

A new variant of the differential gravimetry approach



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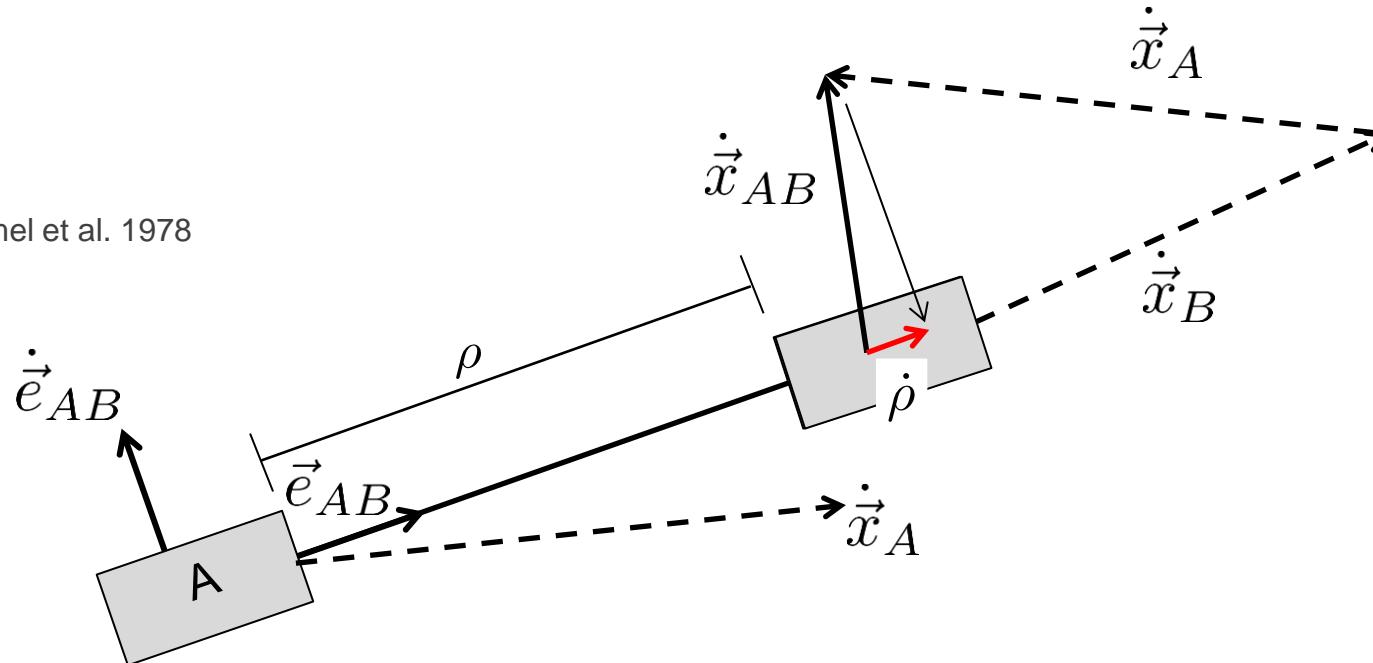
RUES |
RESEARCH UNIT
IN ENGINEERING
SCIENCES

FACULTY OF SCIENCES, TECHNOLOGY AND COMMUNICATION



Geometry of the GRACE system

Rummel et al. 1978



Differentiation
Integration

$$\rho = \vec{r}_{AB} \cdot \vec{e}_{AB}$$

$$\dot{\rho} = \dot{\vec{r}}_{AB} \cdot \vec{e}_{AB}$$

$$\begin{aligned}\ddot{\rho} &= \ddot{\vec{r}}_{AB} \cdot \vec{e}_{AB} + \dot{\vec{r}}_{AB} \cdot \dot{\vec{e}}_{AB} \\ &= \nabla V_{AB}\end{aligned}$$

Solution strategies

Variational equations

Classical

(Reigber 1989, Tapley 2004)

$$\rho, \dot{\rho}$$

Celestial Mechanics approach

(Beutler et al. 2010, Jäggi 2007)

$$\rho, \dot{\rho}, \Delta\rho$$

Short-arc method

(Mayer-Gürr 2006)

$$\rho, \dot{\rho}$$

...

In-situ observations

Energy Integral

(Han 2003, Ramillien et al. 2010)

$$\dot{\rho}$$

Differential gravimetry

(Liu 2010)

$$\ddot{\rho}$$

LoS Gradiometry

(Keller and Sharifi 2005)

$$\frac{\ddot{\rho}}{\rho}$$

...

DIFFERENTIAL GRAVIMETRY

THE STANDARD APPROACH

Differential gravimetry

Range observables: $\vec{x}_{AB} = \rho \vec{e}_{AB}^a$

Differential gravimetry

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Differential gravimetry

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Differential gravimetry

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Multiplication with unit vectors in along-track, cross-track and radial direction:

$$\ddot{\vec{x}}_{AB} \cdot \vec{e}_{AB}^a = \ddot{\rho} + 0 + \rho \ddot{\vec{e}}_{AB}^a \cdot \vec{e}_{AB}^a$$

$$\ddot{\vec{x}}_{AB} \cdot \vec{e}_{AB}^c = 0 + 0 + \rho \ddot{\vec{e}}_{AB}^a \cdot \vec{e}_{AB}^c$$

$$\ddot{\vec{x}}_{AB} \cdot \vec{e}_{AB}^r = 0 + 2 \dot{\rho} \|\dot{\vec{e}}_{AB}^a\| + \rho \ddot{\vec{e}}_{AB}^a \cdot \vec{e}_{AB}^r$$

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GRACE

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Relative motion

$$\ddot{\vec{x}}_{AB} \cdot \vec{e}_{AB}^a = \ddot{\rho} + \rho \ddot{\vec{e}}_{AB}^a \cdot \vec{e}_{AB}^a$$

Epoch 1



Relative motion

absolute motion neglected!

$$\ddot{\vec{x}}_{AB} \cdot \vec{e}_{AB}^a = \ddot{\rho} + \rho \ddot{\vec{e}}_{AB}^a \cdot \vec{e}_{AB}^a$$

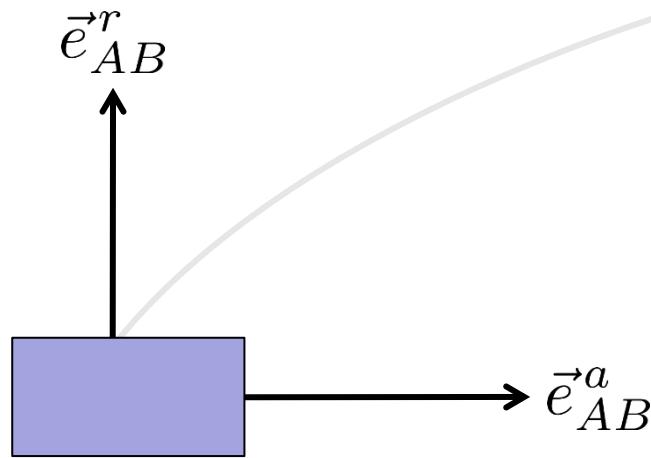


Epoch 2

Relative motion

absolute motion neglected!

$$\ddot{\vec{x}}_{AB} \cdot \vec{e}_{AB}^a = \ddot{\rho} + \rho \ddot{\vec{e}}_{AB}^a \cdot \vec{e}_{AB}^a$$

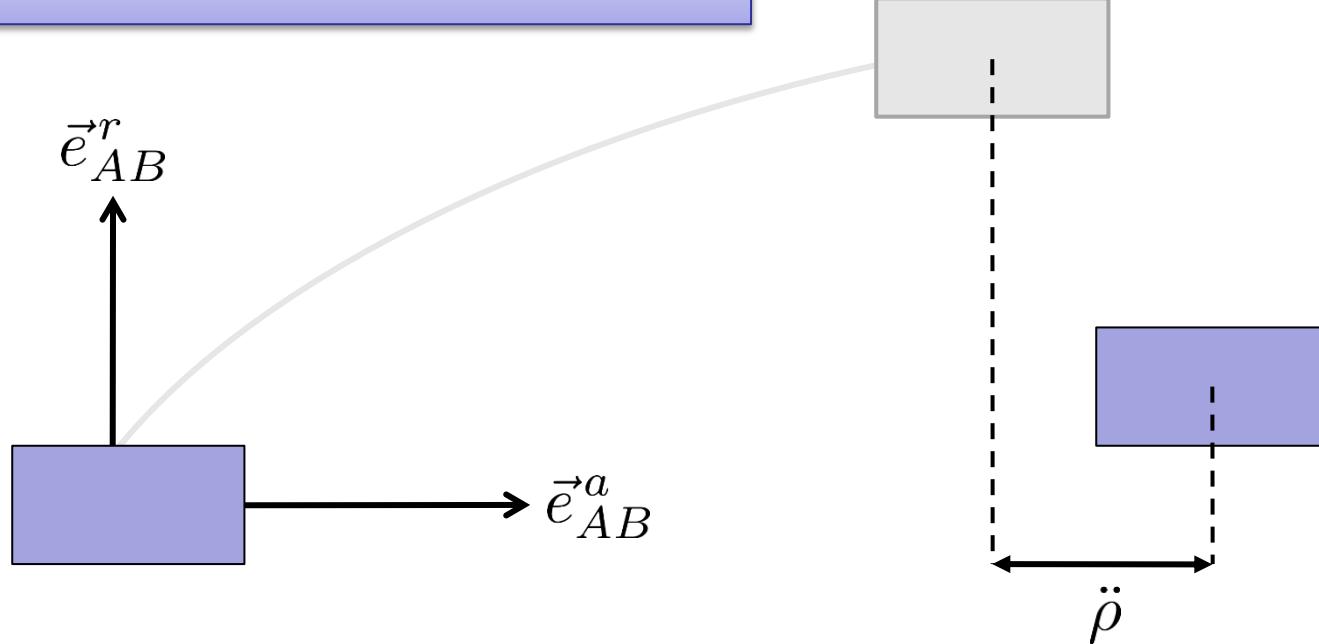


Epoch 2

Relative motion

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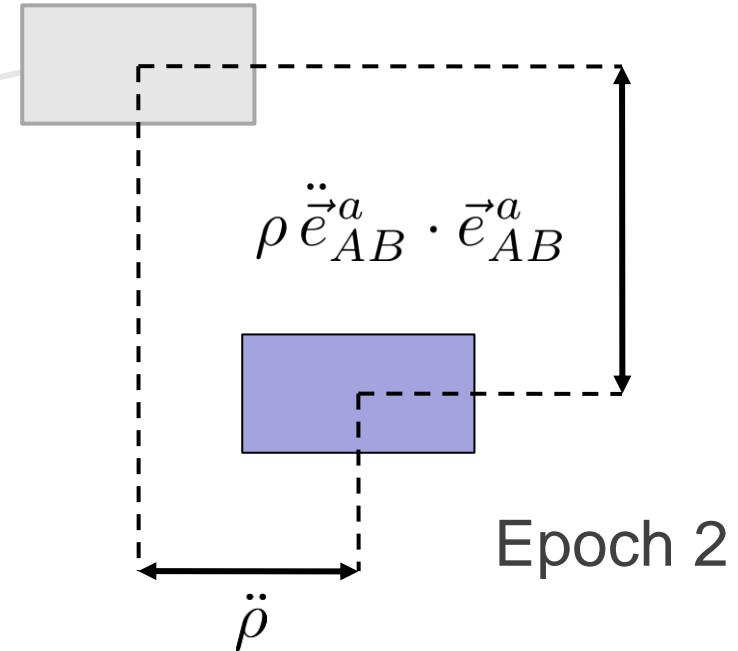
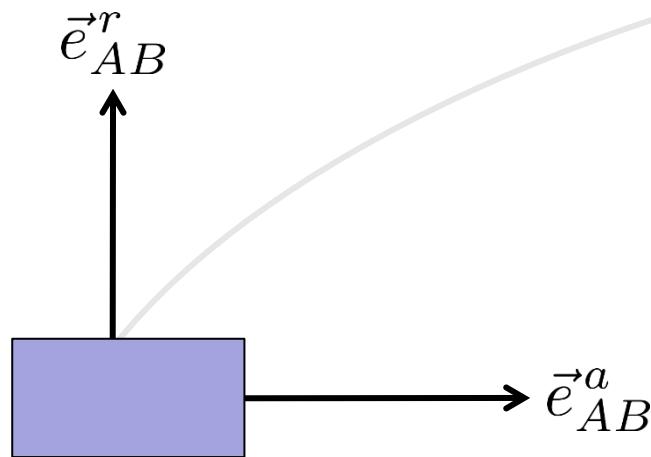
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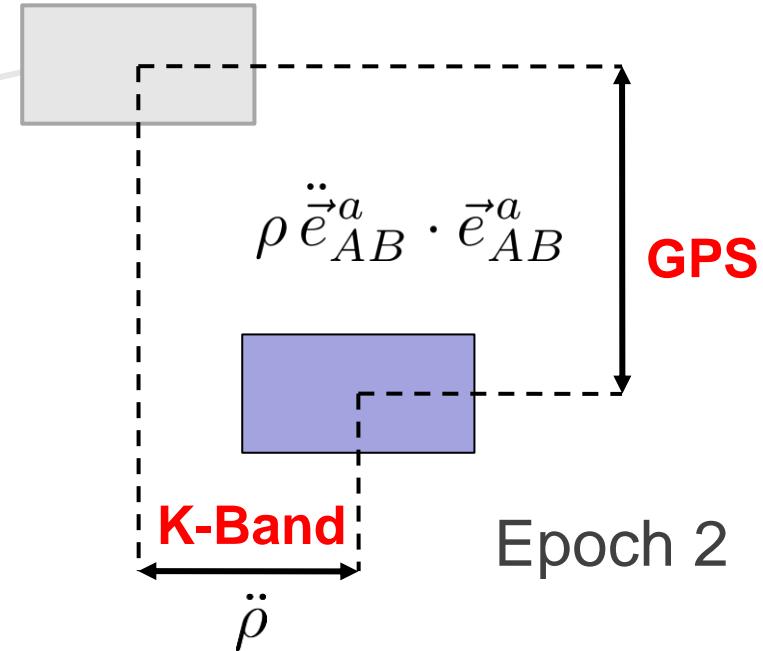
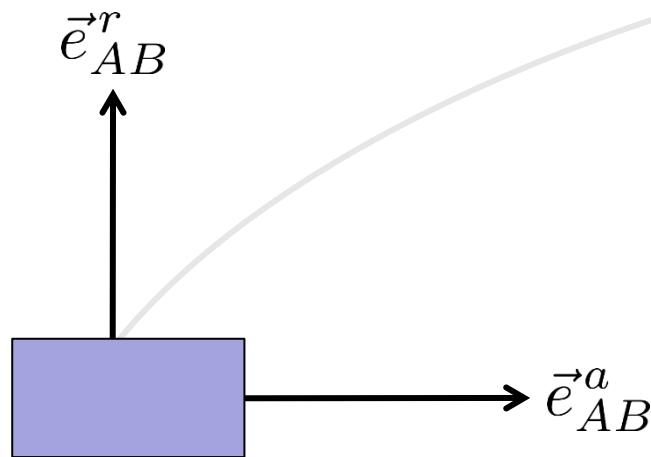


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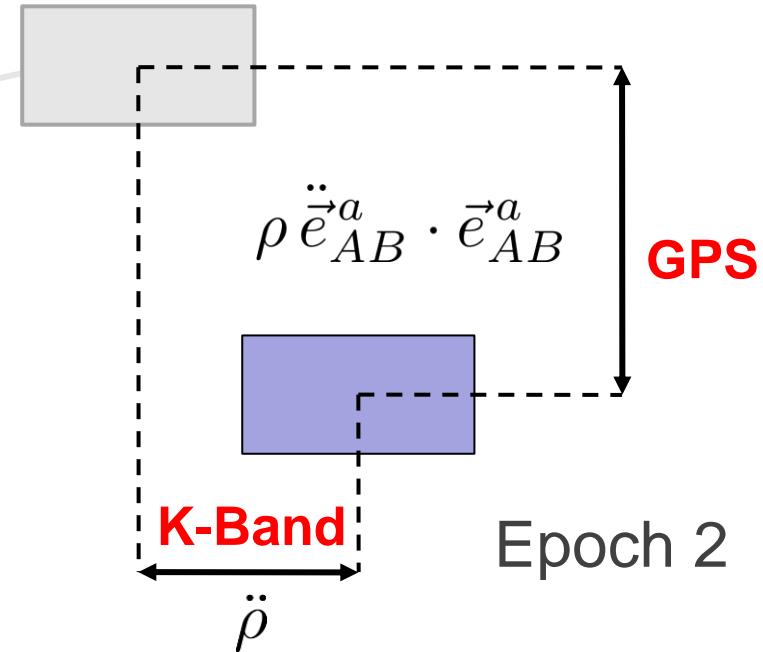
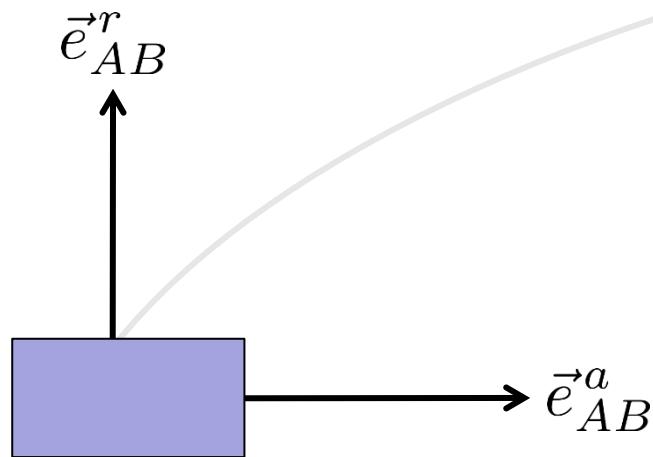
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$$\begin{aligned} \rho \ddot{\vec{e}}_{AB}^a \cdot \vec{e}_{AB}^a &= \vec{x}_{AB} \cdot \ddot{\vec{e}}_{AB}^a = -\dot{\vec{x}}_{AB} \cdot \dot{\vec{e}}_{AB}^a \\ &= -\rho \|\dot{\vec{e}}_{AB}^a\|^2 = -\frac{1}{\rho} \left(\dot{\vec{x}}_{AB} \cdot \dot{\vec{x}}_{AB} - \dot{\rho}^2 \right) \end{aligned}$$

A VARIANT BASED ON ROTATIONS

Instantaneous relative reference frame

Remember:

$$\begin{aligned}\ddot{\vec{x}}_{AB} \cdot \vec{e}_{AB}^a &= \ddot{\rho} + 0 + \rho \ddot{\vec{e}}_{AB}^a \cdot \vec{e}_{AB}^a \\ \ddot{\vec{x}}_{AB} \cdot \vec{e}_{AB}^c &= 0 + 0 + \rho \ddot{\vec{e}}_{AB}^a \cdot \vec{e}_{AB}^c \\ \ddot{\vec{x}}_{AB} \cdot \vec{e}_{AB}^r &= 0 + 2\dot{\rho} \|\dot{\vec{e}}_{AB}^a\| + \rho \ddot{\vec{e}}_{AB}^a \cdot \vec{e}_{AB}^r\end{aligned}$$

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Definition:

$$R_F^I = \begin{pmatrix} (\vec{e}_{AB}^a)^T \\ (\vec{e}_{AB}^c)^T \\ (\vec{e}_{AB}^r)^T \end{pmatrix}$$

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→ $\vec{e}_{AB,F}^a = \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} \quad \vec{e}_{AB,F}^c = \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix} \quad \vec{e}_{AB,F}^r = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}$

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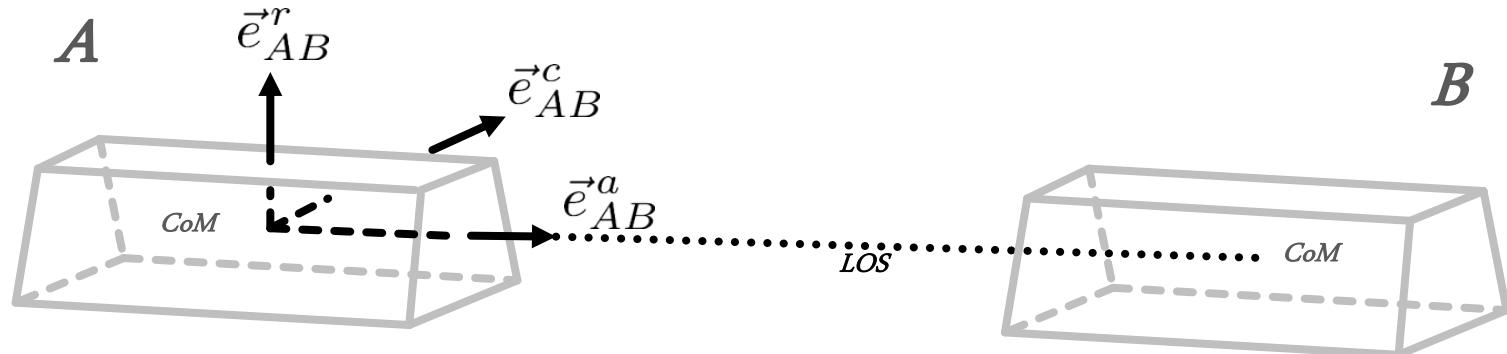
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Need for moving frame quantities:

$$R_F^I \vec{e}_{AB}^{a,c,r} = \vec{e}_{AB,F}^{a,c,r}$$

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$$R_F^I \dot{\vec{e}}_{AB}^a = \dot{\vec{e}}_{AB,F}^a + \vec{\omega} \times \vec{e}_{AB,F}^a = \vec{\omega} \times \vec{e}_{AB,F}^a$$

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What about $\vec{\omega}$?

Instantaneous relative reference frame

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What about $\vec{\omega}$?

defined by the Cartan-Matrix:

$$\Omega = R_F^I \left(\dot{R}_F^I \right)^T = \begin{pmatrix} 0 & -\omega^r & \omega^c \\ \omega^r & 0 & -\omega^a \\ -\omega^c & \omega^a & 0 \end{pmatrix} \quad \dot{R}_F^I = \begin{pmatrix} \left(\dot{\vec{e}}_{AB}^a \right)^T \\ \left(\dot{\vec{e}}_{AB}^c \right)^T \\ \left(\dot{\vec{e}}_{AB}^r \right)^T \end{pmatrix}$$

Differential gravimetry in the IRRF

Inertial: $\ddot{\vec{x}}_{AB} = \ddot{\rho} \vec{e}_{AB}^a + 2 \dot{\rho} \dot{\vec{e}}_{AB}^a + \ddot{\rho} \vec{e}_{AB}^a$

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IRRF: $\ddot{\vec{x}}_{AB,F} = \ddot{\rho} \vec{e}_{AB,F}^a + 2 \dot{\rho} (\vec{\omega} \times \vec{e}_{AB,F}^a)$
 $+ \rho (\vec{\omega} \times (\vec{\omega} \times \vec{e}_{AB,F})) + \rho (\dot{\vec{\omega}} \times \vec{e}_{AB,F})$

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with $\vec{\omega} = (\omega^a, \omega^c, \omega^r)^T$ and introducing $\nabla V_{AB,F}$:

$$\nabla V_{AB,F} \cdot \vec{e}_{AB,F}^a = \ddot{\rho} - \rho ((\omega^c)^2 + (\omega^r)^2)$$

$$\nabla V_{AB,F} \cdot \vec{e}_{AB,F}^c = 2 \dot{\rho} \omega^r - \rho \omega^a \omega^c + \rho \dot{\omega}^r$$

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INSTANTANEOUS RELATIVE REFERENCE FRAME

What is the optimal choice for the IRRF?

Obviously given: \vec{e}_{AB}^a

“Ambiguity” for \vec{e}_{AB}^r :

- radial direction of GRACE A
- radial direction of GRACE B
- radial direction of midpoint
- ...

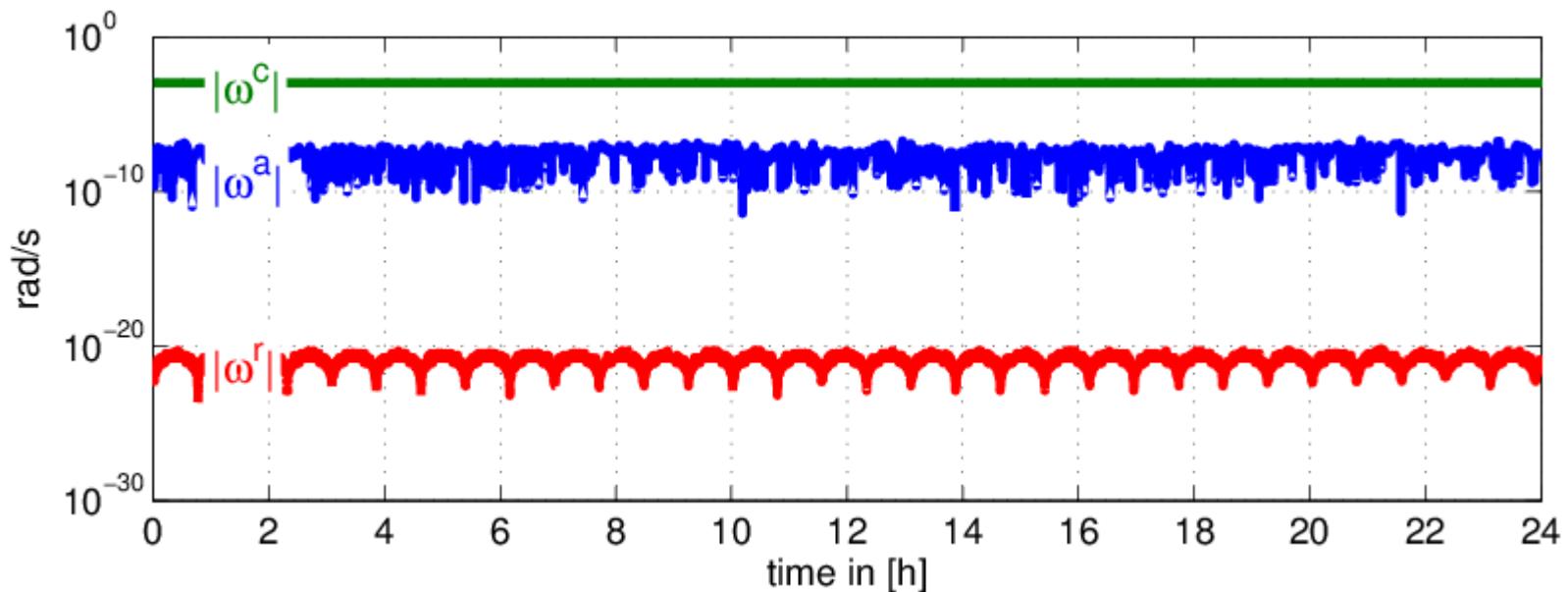
Other considerations:

- accessibility
- accuracy
- simplification
- physical meaning

Instantaneous relative reference frame

Most useful implementation at the current stage:

$$\vec{e}_{AB}^v = \frac{\dot{\vec{x}}_{AB}}{\|\dot{\vec{x}}_{AB}\|} \quad \vec{e}_{AB}^c = \frac{\vec{e}_{AB}^v \times \vec{e}_{AB}^a}{\|\vec{e}_{AB}^v \times \vec{e}_{AB}^a\|} \quad \vec{e}_{AB}^r = \frac{\vec{e}_{AB}^a \times \vec{e}_{AB}^c}{\|\vec{e}_{AB}^a \times \vec{e}_{AB}^c\|}$$



Instantaneous relative reference frame

Best approximation at the current stage:

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$$\nabla V_{AB,F} \cdot \vec{e}_{AB,F}^a = \ddot{\rho} - \rho (\omega^c)^2$$

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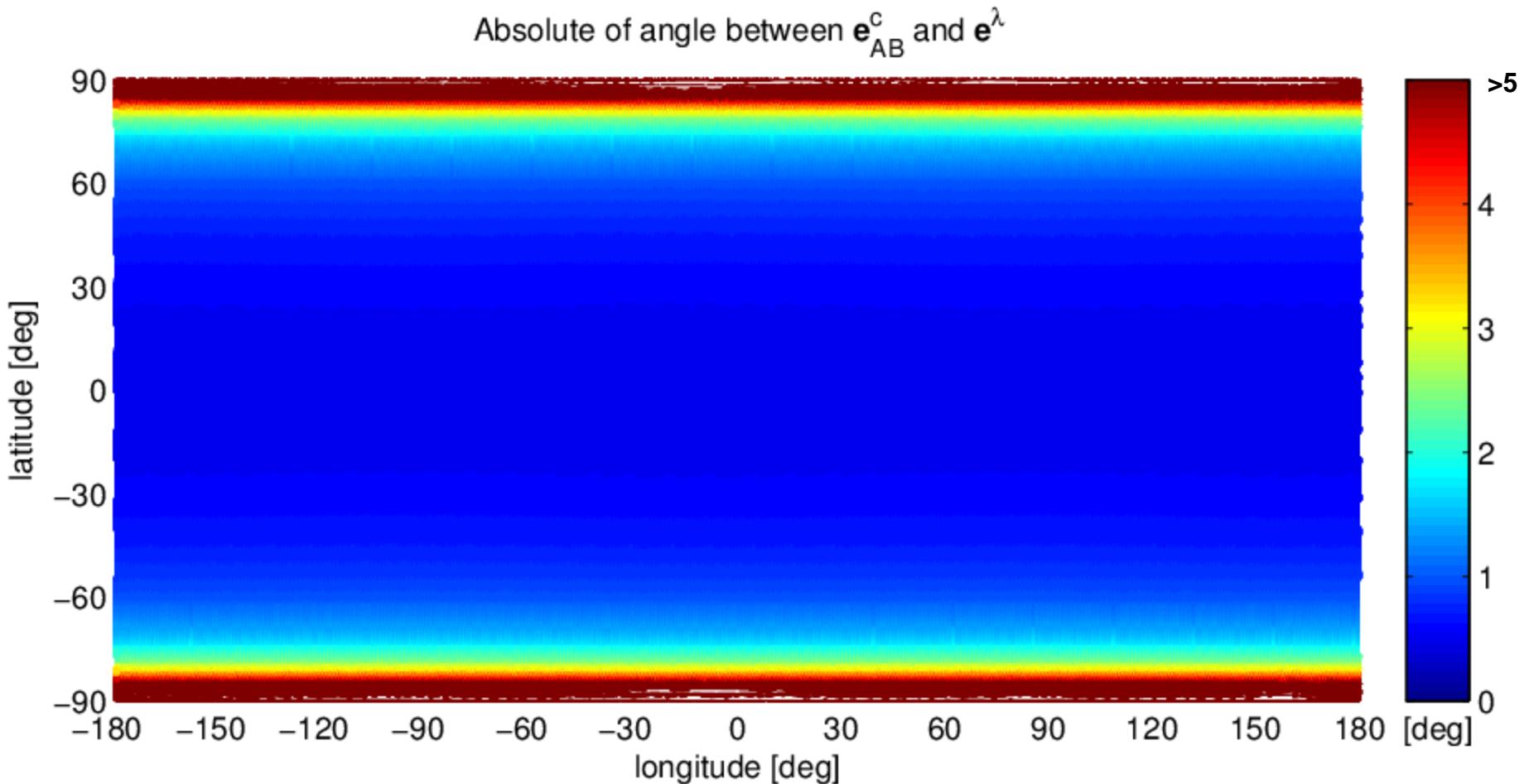
Note the similarity:

$$\nabla V_{AB} \cdot \vec{e}_{AB}^a = \ddot{\rho} + \rho \ddot{\vec{e}}_{AB}^a \cdot \vec{e}_{AB}^a$$

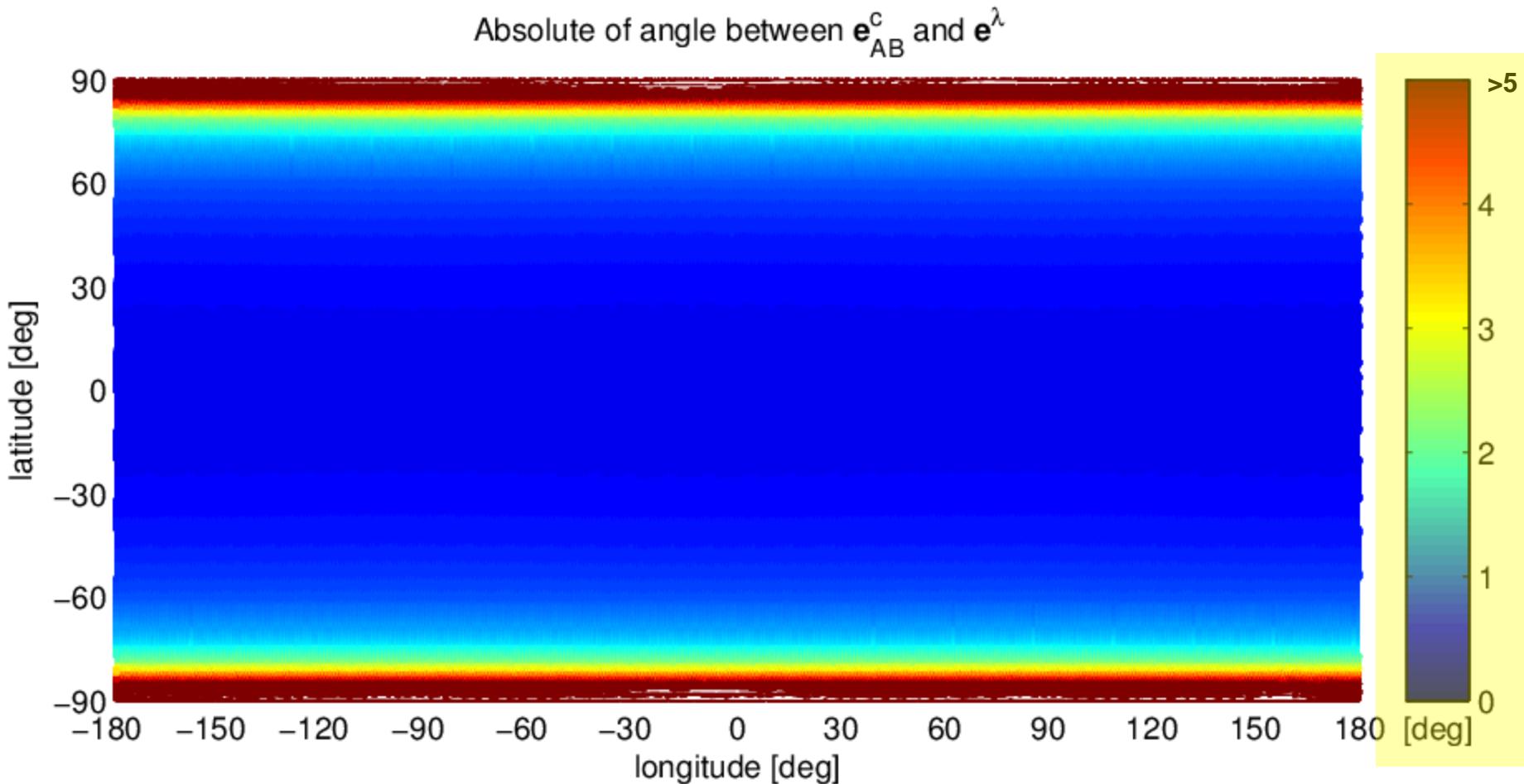
$$\nabla V_{AB} \cdot \vec{e}_{AB}^c = +\rho \ddot{\vec{e}}_{AB}^a \cdot \vec{e}_{AB}^c$$

$$\nabla V_{AB} \cdot \vec{e}_{AB}^r = 2 \dot{\rho} \|\dot{\vec{e}}_{AB}^a\| + \rho \ddot{\vec{e}}_{AB}^a \cdot \vec{e}_{AB}^r$$

Relation cross-track to East-West direction



Relation cross-track to East-West direction



Summary

- Derivation of the acceleration approach based on rotations
→ creating the chance of using star cameras instead of GPS
- (Free) choice of the moving frame allows for optimisation
- Determination of ω^c and $\dot{\omega}^c$ allows for a second (observed) component.
- Explanation of the low East-West sensitivity
- Necessity for GPS observations (determination of the frame)
- Open questions:
 - Can ω^c be determined by the star camera (accuracy) ?
 - Is it possible to find a frame which also fulfills: $\omega^a = 0$?

A new variant of the differential gravimetry approach



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RESEARCH UNIT
IN ENGINEERING
SCIENCES

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