



Institute of Structural Mechanics

The Three Dimensional Extended Bridging Domain Method (XBDM) for Modelling Dynamic Fracture

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Outline

- Motivation
- The eXtended Bridging Domain Method
- Setup and Implementation
- Verification and Validation
- Numerical Examples
- Discussion
- Conclusion and Future Work

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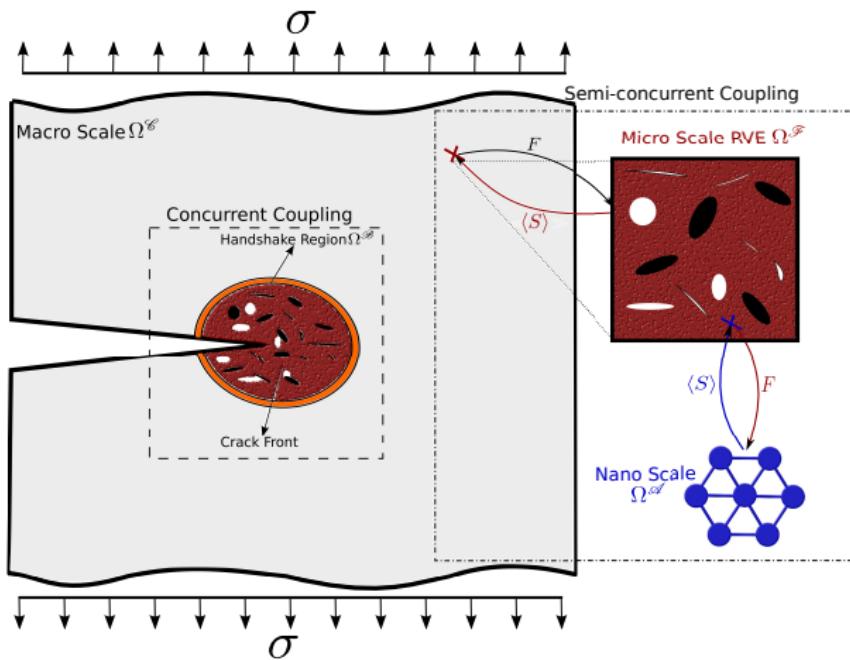
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- In fracture simulation, crack and dislocation propagation should be confined around the crack tip
- We focus on the Arlequin type methods which is suitable for dynamic fracture
- For MD–XFEM coupling it is called *eXtended Bridging Domain Method (XBDM)*

Multiscale methods



Semi-concurrent and Concurrent multiscale methods

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 - ii. Cauchy-Born method can be used for material behavior

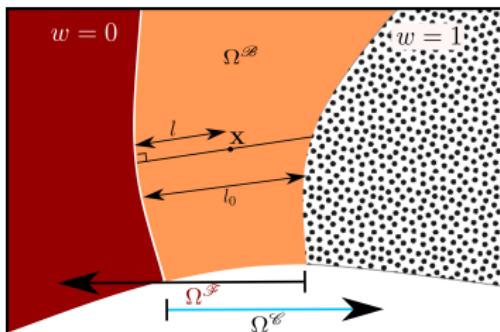
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- Coupling is enforced with the Lagrange multipliers
- Ghost atoms move with the continuum

The Coupling Method



weighting function

$$w(\mathbf{X}) = \begin{cases} 1 & \forall \mathbf{X} \in \Omega^C \setminus \Omega^F \\ [0, 1] & \forall \mathbf{X} \in \Omega^B \\ 0 & \forall \mathbf{X} \in \Omega^F \setminus \Omega^C. \end{cases}$$

$$w(\mathbf{X}) = \frac{l(\mathbf{X})}{l_0}$$

Governing Equations

The governing equations are derived from the Hamiltonian of both systems:

$$H = wH^{\mathcal{F}} + (1 - w)H^{\mathcal{C}} = \sum_{\alpha} (w(\mathbf{X}_{\alpha})) \frac{\mathbf{P}_{\alpha}^{\mathcal{F}} \cdot \mathbf{P}_{\alpha}^{\mathcal{F}}}{2m_{\alpha}} + (w)W^{\mathcal{F}} + \sum_I (1 - w)(\mathbf{X}_I) \frac{\mathbf{P}_I^{\mathcal{C}} \cdot \mathbf{P}_I^{\mathcal{C}}}{2M_I} + (1 - w)W^{\mathcal{C}}$$

In the Lagrange multiplier method, the total Hamiltonian is:

$$H_L = H + \lambda^T \mathbf{g}$$

And \mathbf{g} is the gap vector between the displacements.

Governing Equations

In explicit dynamics the semi-discrete equations are:

$$M_{IJ} \ddot{u}_{Ji} = f_{li}^{\text{ext}} - f_{li}^{\text{int}} + f_{li}^{\lambda \mathcal{C}}$$

$$m_{\alpha}^{\mathcal{F}} \ddot{d}_{\alpha i}^{\mathcal{F}} = f_{\alpha i}^{\mathcal{F}} + f_{\alpha i}^{\lambda \mathcal{F}}$$

$$M_{IJ} = \int_{\Omega_0^{\mathcal{C}}} (1 - w) \rho_0 N_I N_J d\Omega_0^{\mathcal{C}} ,$$

Internal forces in continuum:

$$f_{li}^{\text{int}} = \int_{\Omega_0^{\mathcal{C}}} (1 - w) P_{ij} \frac{\partial N_I}{\partial X_j} d\Omega_0^{\mathcal{C}} ,$$

Governing Equations

The forces on each atom are determined from the interatomic potential W as:

$$f_{\alpha i}^{\mathcal{F}} = - \sum_{\beta} \frac{1}{2} (w(X_{\alpha}) + w(X_{\beta})) \frac{\partial W(r_{\alpha\beta})}{\partial d_{i\beta}^{\mathcal{F}}} ,$$

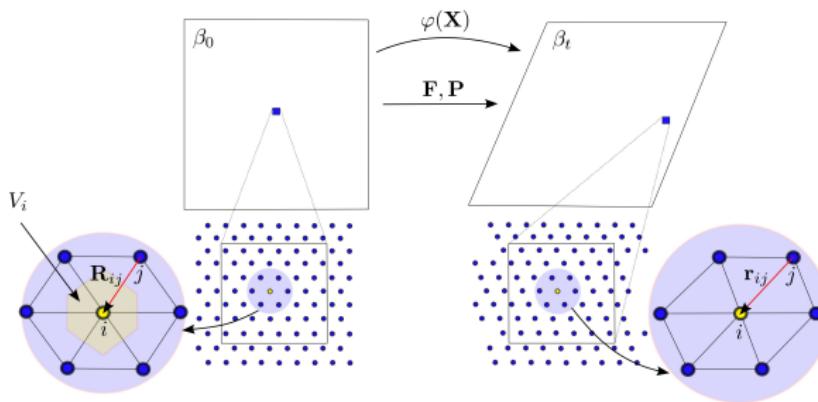
The coupling forces on the fine and coarse scales are:

$$f_{li}^{\lambda \mathcal{C}} = \sum_{\alpha \in \Omega_0^{\mathcal{B}}} \lambda_{\alpha i} N_l(X_{\alpha}), \quad f_{\alpha i}^{\lambda \mathcal{F}} = -\lambda_{\alpha i}$$

The displacement approximation with XFEM is

$$\mathbf{u}^h(\mathbf{X}) = \underbrace{\sum_{l \in \mathcal{N}} N_l(\mathbf{X}) \mathbf{u}_l}_{\mathbf{u}^{\text{cont}}} + \underbrace{\sum_{l \in \mathcal{N}_b} N_l(\mathbf{X}) H(f_l(\mathbf{X})) \mathbf{a}_l}_{\mathbf{u}^{\text{discont}}}$$

Cauchy-Born Rule



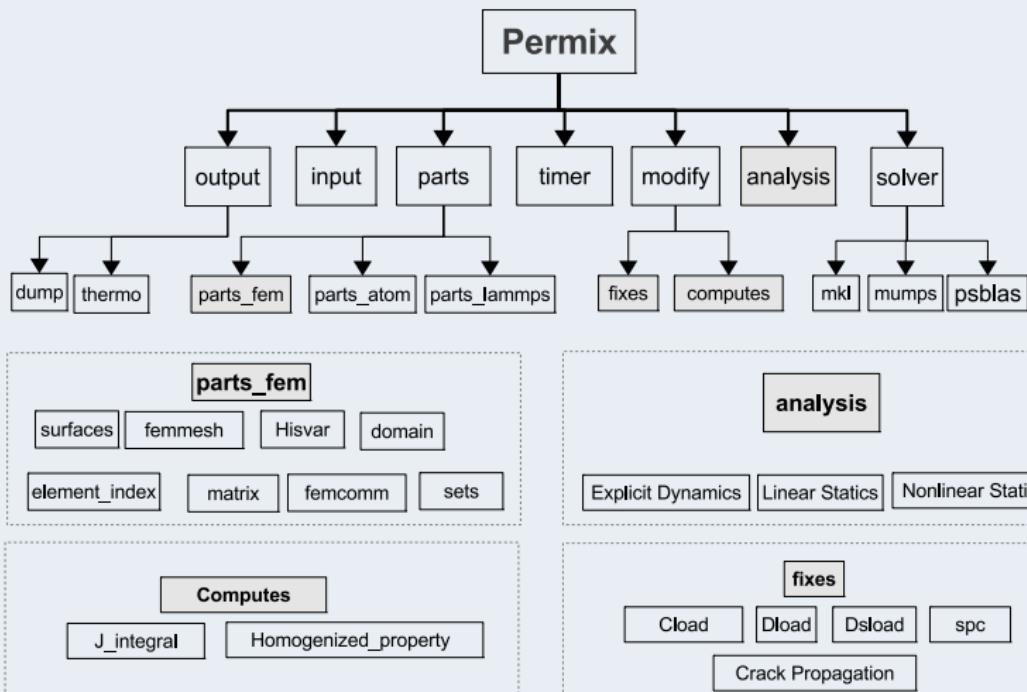
1st Piola-Kirchhoff stress tensor and 4th tangent operator

$$\mathbf{P}_i \doteq \frac{1}{2V_i} \sum_{j \neq i} \mathbf{f}_{ji} \otimes \mathbf{R}_{ij}, \quad \mathbf{C} \doteq \frac{\partial^2 W_0}{\partial \mathbf{F} \otimes \partial \mathbf{F}}$$

Problem Setup

- 1. Read the coarse and fine scale model definitions
- 2. Minimize the potential energy of the atomistic part
- 3. Build the neighbor lists for the coarse scale
- 4. Find all the atoms in all elements
- 5. Find active elements, bridging elements and nodes
- 6. Compute the weights of the nodes and integration points
- 7. Find active atoms, bridging atoms and ghost atoms
- 8. Recompute coarse and fine scale masses
- 9. Set up the Lagrange multiplier points
- 10. Compute the coupling matrix

A Platform for Multiscale Analysis

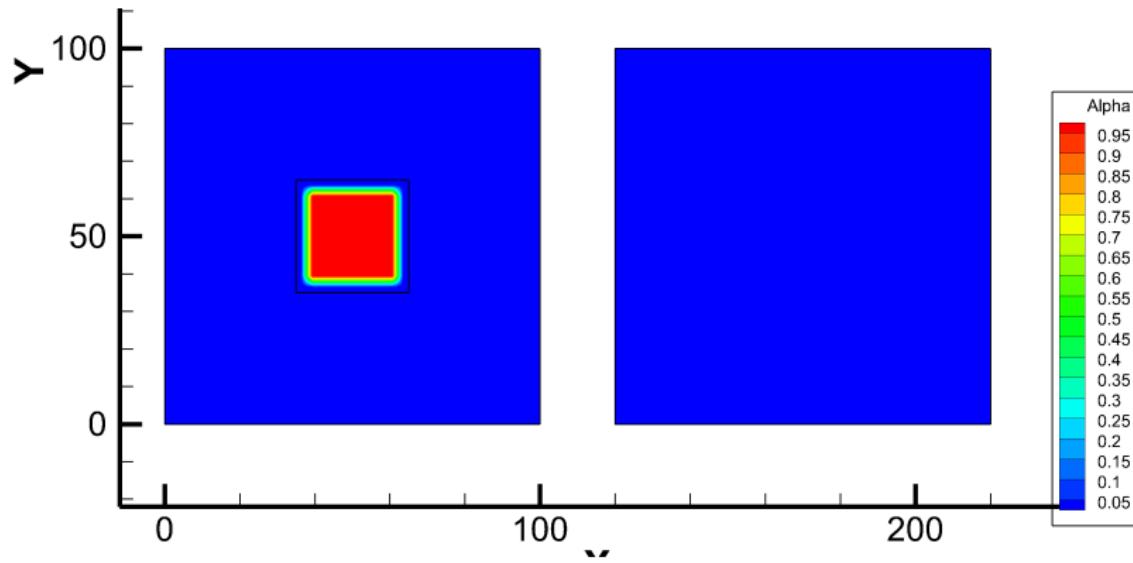


Major PERMIX Features

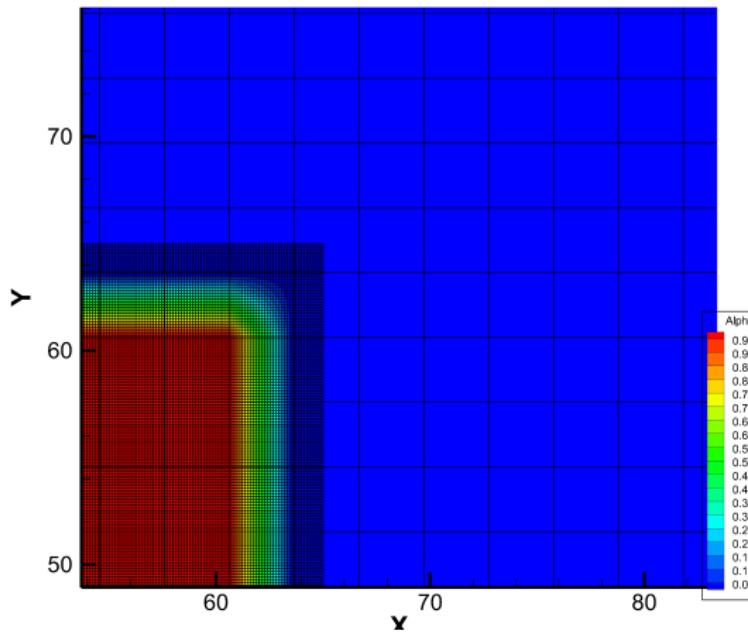
- Fully extensible object oriented Fortran 2003 compliant
- Parallel MD part (LJ, EAM, MEAM) based on WARP
- An F03 interface for LAMMPS (C++ version).
- 2 and 3 dimensional Extended Finite Elements.
- Explicit Dynamic and Nonlinear Static Solver
- Coupling FE–XFEM and XFEM–MD using Arlequin method
- Can handle semi-concurrent multiscale methods
- Material models, boundary conditions and loading types
- Interface to many libraries such as TETGEN, GEOPACK, MUMPS, MKL, etc.

Verification Example 1

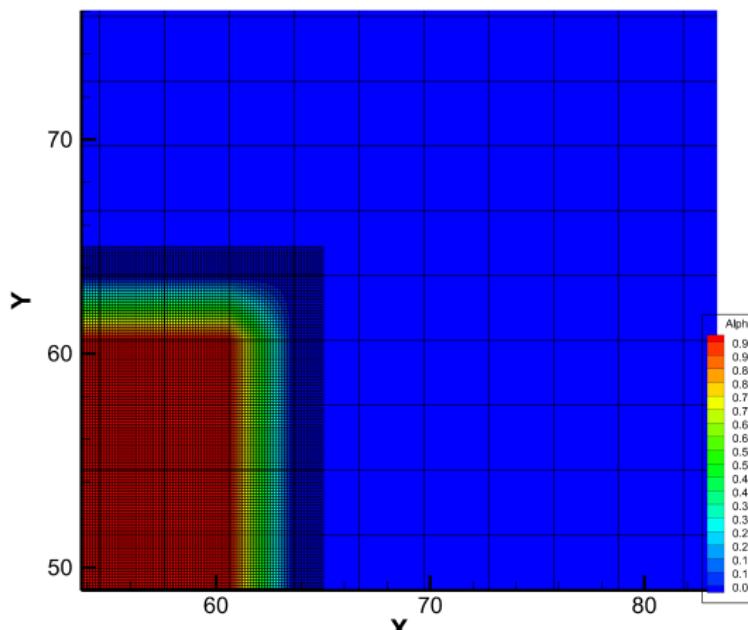
Dynamic FE-FE coupling



Verification Example 1: Zoom



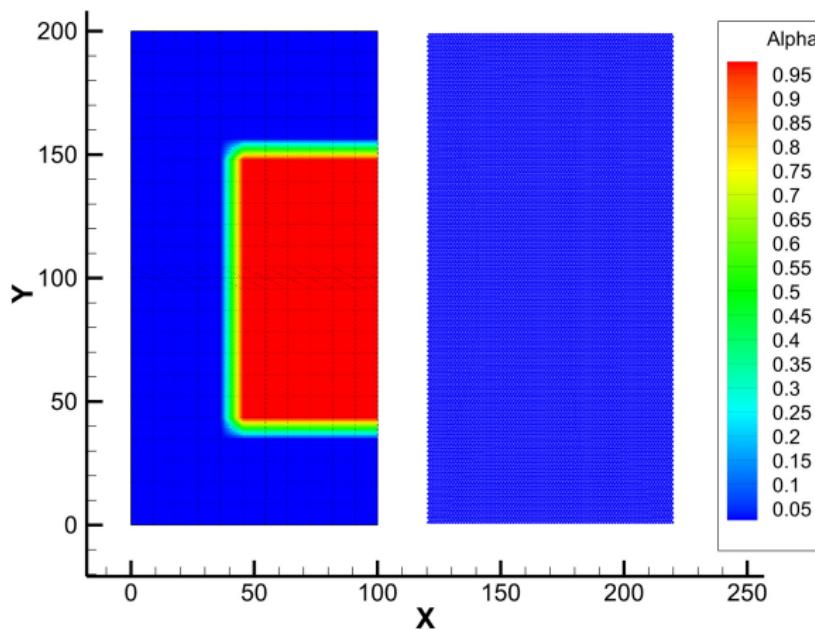
Verification Example 1: Zoom



Results: Movie 1

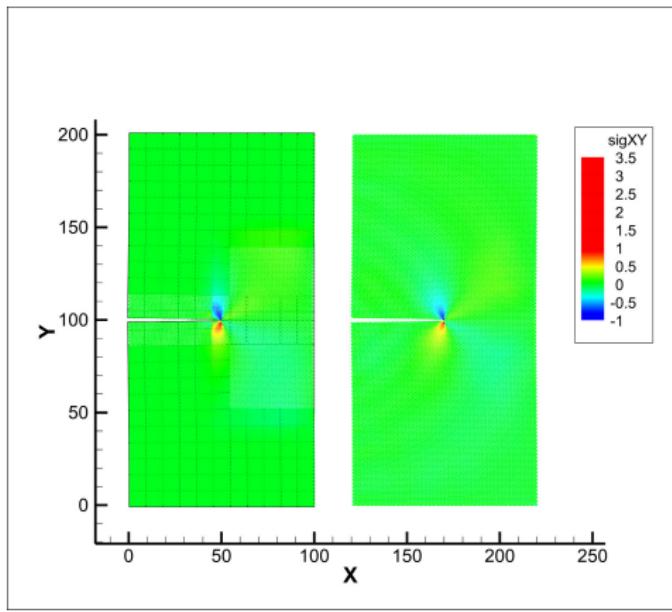
Verification Example 2

Dynamic XFEM-MD coupling in 2D



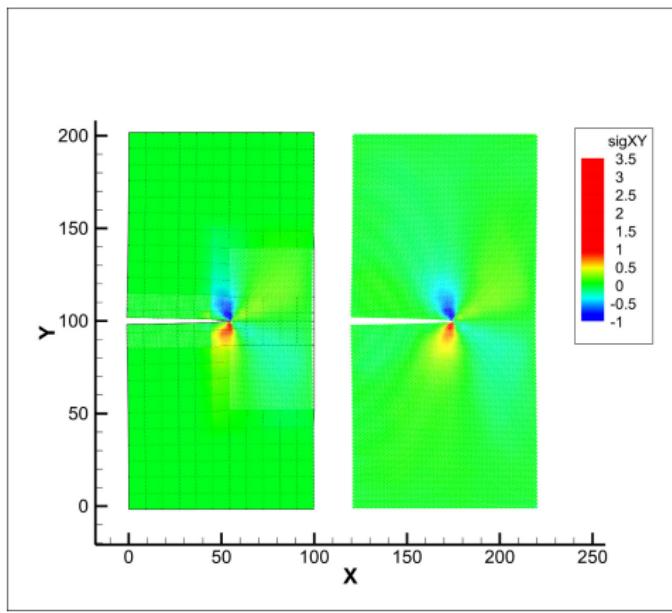
Verification Example 2

Results: Virial Stress is shown



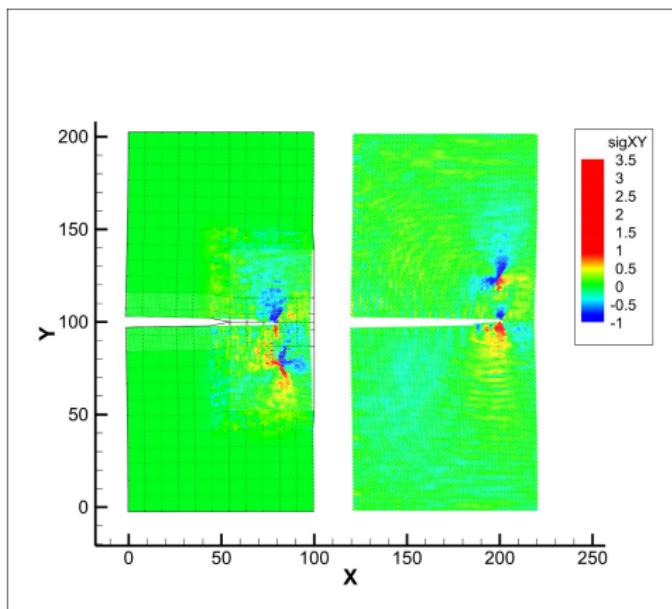
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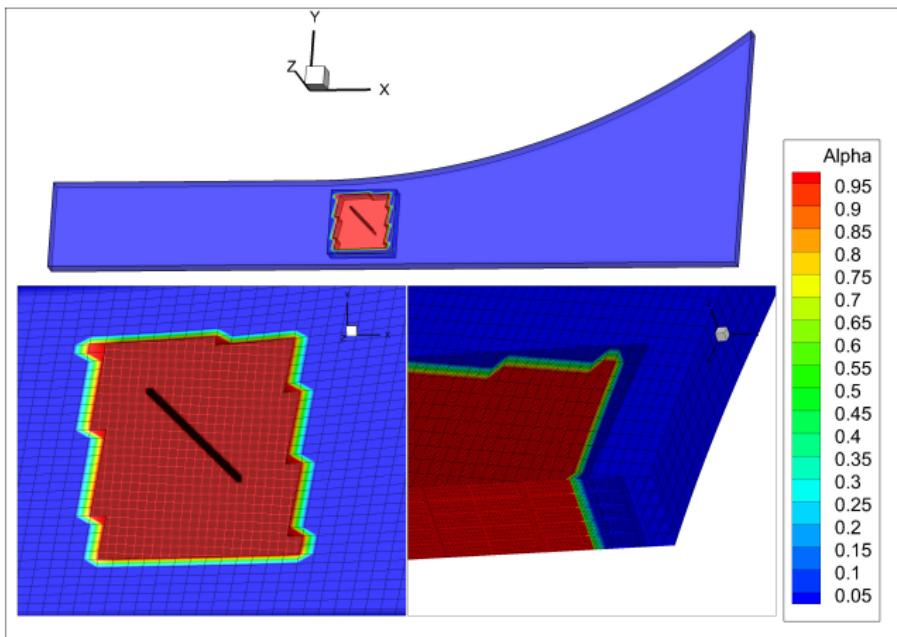
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Numerical Examples

Example 1: 3D FE-XFEM Coupling

Initial Configuration



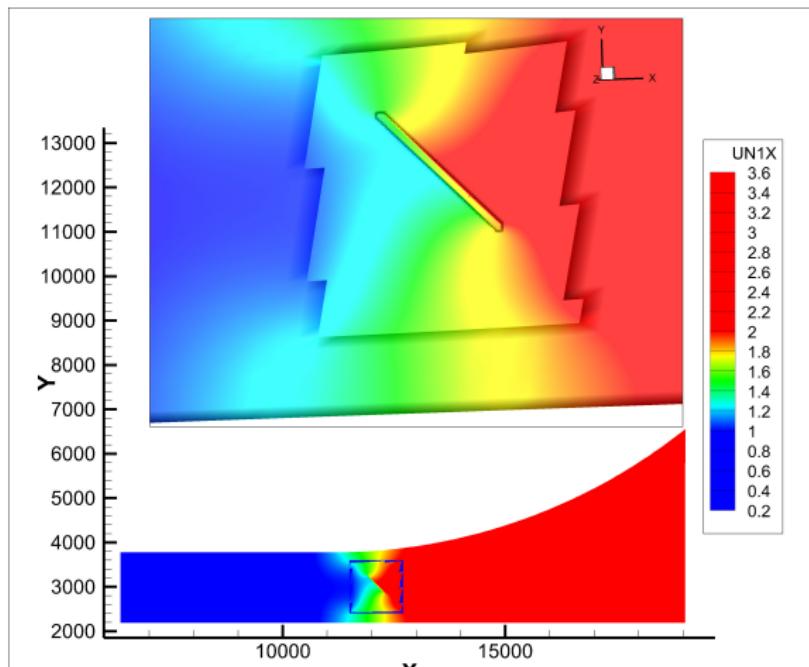
Example 1: 3D FE-XFEM Coupling

Simulation Details

- A 3D dogbone specimen in dynamic explicit
- Coarse scale has 33,735 elements and 41,760 nodes.
- Fine scale has 427,500 elements and 456,020 nodes.
- A linear elastic material model is used.
- The right hand side is loaded with pressure.
- Can be applied to multiscale problems.
- No complicated meshing-remeshing tools/algorithms are needed.

Example 1: FE-XFEM Coupling

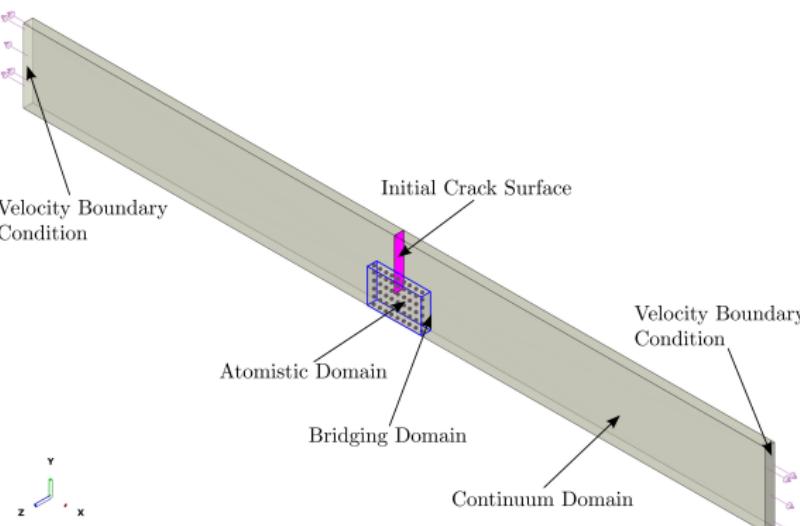
Displacement Contour, Movie 2



Numerical Examples

Example 2: MD-XFEM Coupling

Example 2: Coupled MD-XFEM



Example 2: MD-XFEM Coupling

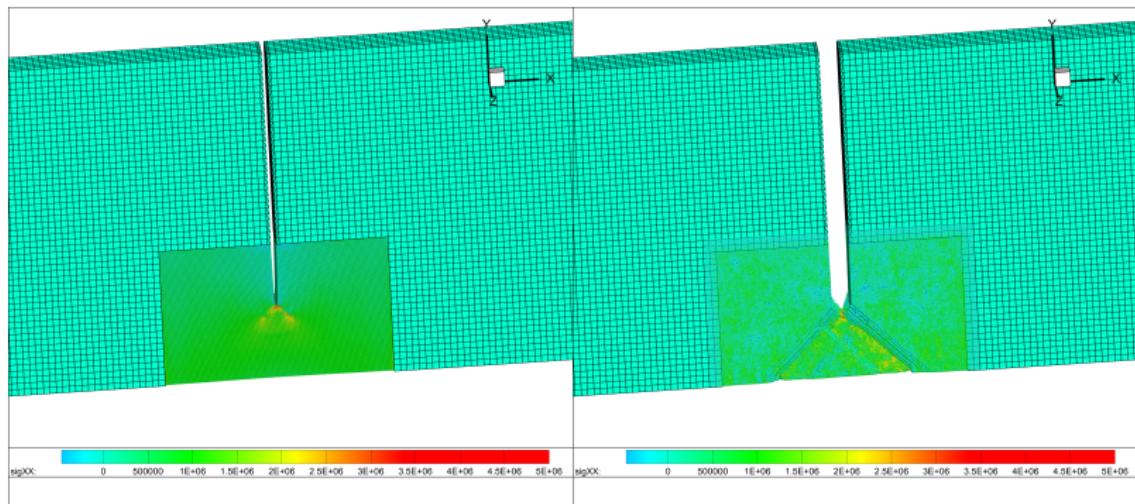
Simulation Details

- A 3D rectangular specimen (8000x800x100³)
- LAMMPS is used for MD part
- Cauchy-Born method for continuum material
- Crack length 620
- 197,743 elements and 692,064 DOFs.
- Atomistic domain is FCC lattice with constant 3.645
- Atomistic region has the size of 540x340x100A3 with 1,626,240 active and 166,815 bridging atoms.
- Lennard-Jones constants are: $\sigma = 2.29$ and $\epsilon = 0.467$ eV
Velocity of 0.1 Å/picoseconds applied to both ends, time step is .003 picoseconds.

Example 2: MD-XFEM Coupling 1

Results at time steps: 32400,63400

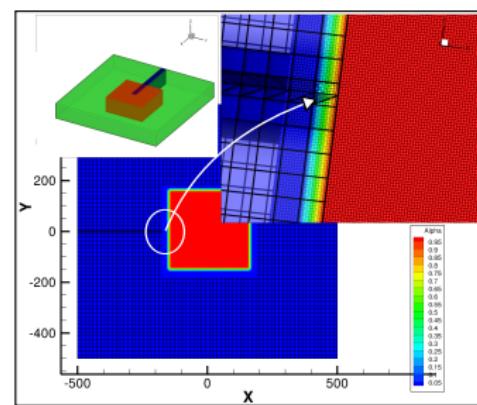
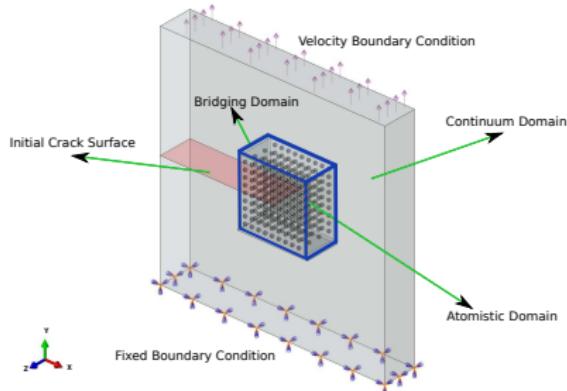
Movie 3



Numerical Examples

Example 3: MD-XFEM Coupling 2

Coupled MD-XFEM using LAMMPS



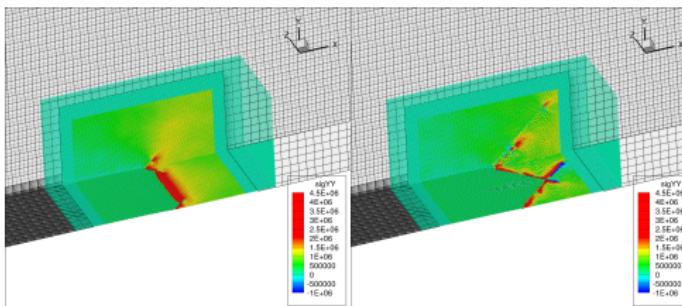
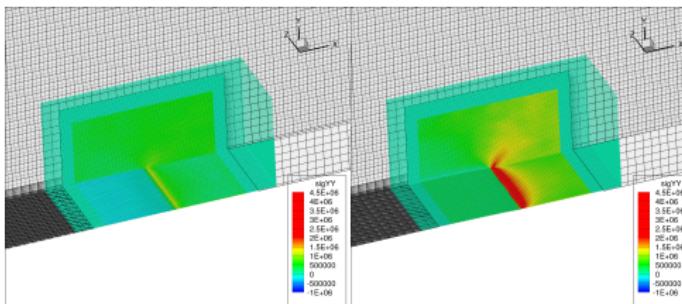
Example 3: MD-XFEM Coupling

Simulation Details

- A 3D rectangular specimen (1000x1000x150A3)
- Cauchy-Born method for continuum material
- Crack length 620A
- 44,890 elements and 152,592 DOFs.
- Element size is 15A
- Atomistic domain is FCC lattice with constant 3.645A
- Atomistic region has the size of 310x310x150A3 with 1,368,575 active atoms
- Velocity B.C. on top nodes

Example 3: MD-XFEM Coupling

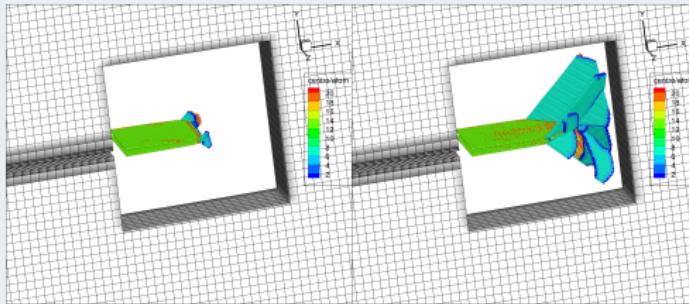
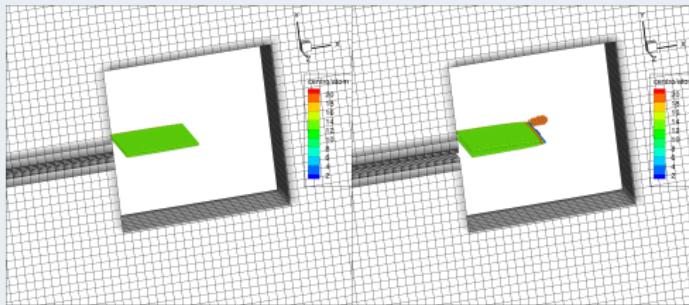
Results at time steps: 10000,33000,34000,35800



Numerical Examples

Example 3: MD-XFEM Coupling Results (Movie 4)

Results at time steps: 10000,33000,34000,35800



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- In XFEM-MD coupling, dislocations should be handled when they propagate close to the continuum domain
 - I. Adaptive refinement of the atomistic domain
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 - III. CG method of Y. Chen et al.
(A concurrent scheme for passing dislocations from atomistic to continuum domains, Acta Materialia, 2012)

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(A concurrent scheme for passing dislocations from atomistic to continuum domains, Acta Materialia, 2012)
- Cauchy-Born method is not always valid
 - I. Strain range, II. Surface effects, III. Temperature range, IV. Material, V. Efficiency

Discussion

- Modeling higher temperatures
- Isothermal simulations can be done with the current method
- A strain rate, temperature dependent material model should be used at the coarse scale
- Computing the material model can be automated based on a hierarchical multiscale method
- Polymeric materials can be modeled with this method

Conclusions and Future Plans

- An extended bridging domain method was presented.
- A multiscale software framework was introduced.
- The verification examples show that the method is stable in dynamics in both FE-FE coupling and FE-MD coupling.
- A comparison between full MD and coupled FE-MD
- Several examples modeling crack propagation was shown.
- Handling dislocation propagating to the continuum domain was discussed.

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- A comparison between full MD and coupled FE-MD
- Several examples modeling crack propagation was shown.
- Handling dislocation propagating to the continuum domain was discussed.
- Future work includes isothermal multiscale simulations, and extension to other materials.
- Efficient parallelization for distributed memory systems is also another challenge.

Conclusions

Thanks you for your attention.

Collaborators:

Prof. Timon Rabczuk (Bauhaus – Supervisor)

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M.S. Mohammad Silani (IUT)