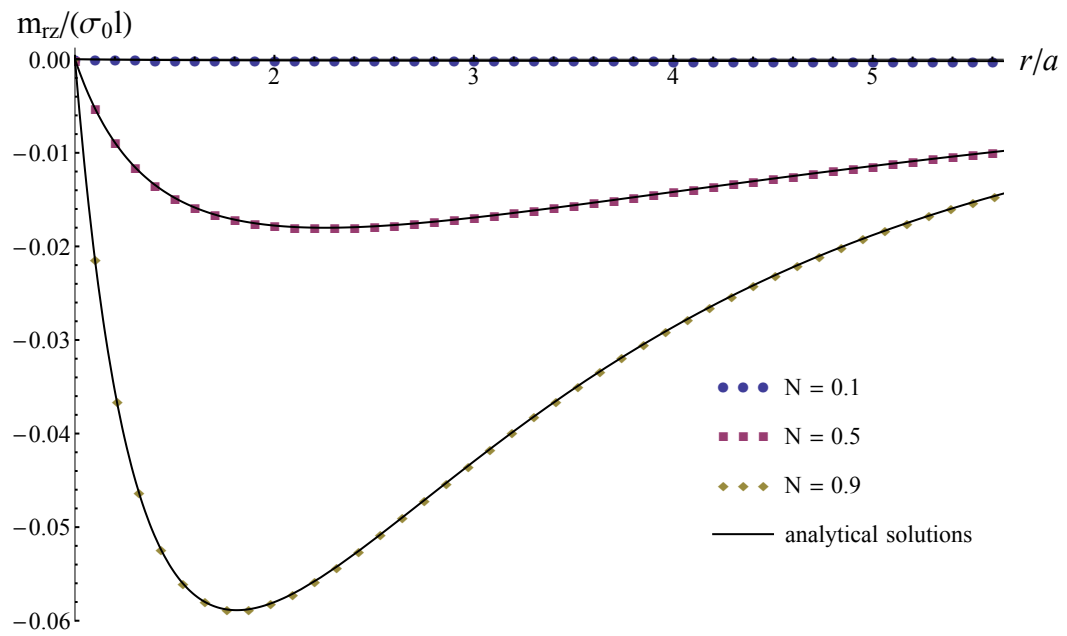


Figure 10. Distribution of normalized m_{rz} along $\theta = \frac{\pi}{4}$ for various values of coupling number N in comparison with the analytical solution [33].

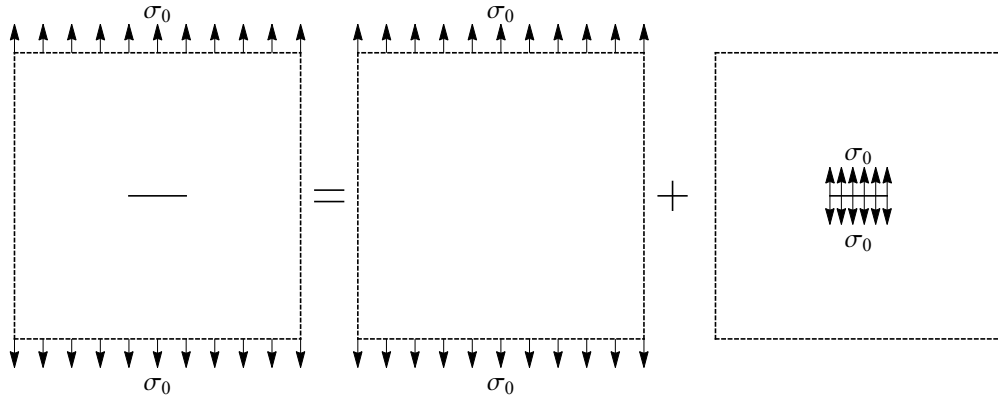


Figure 11. a) A through crack in an infinite plate in tension, b) uncracked plate in tension, c) crack opened up by a uniform tension.

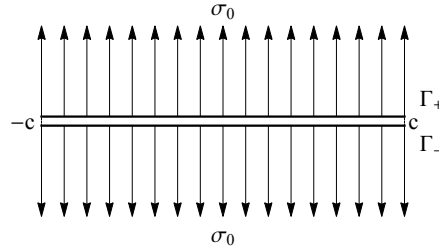


Figure 12. A crack opened up by a uniform tension.

4 the results are given in terms of four parameters. The first parameter is a value of the crack opening displacement at the center of the crack:

$$u_0 = \left(\frac{1}{2} \frac{\sigma_0}{G} \right)^{-1} c^{-1} u_2(0, 0) \quad (5.10)$$

The second parameter is characterized in [13] as "the mechanical energy required to form the crack" and given by

$$E_c = 2c\sigma_0 \int_0^1 u_2(r, 0) dr, \quad r = x_1/c, \quad \bar{E}_c = E_c / \left(\frac{1}{2} \pi (c\sigma_0)^2 (1 - \nu) / G \right) \quad (5.11)$$

Values of u_0 and \bar{E}_c are listed in table 4. Note, that value $\tau = 0.001$ was used in BEM to approximate the limiting case of classical elasticity. In all cases a fine mesh consisting of 196 elements, uniformly graded towards the crack tips, was used. The size of the mesh was chosen for the purpose of extracting stress intensity factors from the limiting values of the crack opening displacement as described below.

The stress intensity factor K_t and the couple-stress intensity factor K_m are defined as

$$\{K_t, K_m\} = \sqrt{2r} \lim_{r \rightarrow 1+} \{\sigma_{22}(r, 0), m_{23}(r, 0)\} \quad (5.12)$$

or in non-dimensional form

$$\bar{K}_t = K_t / (\sigma_0 \sqrt{c}), \quad \bar{K}_m = K_m / (\sigma_0 c \sqrt{c}) \quad (5.13)$$

τ	M	u_0 [13]	u_0 (BEM)	\bar{E}_c [13]	\bar{E}_c (BEM)
0.5	1	1.3022	1.3022	0.8646	0.8649
0.3	1	1.4222	1.4223	0.9467	0.9468
0.1	1	1.4909	1.4910	0.9938	0.9939
0.05	1	1.4977	1.4978	0.9984	0.9985
0	1	1.5000	1.5001	1.0000	1.0001

Table 4. Results for a problem of a Griffith crack.

The stress intensity factor K_t is directly expressed from the BEM-solution for the crack opening displacement $u_2(r, 0)$ according to its asymptotic expansion in the vicinity of the crack tip:

$$u_2(r, 0) = \frac{\sqrt{c}(1-\nu)K_t}{G(1+2(1-\nu)N^2)}\sqrt{1-r^2} + O(r). \quad (5.14)$$

In table 5 the values of K_t for various material parameters are compared with those in [13] and an agreement within 1% is shown.

Following the solution procedure in [13] the couple stress intensity factor K_m is derived as

$$K_m = c\sqrt{c}\sigma_0 \frac{1 - \bar{E}_c}{2}. \quad (5.15)$$

According to equations (5.11), (5.15), K_m for a Griffith crack is entirely defined by the integral of the crack opening displacement $u_2(r, 0)$, i.e. it can be obtained without using the asymptotics of the microrotation and couple-stress fields. This method allows to use coarser discretisation of the crack domain to obtain accurate K_m for all values of material parameters in comparison with the methods, which require fitting solutions near the crack tip.

Values of \bar{K}_t and \bar{K}_m are compared with the analytical solutions from [13] in table 5.

In fig.(13)-(14) the full solutions for the crack opening displacement and microrotations are plotted for various values of material parameters, and an excellent agreement between the analytical solutions of [13] and the BEM-data is seen.

Research in fracture mechanics of Cosserat materials (see for example, [34], [11], [35], [14]) indicates that both, displacements and microrotations in the vicinity of a crack tip have asymptotic expansions of order $\sqrt{\rho}$, where ρ is the distance to the crack tip. The asymptotic expansion of a microrotation in standard system of polar coordinates (ρ, θ) , associated with the crack tip, is given in [14] as:

$$\phi_3 = \frac{K_m\sqrt{2\rho}}{4l^2G} \sin \frac{\theta}{2} + O(\rho) \quad (5.16)$$

In Fig.15 the distribution of microrotations along the crack face is shown for $N = 0.9$ and varying values of parameter l/c together with the plot of the first term of eq.(5.16). Fig.15 illustrates the asymptotic property of microrotations, according to which, the asymptotic range of eq.(5.16) is

$$\rho \ll l, \quad (5.17)$$

i.e. the size of the domain dominated by the first term in (5.16) depends on material parameters and decreases with decreasing l . This behaviour indicates that in the extended finite and boundary element methods the adequate choice of the enrichment zone must significantly depend on the material parameters. However, the application of enriched Cosserat BEM and FEM need detailed study and remain subject of future work.

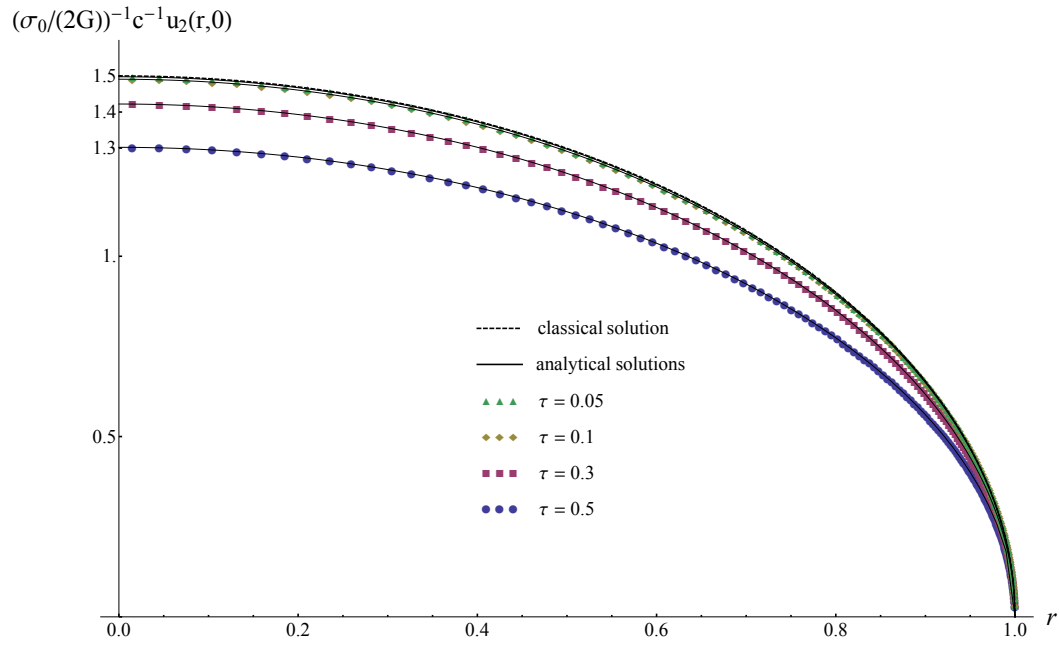


Figure 13. Crack opening displacement for different values of parameter $\tau = \sqrt{2}l/c$ in comparison with the analytical solutions [5].

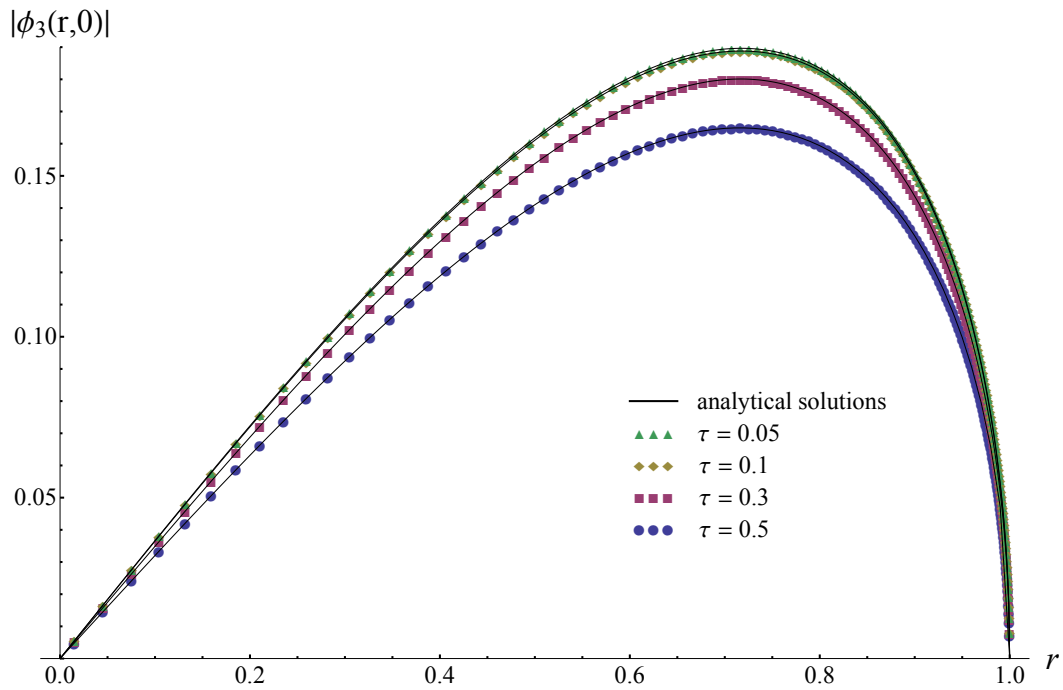


Figure 14. Variation of microrotations along the crack face for different values of parameter $\tau = \sqrt{2}l/c$ in comparison with the analytical solutions [5].

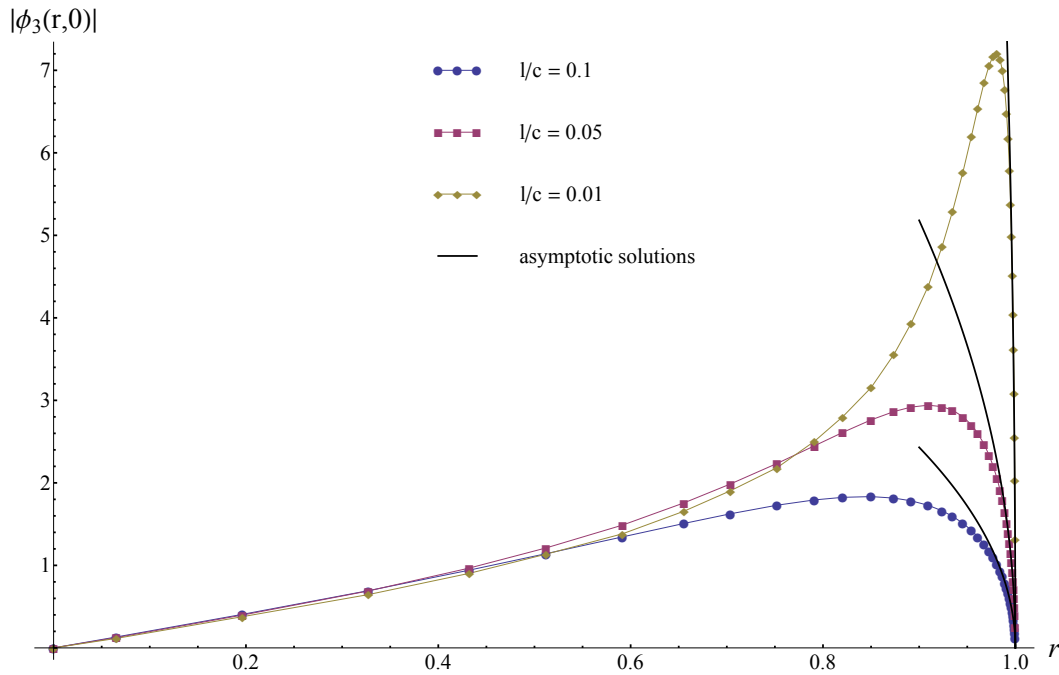


Figure 15. Variation of microrotations along the crack face for coupling number $N = 0.9$ and various values of material length l .

τ	M	\bar{K}_t [13]	\bar{K}_t (BEM)	relative error	\bar{K}_m [13]	\bar{K}_m (BEM)	relative error
0.5	1	1.0150	1.0222	0.71 %	0.0676	0.0676	0.06 %
0.3	1	1.0059	1.0100	0.41 %	0.0266	0.0266	0.02 %
0.1	1	1.0007	1.0013	0.06 %	0.0031	0.0031	1.13 %
0.05	1	1.0002	1.0004	0.02 %	0.0008	0.0007	7.84 %
0	1	1.0000	1.0001	0.01 %	0.0000	0.0000	- %

Table 5. Stress and couple stress intensity factors for a Griffith crack.

(d) A plate with an edge crack

In this example we consider the problem of a plate with an edge crack (Fig. 16) and compare our results with the FEM-data obtained in [14]. For the sake of comparison, we consider the same dimensions of the plate and the loading conditions, as in [14], i.e. the width of the plate $W = 11$ mm, height $2H = 20$ mm and the length of the crack $c = 1$ mm. The center of the coordinate system is placed at the crack tip and the polar coordinates (r, θ) are introduced. However, in order to avoid the rigid body motions, we impose slightly different Dirichlet condition than the one in [14], i.e. since in the collocation boundary element method, the boundary condition cannot be imposed at the crack tip, we fix the point $(10, 0)$ on the boundary of the plate, i.e.

$$u_1(10, 0) = u_2(10, 0) = \phi_3(10, 0) = 0. \quad (5.18)$$

All sides of the plate are assumed to be traction free, and the loading is applied to the crack faces. We consider two standard cases: in mode I the crack is opened up by the applied normal stress $\sigma_0 = 100$ MPa, i.e:

$$t_1 = 0, \quad t_2 = -\sigma_0 n_2, \quad t_3 = 0, \quad -c \leq x_1 \leq 0, \quad x_2 = 0. \quad (5.19)$$

Mode II corresponds to the applied shear stress $\sigma_0 = 100$ MPa, i.e.

$$t_1 = -\sigma_0 n_2, \quad t_2 = 0, \quad t_3 = 0, \quad -c \leq x_1 \leq 0, \quad x_2 = 0. \quad (5.20)$$

Material parameters were set to $E = 100$ GPa and $\nu = 0.3$.

In fig.17,18,19,20 we demonstrate the angular distributions of the stresses and couple-stresses (for an equivalent problem of a crack with the traction-free faces) defined as

$$f_{\alpha\beta}(\theta) = \sqrt{2\pi r} \sigma_{\alpha\beta}, \quad g_{\alpha z}(\theta) = \sqrt{2\pi r} m_{\alpha z} \quad \alpha, \beta = r, \theta \quad (5.21)$$

which are normalized in such a way that $f_{\theta\theta}(0) = g_{\theta z}(0) = 1$ in Mode I and $f_{\theta r}(0) = g_{rz}(0) = 1$ in Mode II. The remaining material parameters in fig.17,18,19,20 were taken $l = 0.025495$ mm, $N = 0.849837$, which correspond to parameters $\gamma = 100$ MPa and $\alpha/E = 1$ in [14]. The eq.5.21 were evaluated at $r = 10^{-5}$ mm. In Fig.17,18,19,20 the excellent agreement of the BEM-data with the analytical solutions, derived in [14] is shown for both loading modes. Note, that due to the zero boundary condition imposed in [14] for $\sigma_{r\theta}$ instead of $\sigma_{\theta r}$, our BEM-solution for $\sigma_{r\theta}$ corresponds to $\sigma_{\theta r}$ in [14], and $\sigma_{\theta r}$ corresponds to $\sigma_{r\theta}$ in [14]. Note, that according to [14], couple-stresses $m_{rz}, m_{\theta z}$ do not have a $1/\sqrt{r}$ -singularity in Mode II. This is in agreement with our BEM-calculations, as can be seen in Fig. 20, where as a direct implementation of eq.(5.21), we observe the BEM-data for the regular parts of $m_{rz}, m_{\theta z}$, which, according to [14], for fixed r , have the analytical form:

$$m_{rz} \sim \cos \theta, \quad m_{\theta z} \sim -\sin \theta. \quad (5.22)$$

Next, we compare our results in terms of the stress and couple stress intensity factors with those obtained in [14] by the finite element method. For comparison we have chosen the case of $N = 0.849837$ and the four values of the parameter $l = 0.025495, 0.254951, 0.806226, 2.54951$ corresponding to $\gamma = 10^2, 10^4, 10^5, 10^6$ in [14]. The results for both modes are given in Table 6. The data in table 6 was obtained by fitting the displacements the crack faces according to

$$u_2^I(r) = \frac{4(1-\nu^2)}{E(1+2N^2(1-\nu))} \frac{K_\sigma^I \sqrt{r}}{\sqrt{2\pi}} + O(\sqrt{r}), \quad u_1^{II}(\rho) = \frac{4(1-\nu^2)}{E(1+2N^2(1-\nu))} \frac{K_\sigma^{II} \sqrt{r}}{\sqrt{2\pi}} + O(\sqrt{r}) \quad (5.23)$$

in Mode I and Mode II respectively. Equations (5.23) were obtained from [14], however note, that there is a typo in their expression for u_r^{II} in eq.(72), which can be easily seen by integrating the Mode II-stresses from eq.(70) leading to the term $2(\mu + \alpha)(1 - \nu)$ instead of $2(\mu - \alpha)(1 - \nu)$ in eq.(72). The corrected constant is consisted with our BEM-data.

For all material parameters the same mesh with 193 elements on each crack face, gradually refined towards the crack tip was employed for the BEM analysis, and the data in the vicinity of $r = 10^{-3}l$ mm was used for fitting. The stress intensity factors in Table 6 were normalized as follows:

$$\bar{K}_\sigma^I = K_\sigma^I / k_I, \quad \bar{K}_\sigma^{II} = K_\sigma^{II} / k_{II}, \quad (5.24)$$

where $k_I = 208.1$ MPa·mm^{1/2}, $k_{II} = 199.3$ MPa·mm^{1/2} are the values corresponding to the Mode I and Mode II SIF-solutions for an edge-cracked specimen in the case of the classical elasticity.

The couple stress intensity factors were obtained by fitting the microrotations on the crack faces according to (5.16). The normalized couple stress intensity factors are given by

$$\bar{K}_m^I = K_m^I / (\sigma_0 c \sqrt{c}), \quad (5.25)$$

which differ with the definition in [14] by the factor of $\sqrt{\pi} \sigma_0 c \sqrt{c}$. Values of $\sqrt{\pi} \sigma_0 c \sqrt{c} \bar{K}_m^I$ are also provided in Table 6. The results in Table 6 are in a good agreement with the data in [14]. For the Mode I stress intensity factors the difference is estimated to be less than 1.2%, for the mode I couple stress intensity factors - less than 4.6% and for the mode II stress intensity factors - less than 2.3%. The difference in the results can be explained by the difference in the method of evaluating $K_\sigma^I, K_\sigma^{II}$ and K_m^I as well as by the slight difference in the boundary conditions.

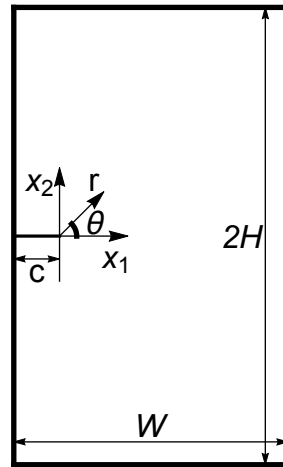


Figure 16. Edge crack in a rectangular plate.

N	l	\bar{K}_σ^I	\bar{K}_m^I	$\sqrt{\pi}\sigma_0 c \sqrt{c} \bar{K}_m^I$	\bar{K}_σ^{II}
0.849837	0.025495	1.1819	0.0270	4.79	1.4053
0.849837	0.254951	1.0803	0.2120	37.58	1.2272
0.849837	0.806226	0.9542	0.3689	65.39	1.0154
0.849837	2.549510	0.8836	0.4644	82.32	0.9222

Table 6. Stress and couple stress intensity factors for an edge crack in Mode I and Mode II.

6. Conclusions

This paper presented the derivation of the fundamental solutions for plane Cosserat elasticity and their application within a boundary element framework. Both singular and hypersingular boundary integral equations of plane Cosserat elasticity were formulated using these fundamental solutions and solved by the boundary element method. The dual BEM, developed in this work, was shown to be an accurate numerical tool which can be used for analysis of problems with singularities, such as certain crack problems without limitations on the geometry or the type of the loading conditions. The excellent accuracy of the method was demonstrated on the classical example of a Griffith crack. The approach can be further used to model crack propagation in micropolar materials and can be extended to the three-dimensional case. The accuracy of the method for crack problems can be further improved, for a given number of degrees of freedom, by incorporating crack tip enrichments into the approximation space which can be derived from the asymptotic behavior of the displacements and microrotations in the vicinity of a crack tip, also studied within this paper. This approach is known as the eXtendend BEM and is the subject of further study.

Acknowledgment

The work presented in this paper was partially supported by Fondecyt Chile grant number 11130259 entitled "Boundary element modeling of crack propagation in micropolar materials".

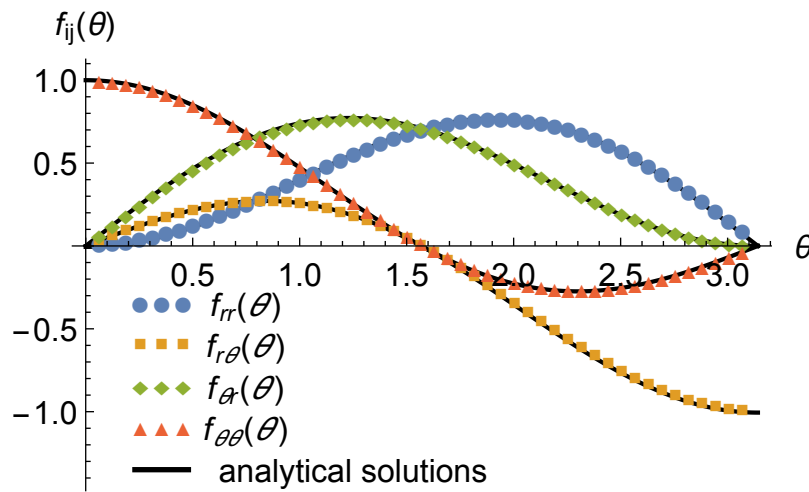


Figure 17. Edge crack in Mode I: Angular distribution of stresses around the crack tip in comparison with the analytical solutions [14].

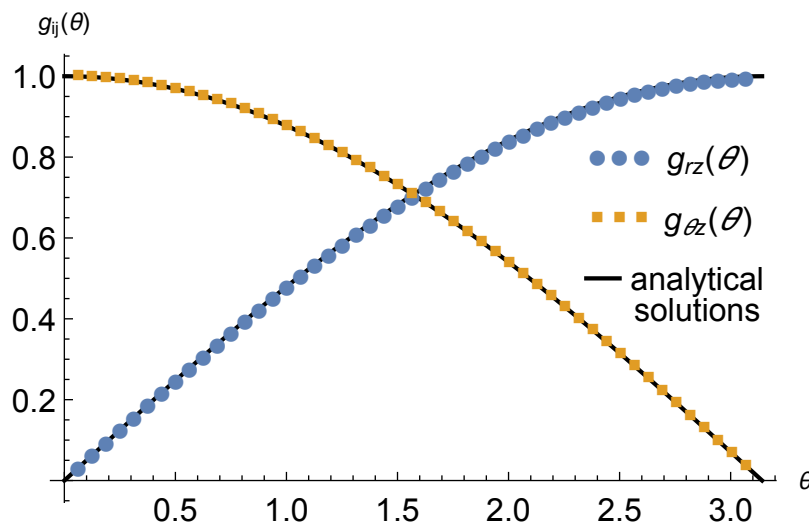


Figure 18. Edge crack in Mode I: Angular distribution of couple-stresses around the crack tip in comparison with the analytical solutions [14].

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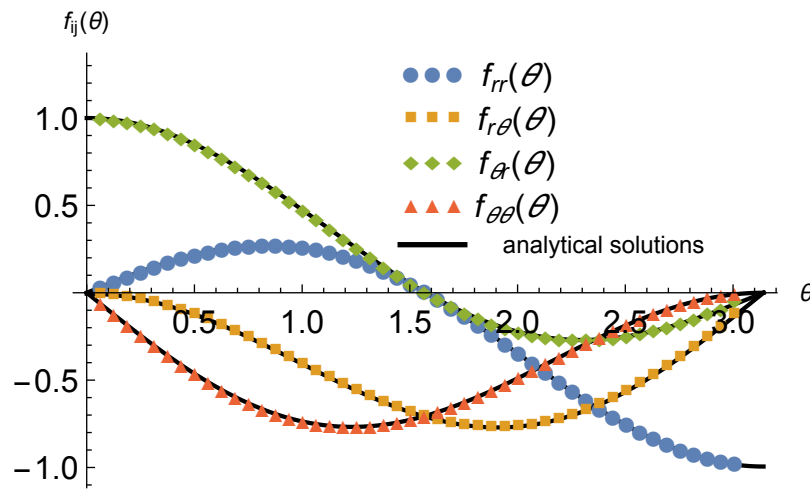


Figure 19. Edge crack in Mode II: Angular distribution of stresses around the crack tip in comparison with the analytical solutions [14].

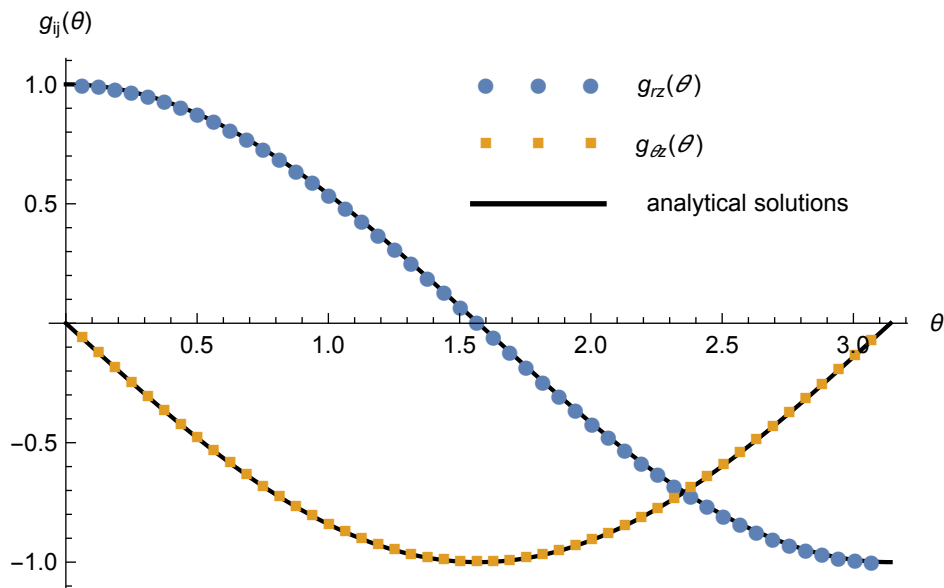


Figure 20. Edge crack in Mode II: Angular distribution of couple-stresses around the crack tip in comparison with the analytical solutions [14].

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