

# A new variant of the differential gravimetry approach



Matthias Weigelt, Tonie van Dam



Tamara Bandikova

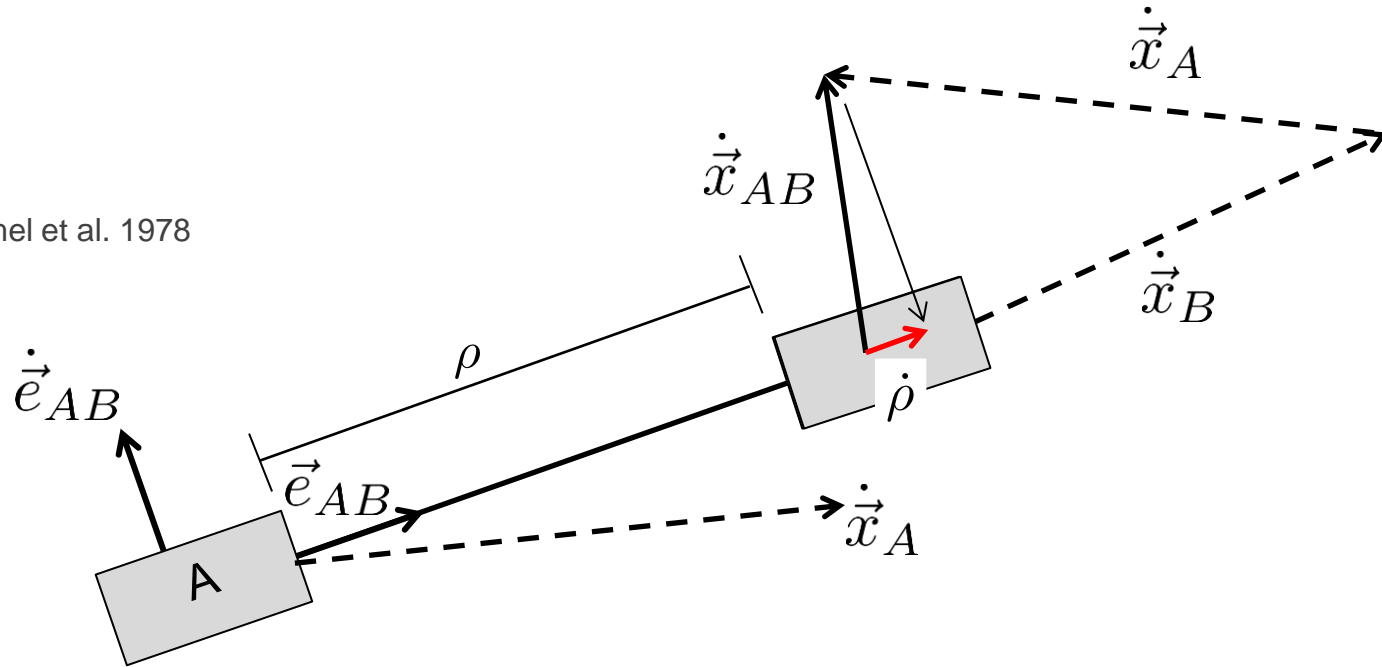
RUES

RESEARCH UNIT  
IN ENGINEERING  
SCIENCES



# Geometry of the GRACE system

Rummel et al. 1978



**Differentiation**

**Integration**

$$\rho = \vec{x}_{AB} \cdot \vec{e}_{AB}$$

$$\dot{\rho} = \dot{\vec{x}}_{AB} \cdot \vec{e}_{AB}$$

$$\ddot{\rho} = \ddot{\vec{x}}_{AB} \cdot \vec{e}_{AB} + \dot{\vec{x}}_{AB} \cdot \dot{\vec{e}}_{AB} \\ = \nabla V_{AB}$$

# Solution strategies

## Variational equations

Classical  
(Reigber 1989, Tapley 2004)

$$\rho, \dot{\rho}$$

Celestial Mechanics approach  
(Beutler et al. 2010, Jäggi 2007)

$$\rho, \dot{\rho}, \Delta\rho$$

Short-arc method  
(Mayer-Gürr 2006)

$$\rho, \dot{\rho}$$

...

## In-situ observations

Energy Integral  
(Han 2003, Ramillien et al. 2010)

$$\dot{\rho}$$

Differential gravimetry  
(Liu 2010)

$$\ddot{\rho}$$

LoS Gradiometry  
(Keller and Sharifi 2005)

$$\frac{\ddot{\rho}}{\rho}$$

...

# DIFFERENTIAL GRAVIMETRY

## THE STANDARD APPROACH

# Differential gravimetry

Range observables:  $\vec{x}_{AB} = \rho \vec{e}_{AB}^a$

# Differential gravimetry

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$$\dot{\vec{x}}_{AB} = \dot{\rho} \vec{e}_{AB}^a + \rho \dot{\vec{e}}_{AB}^a$$

# Differential gravimetry

Range observables:  $\vec{x}_{AB} = \rho \vec{e}_{AB}^a$

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$$\ddot{\vec{x}}_{AB} = \ddot{\rho} \vec{e}_{AB}^a + 2 \dot{\rho} \dot{\vec{e}}_{AB}^a + \rho \ddot{\vec{e}}_{AB}^a$$

# Differential gravimetry

Range observables:  $\vec{x}_{AB} = \rho \vec{e}_{AB}^a$

$$\dot{\vec{x}}_{AB} = \dot{\rho} \vec{e}_{AB}^a + \rho \dot{\vec{e}}_{AB}^a$$

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Multiplication with unit vectors in along-track, cross-track and radial direction:

$$\ddot{\vec{x}}_{AB} \cdot \vec{e}_{AB}^a = \ddot{\rho} + 0 + \rho \ddot{\vec{e}}_{AB}^a \cdot \vec{e}_{AB}^a$$

$$\ddot{\vec{x}}_{AB} \cdot \vec{e}_{AB}^c = 0 + 0 + \rho \ddot{\vec{e}}_{AB}^a \cdot \vec{e}_{AB}^c$$

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Multiplication with unit vectors in along-track, cross-track and radial direction:

**GRACE**

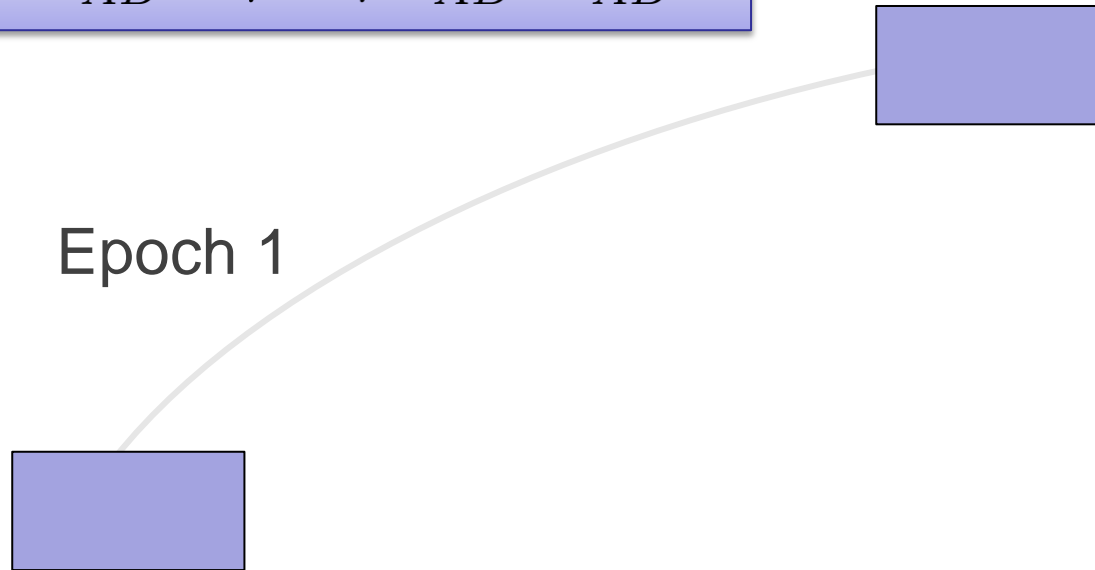
$$\ddot{\vec{x}}_{AB} \cdot \vec{e}_{AB}^a = \ddot{\rho} + 0 + \rho \ddot{\vec{e}}_{AB}^a \cdot \vec{e}_{AB}^a$$

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# Relative motion

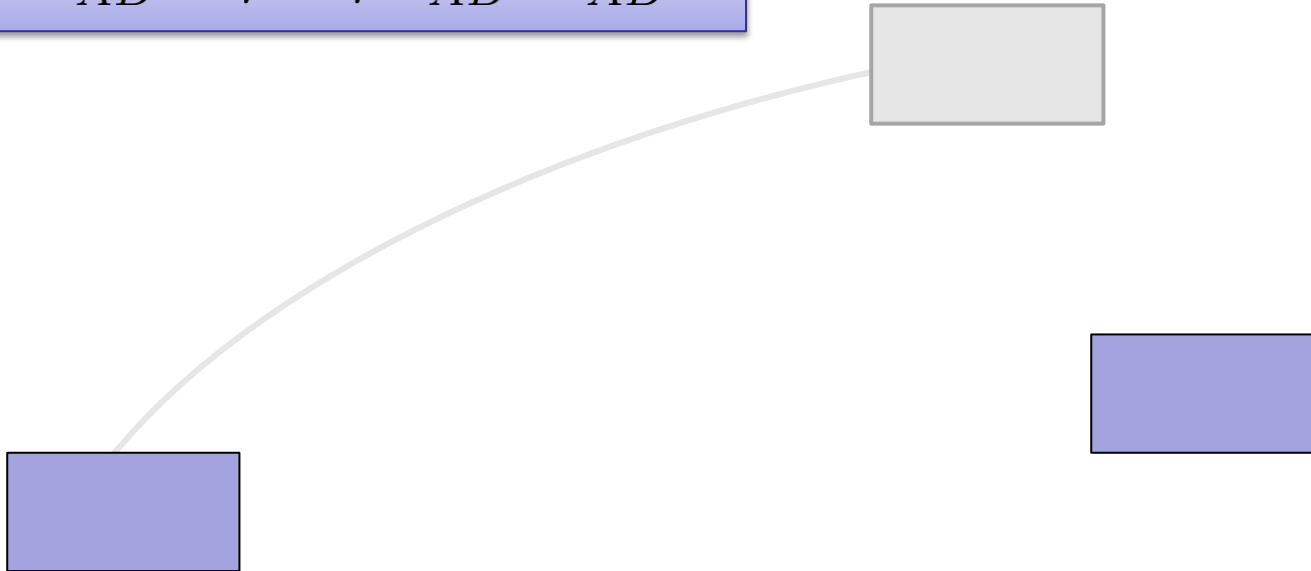
$$\ddot{\vec{x}}_{AB} \cdot \vec{e}_{AB}^a = \ddot{\rho} + \rho \ddot{\vec{e}}_{AB}^a \cdot \vec{e}_{AB}^a$$



# Relative motion

absolute motion neglected!

$$\ddot{\vec{x}}_{AB} \cdot \vec{e}_{AB}^a = \ddot{\rho} + \rho \ddot{\vec{e}}_{AB}^a \cdot \vec{e}_{AB}^a$$

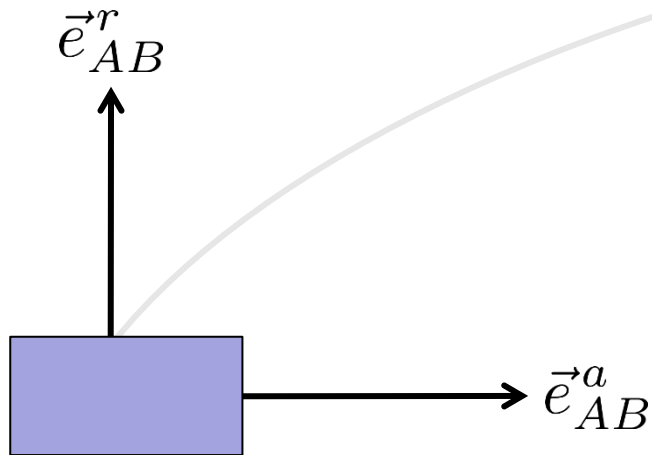


Epoch 2

# Relative motion

absolute motion neglected!

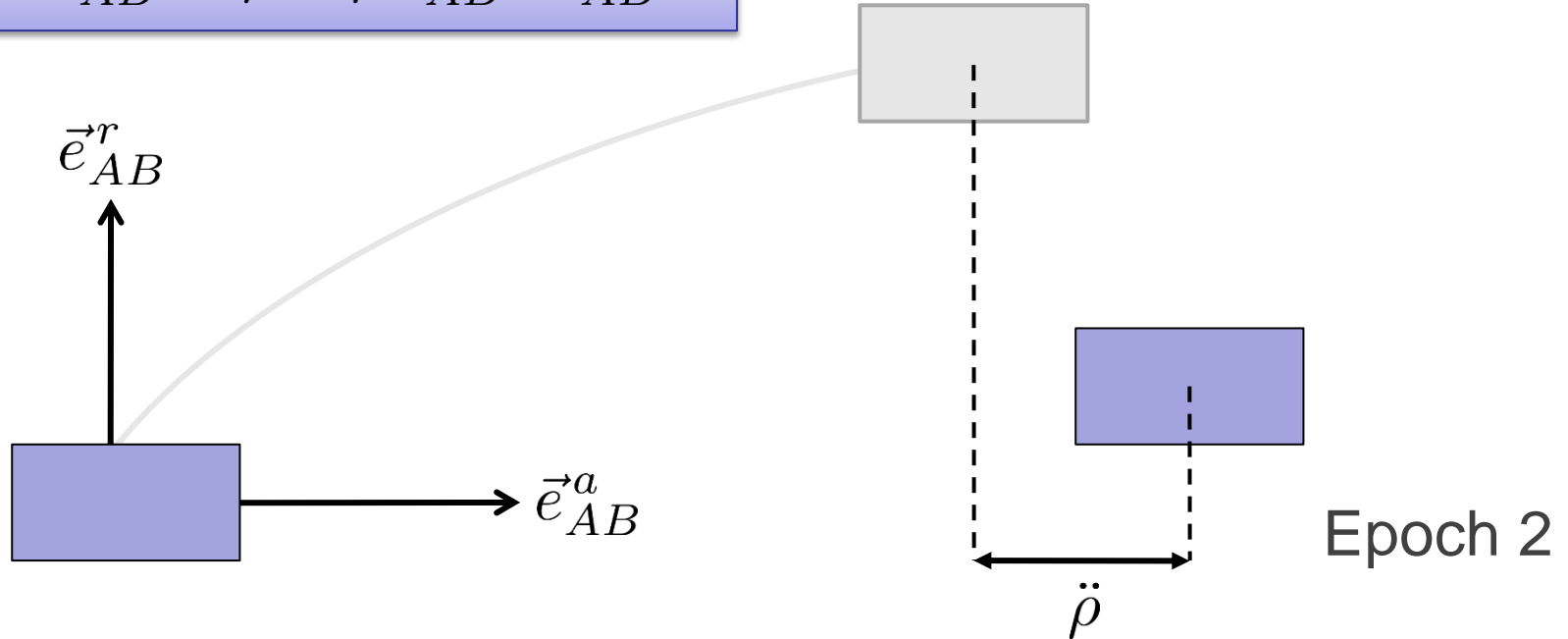
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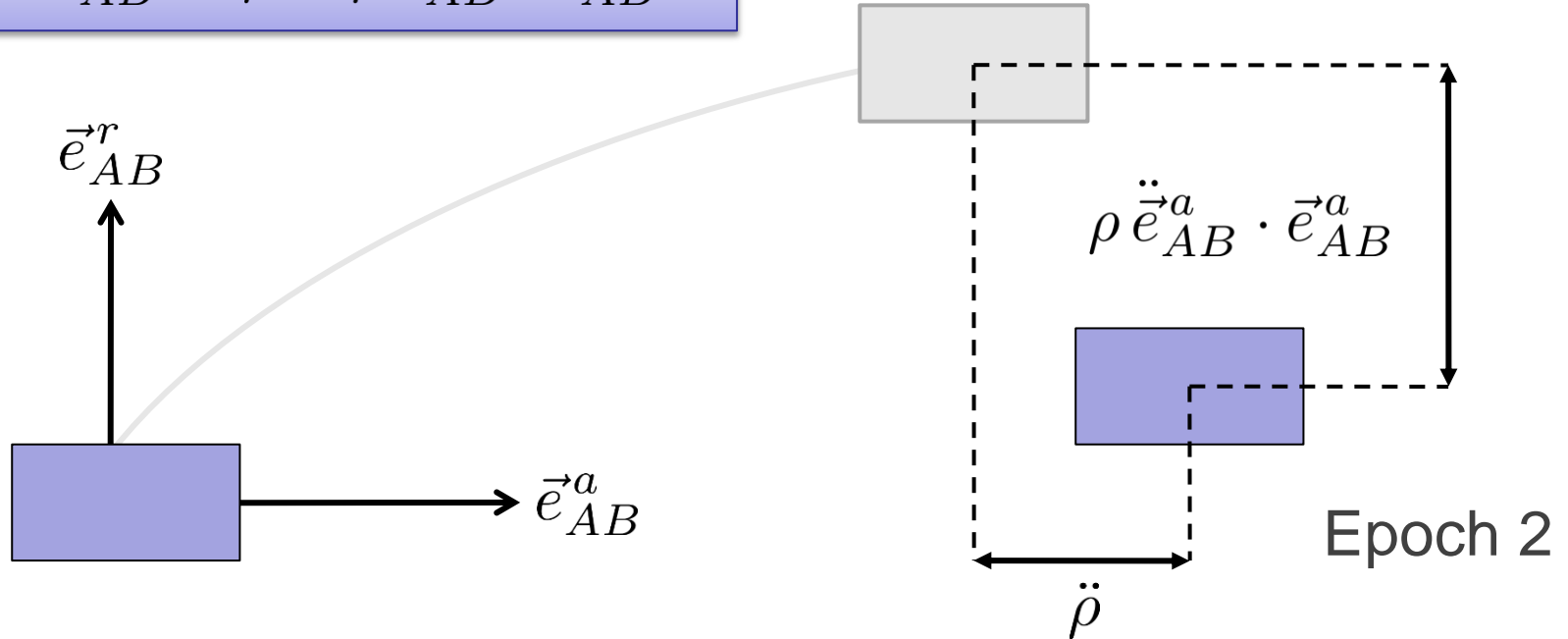
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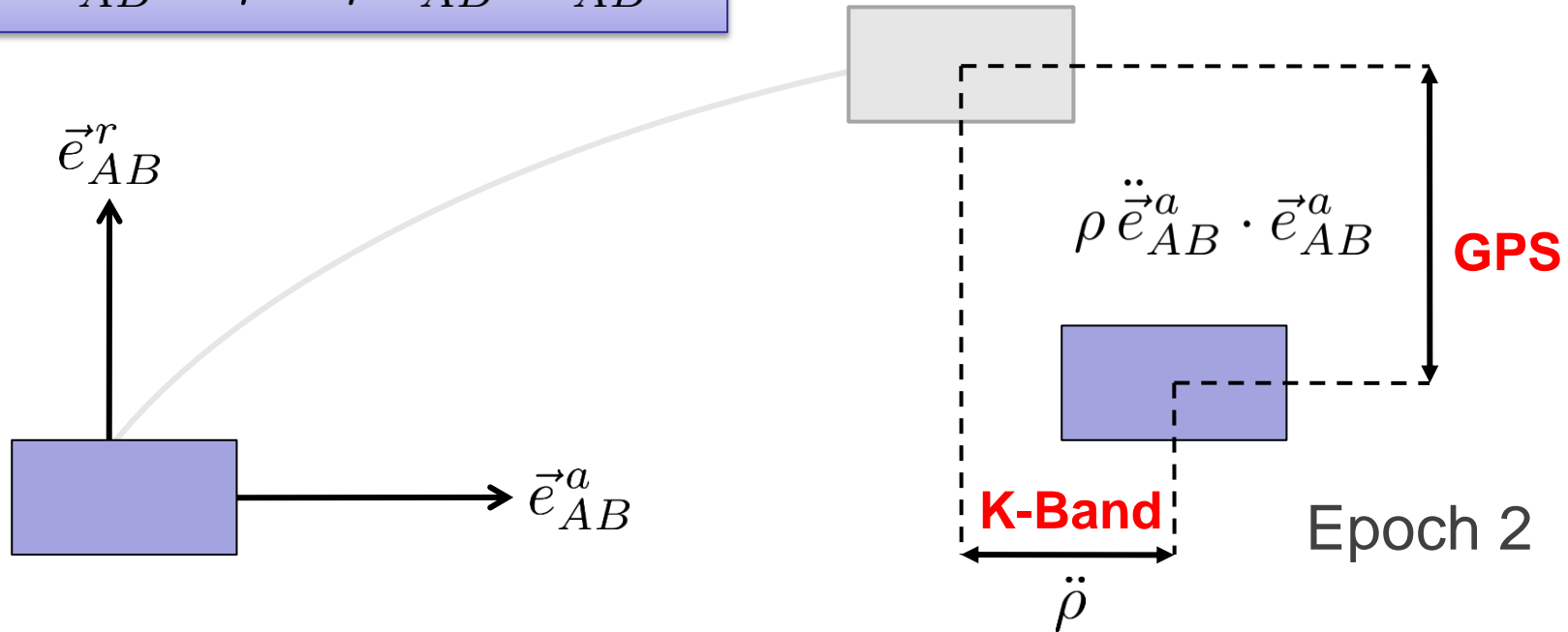
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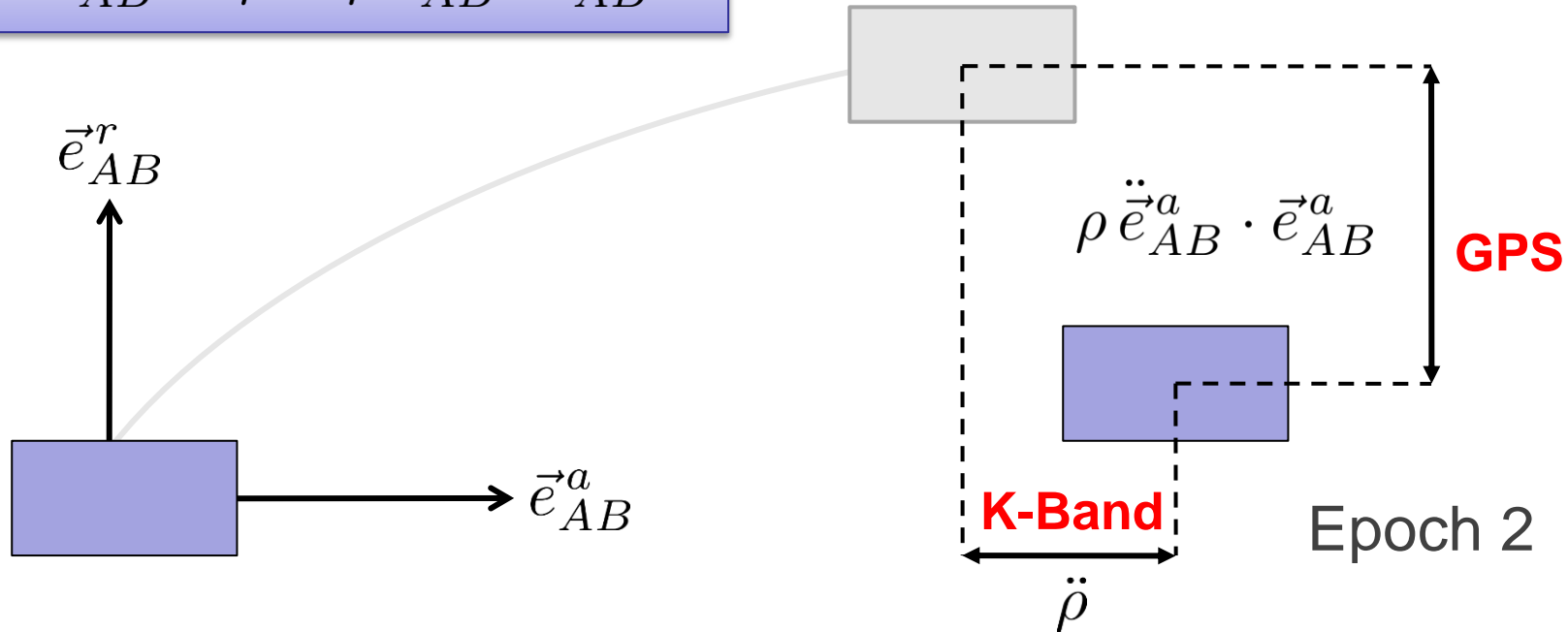
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absolute motion neglected!

$$\ddot{\vec{x}}_{AB} \cdot \vec{e}_{AB}^a = \ddot{\rho} + \rho \ddot{\vec{e}}_{AB}^a \cdot \vec{e}_{AB}^a$$



$$\begin{aligned} \rho \ddot{\vec{e}}_{AB}^a \cdot \vec{e}_{AB}^a &= \ddot{\vec{x}}_{AB} \cdot \vec{e}_{AB}^a = -\dot{\vec{x}}_{AB} \cdot \dot{\vec{e}}_{AB}^a \\ &= -\rho \|\dot{\vec{e}}_{AB}^a\|^2 = -\frac{1}{\rho} \left( \dot{\vec{x}}_{AB} \cdot \dot{\vec{x}}_{AB} - \dot{\rho}^2 \right) \end{aligned}$$



# A VARIANT BASED ON ROTATIONS

# Instantaneous relative reference frame

Remember:

$$\begin{aligned}\ddot{\vec{x}}_{AB} \cdot \vec{e}_{AB}^a &= \ddot{\rho} & + & 0 & + & \rho \ddot{\vec{e}}_{AB}^a \cdot \vec{e}_{AB}^a \\ \ddot{\vec{x}}_{AB} \cdot \vec{e}_{AB}^c &= 0 & + & 0 & + & \rho \ddot{\vec{e}}_{AB}^a \cdot \vec{e}_{AB}^c \\ \ddot{\vec{x}}_{AB} \cdot \vec{e}_{AB}^r &= 0 & + & 2\dot{\rho} \|\dot{\vec{e}}_{AB}^a\| & + & \rho \ddot{\vec{e}}_{AB}^a \cdot \vec{e}_{AB}^r\end{aligned}$$

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Definition:

$$R_F^I = \begin{pmatrix} (\vec{e}_{AB}^a)^T \\ (\vec{e}_{AB}^c)^T \\ (\vec{e}_{AB}^r)^T \end{pmatrix}$$

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$$\Rightarrow \vec{e}_{AB,F}^a = \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} \quad \vec{e}_{AB,F}^c = \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix} \quad \vec{e}_{AB,F}^r = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}$$

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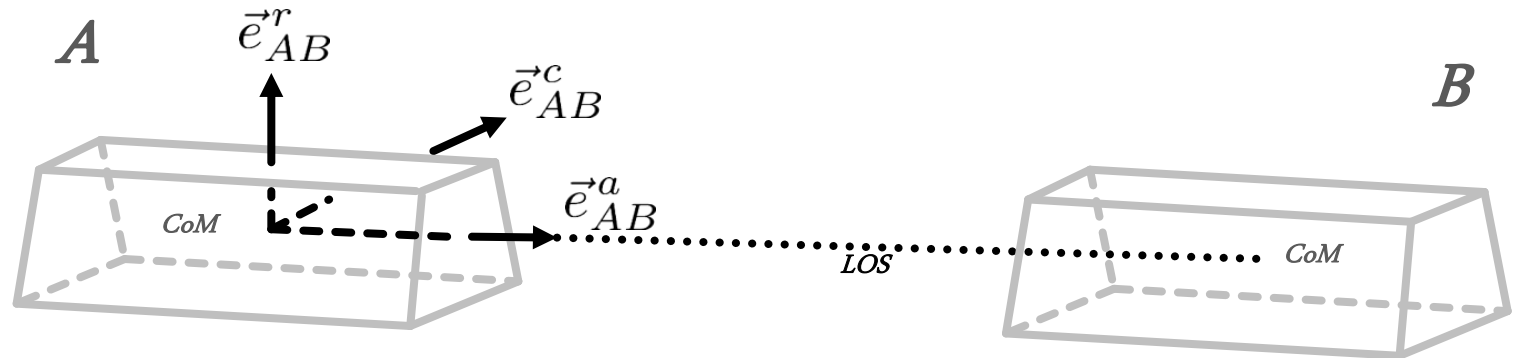
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# Instantaneous relative reference frame

Need for moving frame quantities:

$$R_F^I \vec{e}_{AB}^{a,c,r} = \vec{e}_{AB,F}^{a,c,r}$$



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$$R_F^I \dot{\vec{e}}_{AB}^a = \dot{\vec{e}}_{AB,F}^a + \vec{\omega} \times \vec{e}_{AB,F}^a = \vec{\omega} \times \vec{e}_{AB,F}^a$$

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What about  $\vec{\omega}$ ?

# Instantaneous relative reference frame

Need for moving frame quantities:

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What about  $\vec{\omega}$  ?

defined by the Cartan-Matrix:

$$\Omega = R_F^I \left( \dot{R}_F^I \right)^T = \begin{pmatrix} 0 & -\omega^r & \omega^c \\ \omega^r & 0 & -\omega^a \\ -\omega^c & \omega^a & 0 \end{pmatrix} \quad \dot{R}_F^I = \begin{pmatrix} \left( \dot{\vec{e}}_{AB}^a \right)^T \\ \left( \dot{\vec{e}}_{AB}^c \right)^T \\ \left( \dot{\vec{e}}_{AB}^r \right)^T \end{pmatrix}$$

# Differential gravimetry in the IRRF

Inertial:  $\ddot{\vec{x}}_{AB} = \ddot{\rho} \vec{e}_{AB}^a + 2 \dot{\rho} \dot{\vec{e}}_{AB}^a + \rho \ddot{\vec{e}}_{AB}^a$

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IRRF:  $\ddot{\vec{x}}_{AB,F} = \ddot{\rho} \vec{e}_{AB,F}^a + 2 \dot{\rho} (\vec{\omega} \times \vec{e}_{AB,F}^a) + \rho (\vec{\omega} \times (\vec{\omega} \times \vec{e}_{AB,F})) + \rho (\dot{\vec{\omega}} \times \vec{e}_{AB,F})$

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with  $\vec{\omega} = (\omega^a, \omega^c, \omega^r)^T$  and introducing  $\nabla V_{AB,F}$  :

$$\nabla V_{AB,F} \cdot \vec{e}_{AB,F}^a = \ddot{\rho} - \rho \left( (\omega^c)^2 + (\omega^r)^2 \right)$$

$$\nabla V_{AB,F} \cdot \vec{e}_{AB,F}^c = 2 \dot{\rho} \omega^r - \rho \omega^a \omega^c + \rho \dot{\omega}^r$$

$$\nabla V_{AB,F} \cdot \vec{e}_{AB,F}^r = -2 \dot{\rho} \omega^c + \rho \omega^a \omega^r - \rho \dot{\omega}^c$$

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# INSTANTANEOUS RELATIVE REFERENCE FRAME

# What is the optimal choice for the IRRF?

Obviously given:  $\vec{e}_{AB}^a$

“Ambiguity” for  $\vec{e}_{AB}^r$  :

- radial direction of GRACE A
- radial direction of GRACE B
- radial direction of midpoint
- ...

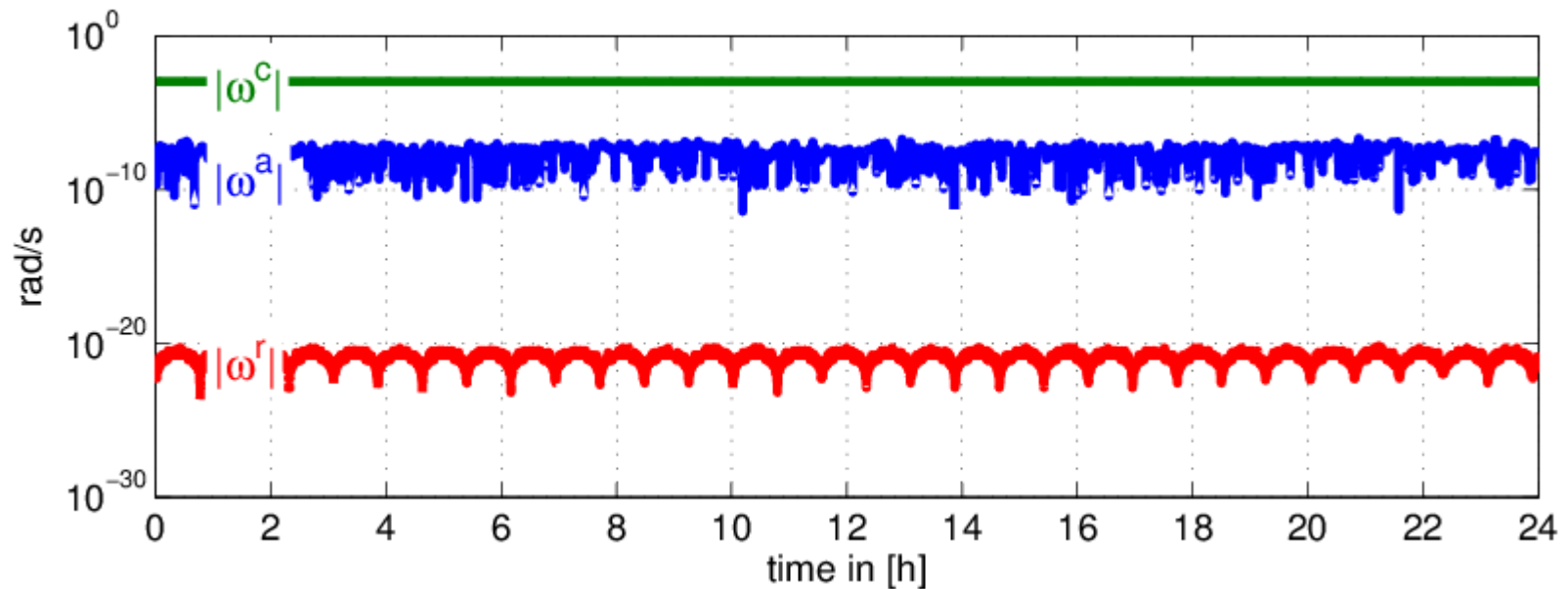
Other considerations:

- accessibility
- accuracy
- simplification
- physical meaning

# Instantaneous relative reference frame

Most useful implementation at the current stage:

$$\vec{e}_{AB}^v = \frac{\dot{\vec{x}}_{AB}}{\|\dot{\vec{x}}_{AB}\|} \quad \vec{e}_{AB}^c = \frac{\vec{e}_{AB}^v \times \vec{e}_{AB}^a}{\|\vec{e}_{AB}^v \times \vec{e}_{AB}^a\|} \quad \vec{e}_{AB}^r = \frac{\vec{e}_{AB}^a \times \vec{e}_{AB}^c}{\|\vec{e}_{AB}^a \times \vec{e}_{AB}^c\|}$$



# Instantaneous relative reference frame

Best approximation at the current stage:

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$$\nabla V_{AB,F} \cdot \vec{e}_{AB,F}^a = \ddot{\rho} \quad -\rho (\omega^c)^2$$

$$\nabla V_{AB,F} \cdot \vec{e}_{AB,F}^c = \quad -\rho \omega^a \omega^c$$

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$$\nabla V_{AB,F} \cdot \vec{e}_{AB,F}^a = \ddot{\rho} - \rho (\omega^c)^2$$

$$\nabla V_{AB,F} \cdot \vec{e}_{AB,F}^c = -\rho \omega^a \omega^c$$

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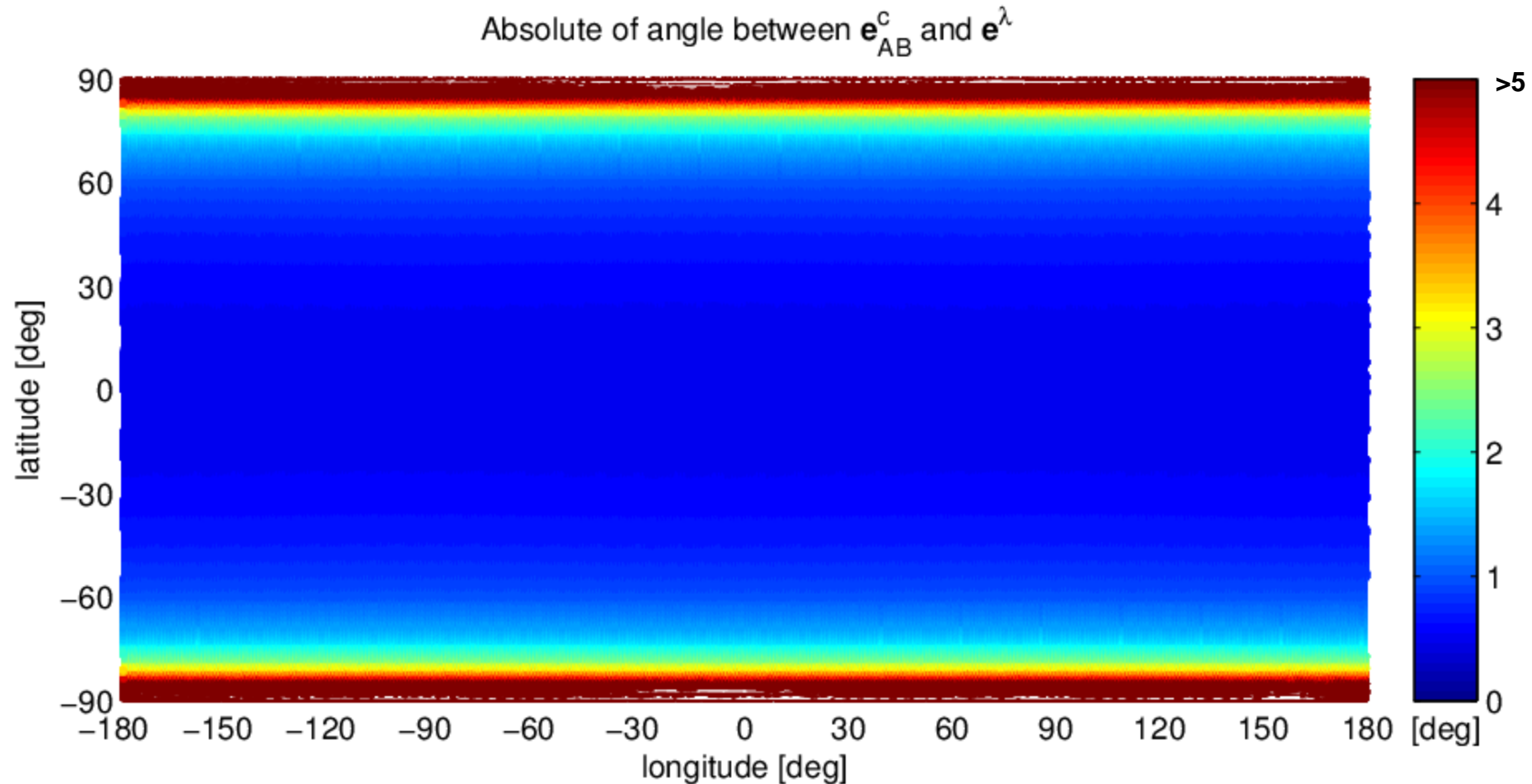
Note the similarity:

$$\nabla V_{AB} \cdot \vec{e}_{AB}^a = \ddot{\rho} + \rho \ddot{\vec{e}}_{AB}^a \cdot \vec{e}_{AB}^a$$

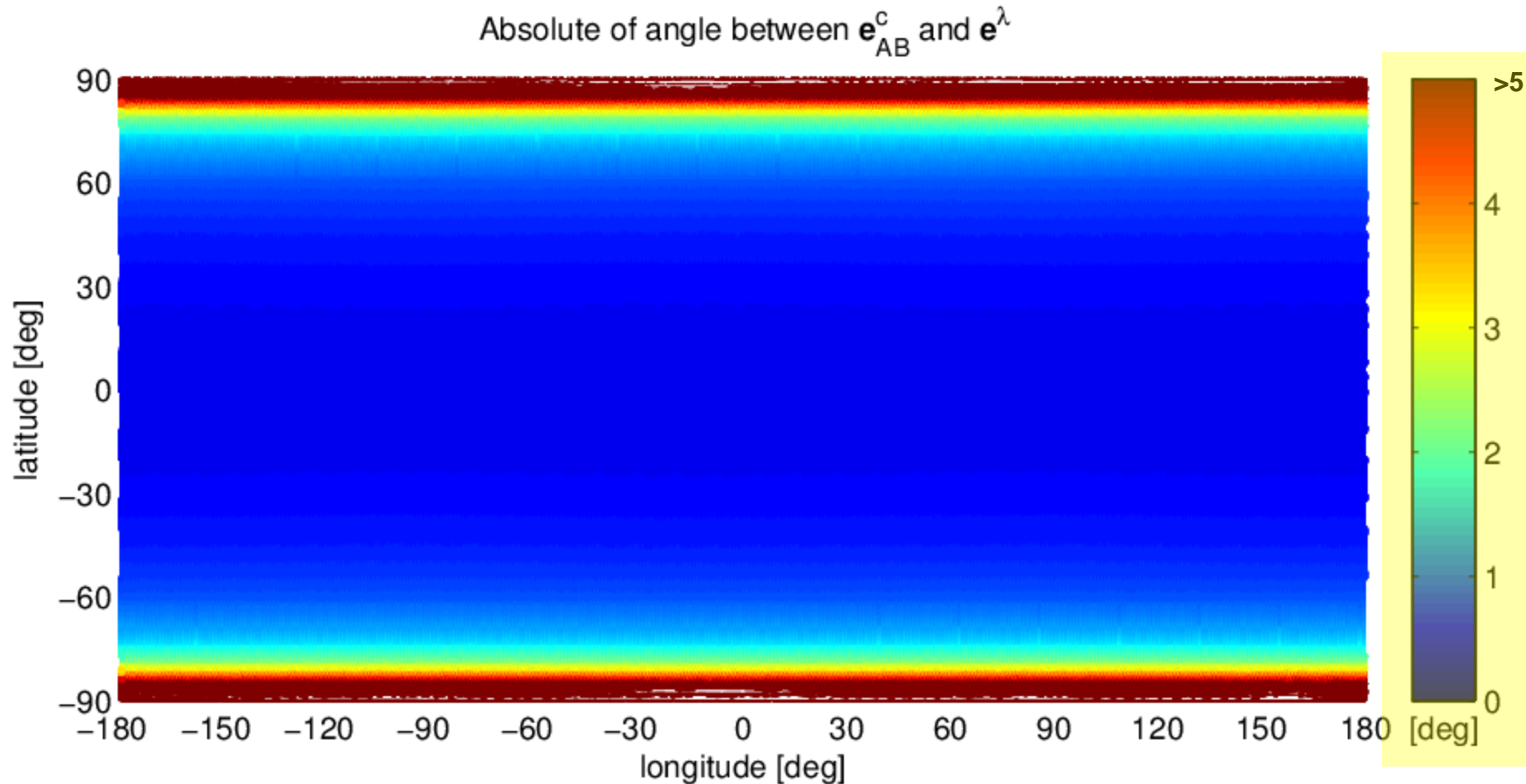
$$\nabla V_{AB} \cdot \vec{e}_{AB}^c = +\rho \ddot{\vec{e}}_{AB}^a \cdot \vec{e}_{AB}^c$$

$$\nabla V_{AB} \cdot \vec{e}_{AB}^r = 2 \dot{\rho} \|\dot{\vec{e}}_{AB}^a\| + \rho \ddot{\vec{e}}_{AB}^a \cdot \vec{e}_{AB}^r$$

# Relation cross-track to East-West direction



# Relation cross-track to East-West direction





# Summary

- Derivation of the acceleration approach based on rotations  
→ creating the chance of using star cameras instead of GPS
- (Free) choice of the moving frame allows for optimisation
- Determination of  $\omega^c$  and  $\dot{\omega}^c$  allows for a second (observed) component.
- Explanation of the low East-West sensitivity
- Necessity for GPS observations (determination of the frame)
- Open questions:
  - Can  $\omega^c$  be determined by the star camera (accuracy) ?
  - Is it possible to find a frame which also fulfils:  $\omega^a = 0$  ?

# A new variant of the differential gravimetry approach



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